

# Djelovanje vjetra na građevinske konstrukcije

- utjecaj vjetra na stabilnost građevinske konstrukcije
- utjecaj vjetra na sigurnost prometa
- utjecaj vjetra na pronos tvari (ekologija)
- ...

# Vladajuće jednačbe

**Osnovni zakoni koji vrijede za opisivanje opstrujanja zraka oko tijela malim brzinama su:**

- a) zakon održanja mase,**
- b) II Newtonov zakon i**
- c) prvi zakon termodinamike**

- + konstitutivne jednačbe za zrak
- + rubni i početni uvjeti

Proučavat će se opstrujavnje oko tijela za male brzine zraka u kojima ne dolazi do njegove stišljivosti odnosno promatrat će se pojave vezane za brzine strujanja do 0.4 Macha tj. do  $v = 134 \text{ m/s}$ .

# Zakon održanja mase

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho v) = 0$$

pri čemu je:  
 $\rho$  gustoća fluida  
 $v$  vektor brzine

# Drugi Newtonov zakon

$$\rho \left( \frac{dv}{dt} \right) = \rho F_B + F_s$$

$F_B$  volumna sila po jedinici mase

$F_s$  površinska sila

Derivacija brzine se sastoji od lokalne i konvektivne komponente

$$\rho \left( \frac{dv}{dt} \right) = \rho \left( \frac{\partial v}{\partial t} + (v \cdot \nabla) v \right)$$

Uvrštavanjem Stokesovog zakona za opis površinskih sila dobiva se Navier-Stokesova jednačba

$$\rho \frac{d\vec{v}}{dt} = \rho \vec{R} - \text{grad } p + \mu \nabla^2 \vec{v}$$

# Prvi zakon termodinamike

(matematički zapis principa održanja energije)

$$\rho \frac{\partial}{\partial t} \left( C_v T + \frac{v^2}{2} \right) + \rho v \cdot \nabla \left( C_v T + \frac{v^2}{2} \right) =$$
$$\rho g \cdot v - \nabla \cdot p v + \nabla \cdot \left[ 2\mu \nabla \left( \frac{v^2}{2} \right) + \mu (\nabla \times v) \times v - \frac{2}{3} \mu (\nabla \cdot v) v \right] + \nabla \cdot k \nabla T$$

pri čemu je:

- $T$  temperatura
- $C_v$  specifična toplina
- $k$  termalna provodljivost

**Najbolji pristup rješavanju praktički svih aerodinamičkih problema se zasniva na odgovarajuće kombiniranim rezultatima eksperimentalnih istraživanja, teoretskih razmatranja te numeričkih simulacijama na računalu usmjeravanih iskustvom.**

# Karakteristike zraka

## Gustoća zraka

$$\rho_a = \left( \frac{0.0034847}{T} \right) (p - 0.003796 R_h e_s)$$

$R_h$  relativna vlaga  
 $T$  temperatura ( $^{\circ}\text{K}$ )  
 $p$  tlak (Pa)

## Napon vodenih para

$$e_s = (1.7526 \times 10^{11}) e^{\left( \frac{-5315.56}{T} \right)}$$

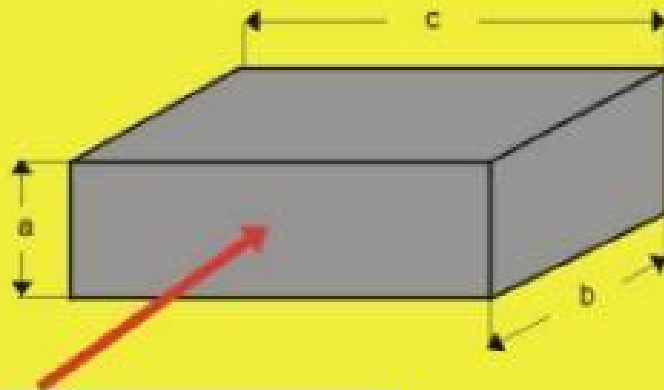
## Standardne (prosječne) karakteristike zraka

Karakteristike zraka	
Gustoća	1,225 kg/m <sup>3</sup>
Tlak	101 325 Pa [N/m <sup>2</sup> ]
Viskoznost $\mu$	1.791 × 10 <sup>-6</sup> kg/m-s
Kinematska viskoznost $\nu$	1.44 × 10 <sup>-5</sup> m <sup>2</sup> /s

# Aerodinamičko opterećenje od vjetra

$$F = c_f \rho A \frac{v^2}{2}$$

$$q_{ref} = \rho \frac{v^2}{2}$$



Smjer djelovanja vjetra

Na građevinske strukture djeluju sile vjetra koje ovise o obliku strukture i jačini vjetra. Generalno, djeluju tlačne, usisne i sile trenja.

Ukupna sila djelovanja vjetra dana je u formi:

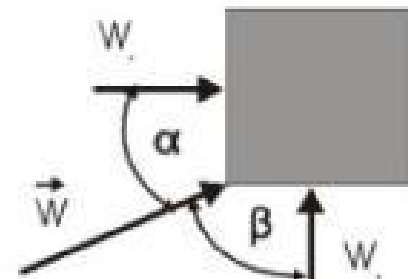
$$W = c_f q A$$

$C_f$  - bezdimenzionalni aerodinamički koeficijent (za jednostavne oblike vrijednosti su dane u tablicama normi)

Pri djelovanju kutne devijacije (odmaka) vektora brzina od geometrijskih osi tijela komponente ukupne sile u smjeru osi tijela (x,y) izražene su kao:

$$W_x = |\vec{W}| \cdot \cos \alpha$$

$$W_y = |\vec{W}| \cdot \cos \beta$$





# Sile otpora oblika

Sile vjeta na strukturu  
(definicija preuzeta iz EUROCODE 1, dio 2.4 ; 6.6)

referentna vremenski osrednjena (10min)  
dinamička komponenta tlaka na 10m visine iznad  
terena druge kategorije, povratnog perioda 50g.

dinamički koeficijent povećanja pri  
vremenski promjenjivom intenzitetu  
djelovanja vjeta

ravninska projekcija  
strukture okomito na  
smjer djelovanja vjeta

$$F_W = q_{ref} \cdot c_e(z_e) \cdot c_d \cdot c_f \cdot A_{ref}$$

koeficijent okoline u kojem je uzeta u  
obzir konfiguracija terena, visina iznad tla  
i efekti turbulencije

koeficijent otpora oblika  
opstrujavane strukture

# Sile otpora trenja

Sile trenja vjetra na strukturu  
(definicija preuzeta iz EUROCODE 1, dio 2.4 ; 6.6)

referentna vremenski osrednjena (10min)  
dinamička komponenta tlaka na 10m visine iznad  
terena druge kategorije, povratnog perioda 50g.

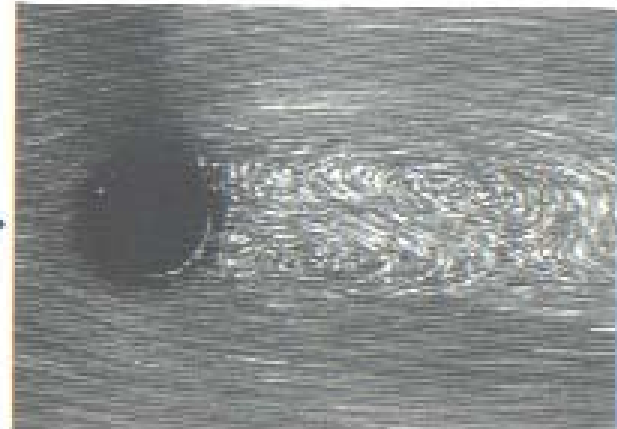
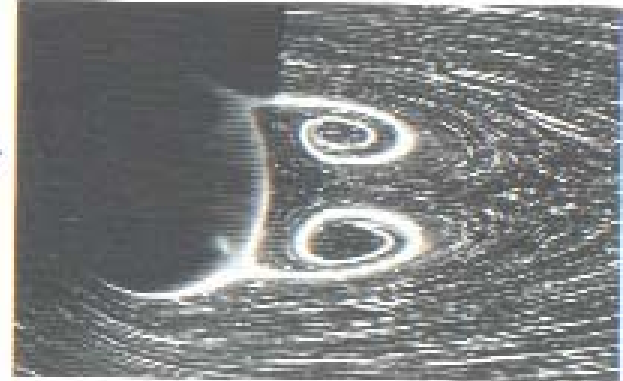
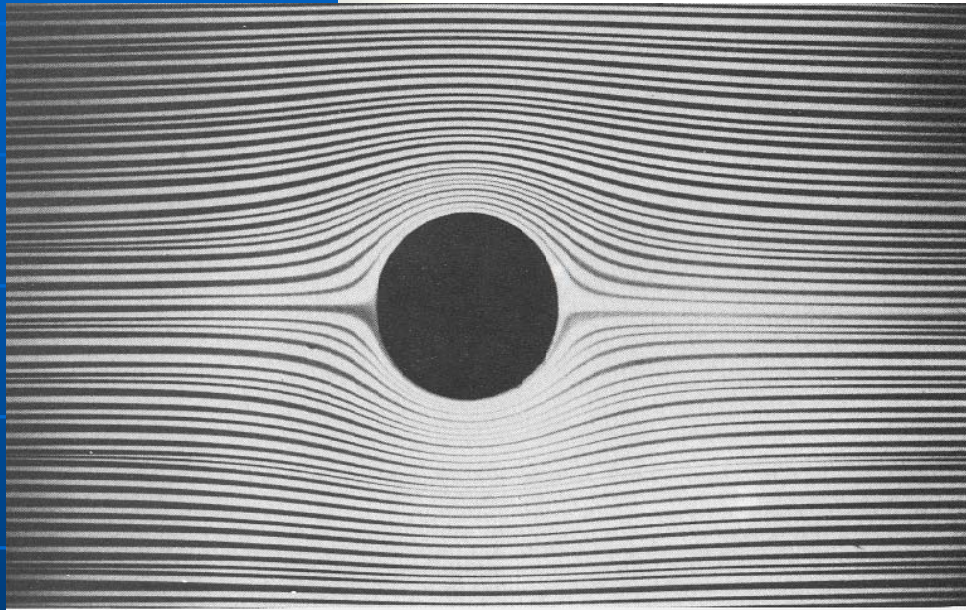
$$F_{fr} = q_{ref} \cdot c_e(z_e) \cdot c_{fr} \cdot A_{fr}$$

površina strukture u  
smjeru djelovanja  
vjetra

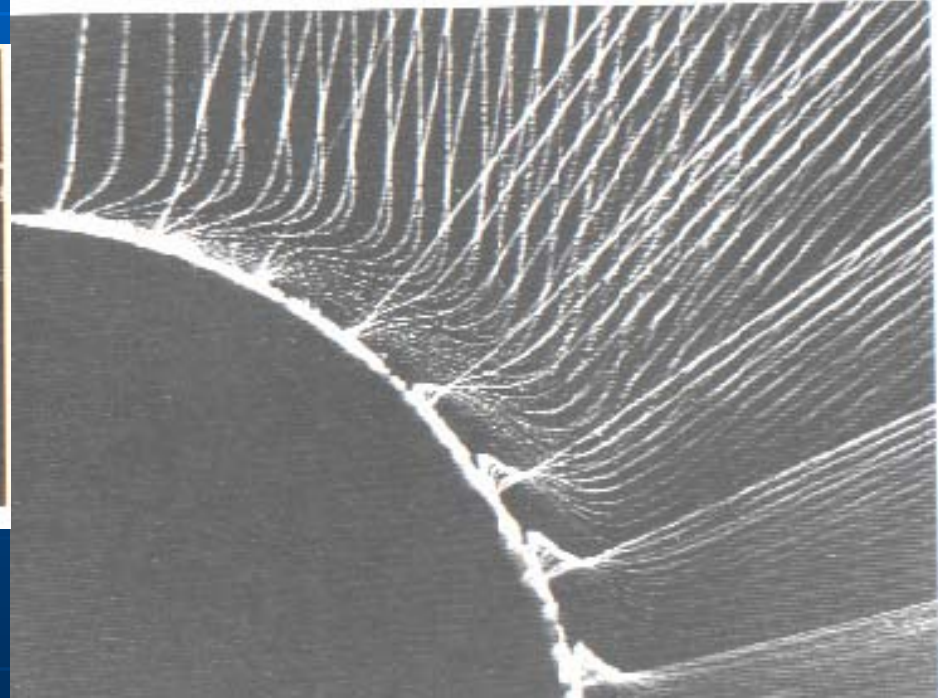
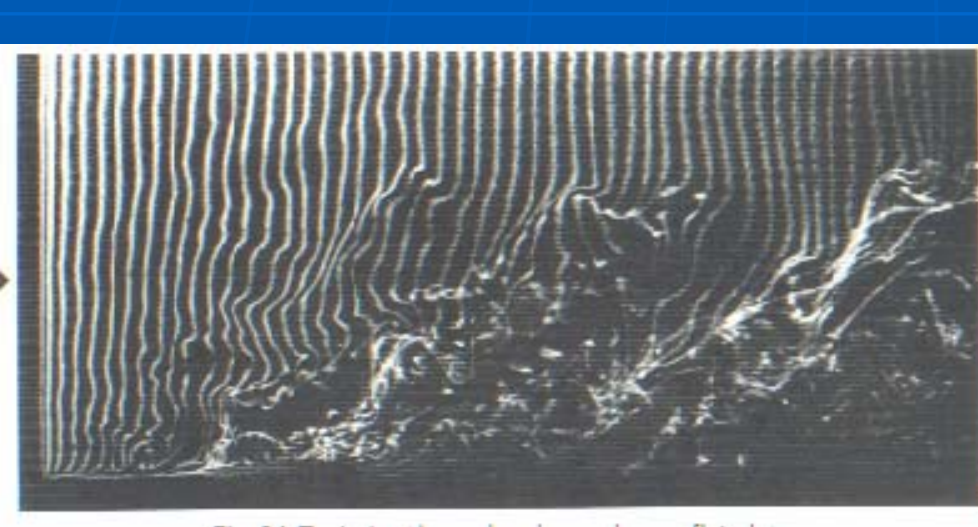
koeficijent okoline u kojem je uzeta u  
obzir konfiguracija terena, visina iznad tla  
i efekti turbulencije

koeficijent otpora trenja  
prirodnog strukturnog oblika

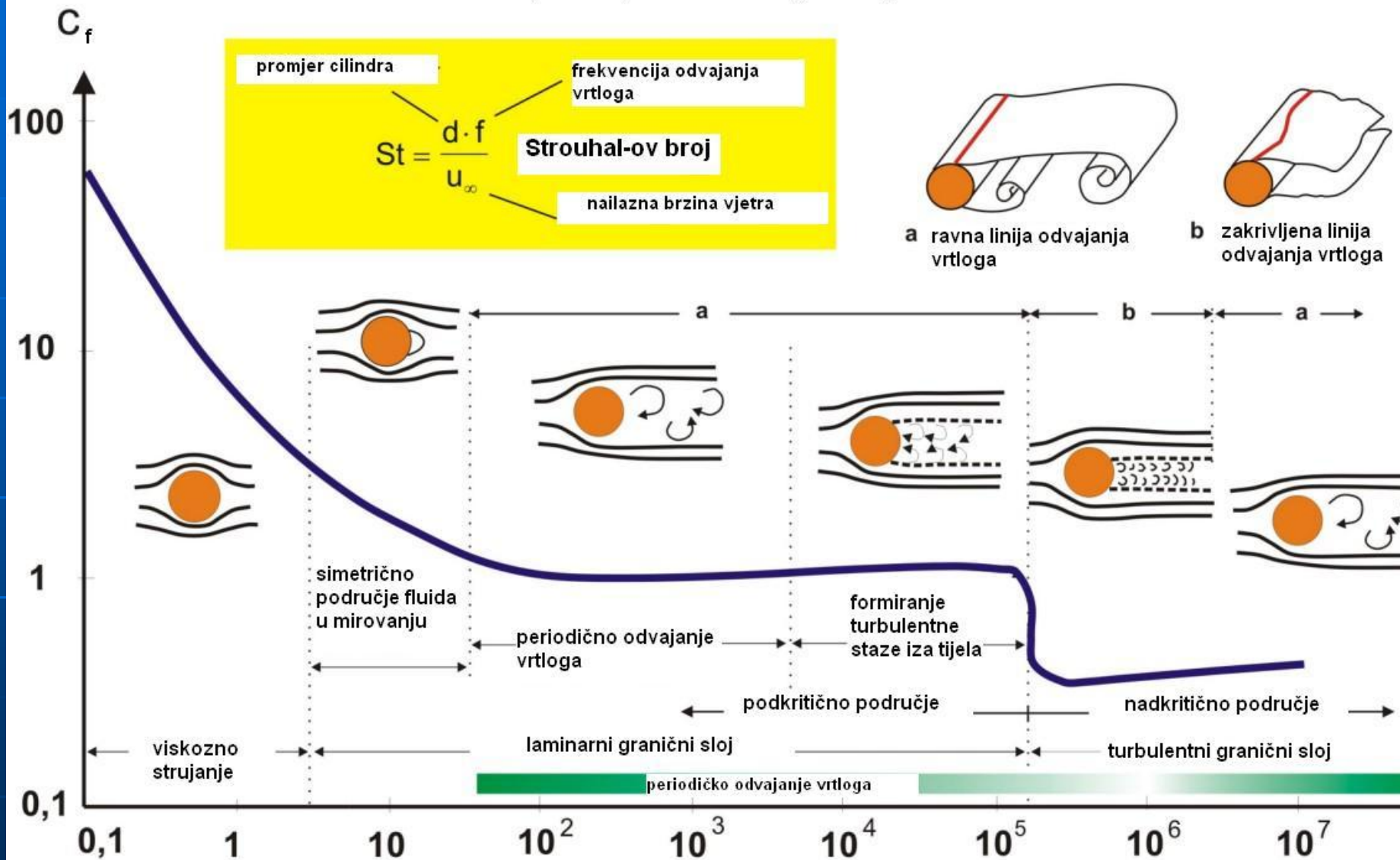
# Strujna slika u ovisnosti o Reynoldsovom broju



# Formiranje i odvajanje graničnog sloja

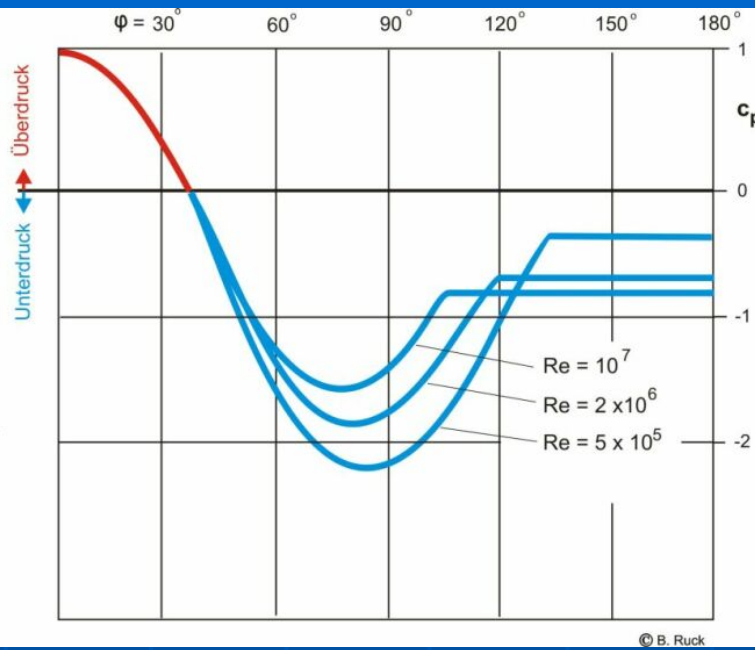
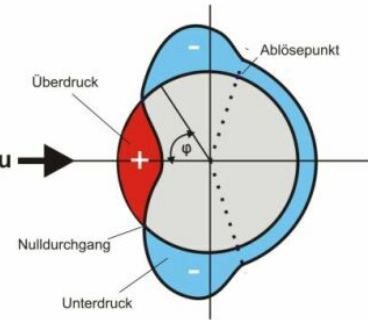


# Koeficijent otpora oblika glatkog cilindra

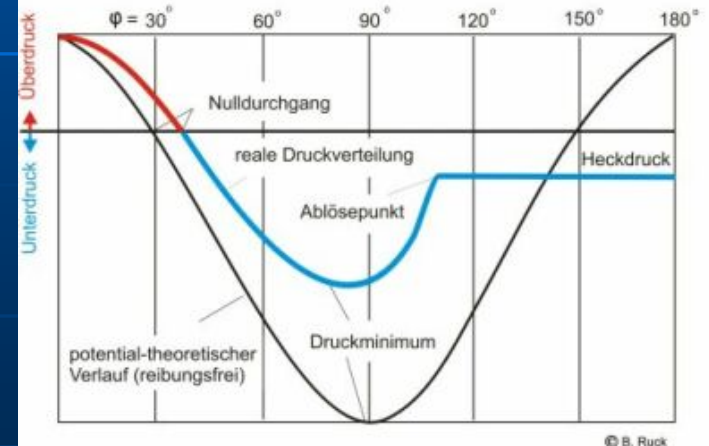
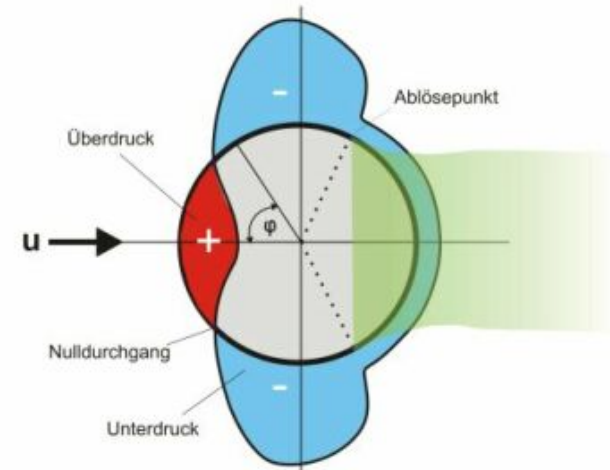


Jednoliko periodično odvajanje vrtloga pojavljuje se u područjima  $60 < Re < 5000$  i  $Re > 3 \times 10^6$

Abhängigkeit der Wanddruckbeiwerte beim (unendlich langen) Zylinder in Abhängigkeit von der Reynolds-Zahl



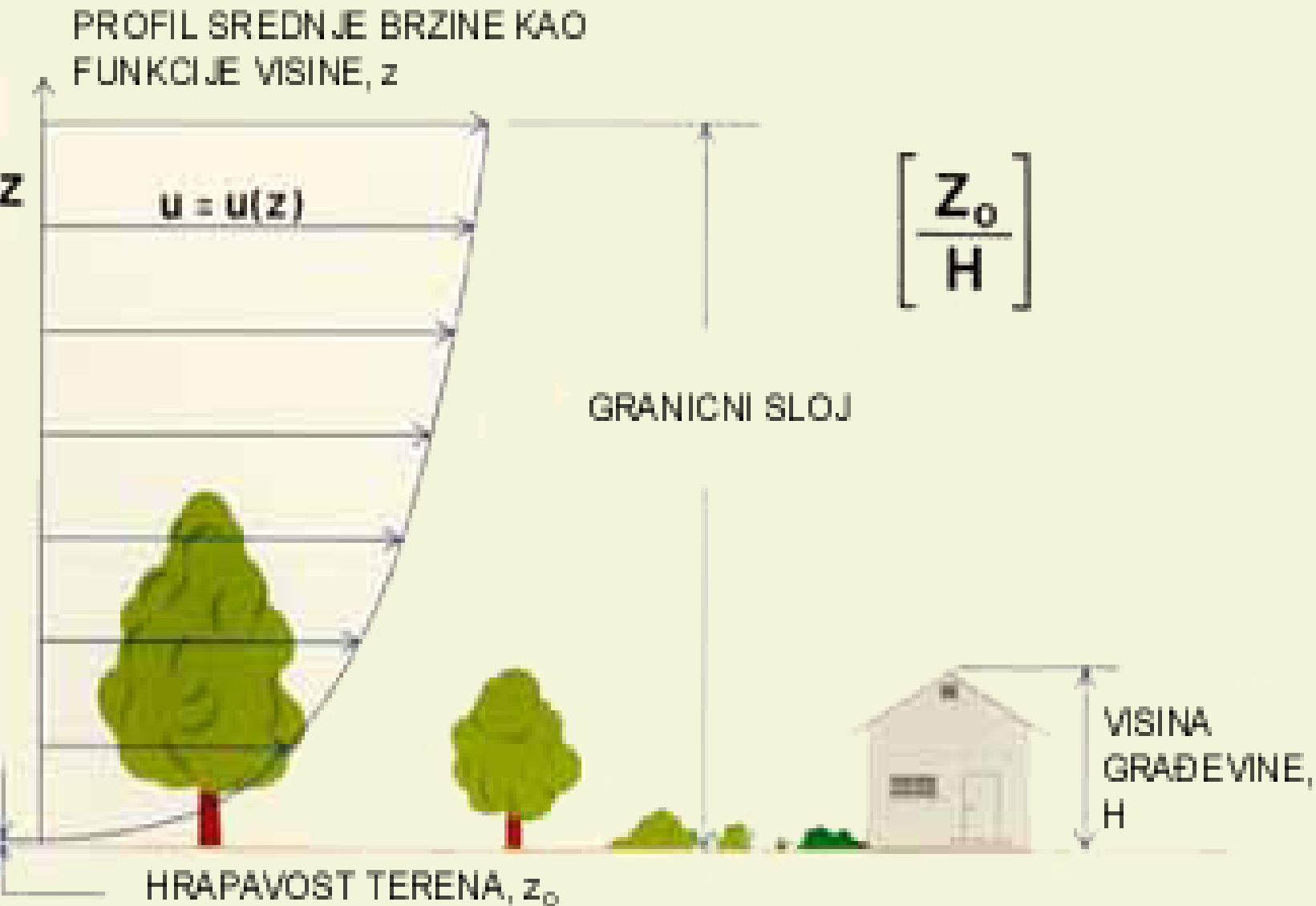
Zylinderumströmung (turbulente Grenzschicht)



Film: zrak-optjecanje oko kugle

Gjetvaj - hidraulika - Djelovanje vjetra

# Razvoj graničnog sloja



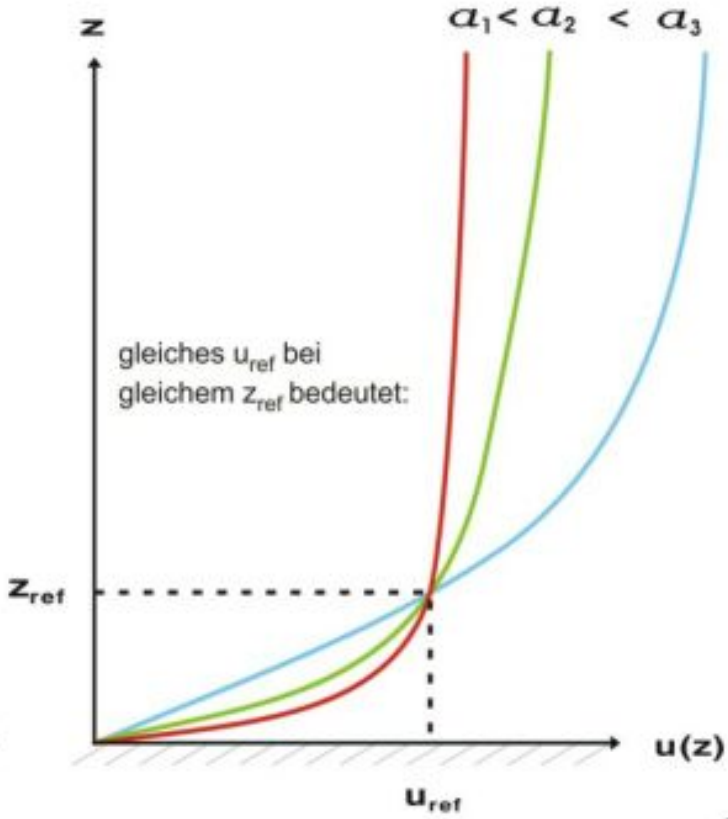
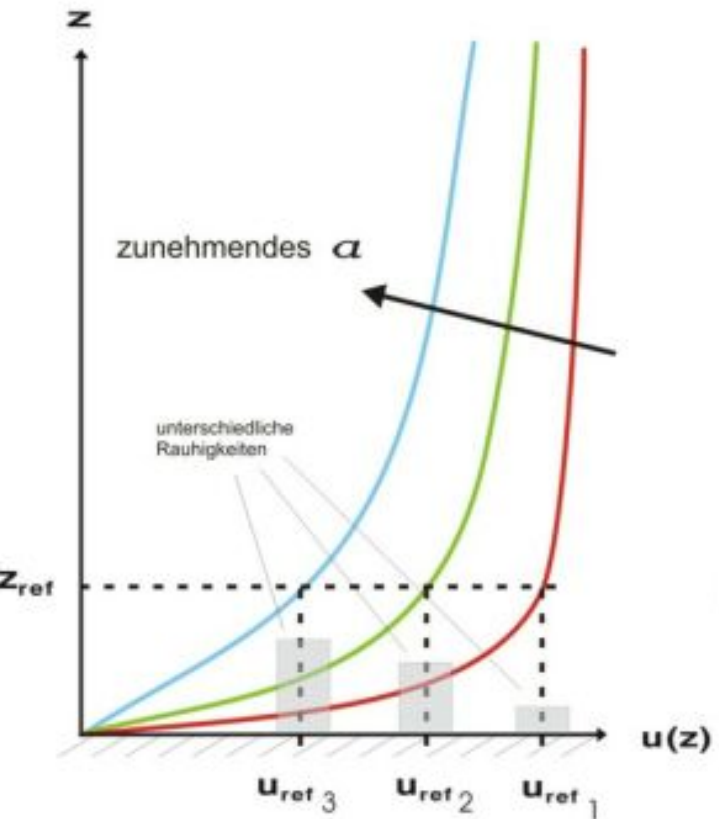
# Exponentialgesetz des Windgeschwindigkeitsverlaufes mit der Höhe

$$\frac{u(z)}{u_{ref}} = \left( \frac{z}{z_{ref}} \right)^{\alpha}$$

Typische Werte:

Oberflächentyp	$\alpha$
Innenstadtgebiet	0,4
Vorstadtgebiet	0,3
Landw. Flächen	0,25
Waldflächen	0,28
Über See	0,16

$$v_2 = v_1 \left( \frac{z_2}{z_1} \right)^{\alpha}$$





# Raspored brzine vjetra u graničnom sloju

$$v_M = v_{10} \left( \frac{z_M}{z_{10}} \right)^\alpha$$



Vrsta površine	$\alpha$
Gradsko područje	0,4
Predgrađa	0,3
Pošumljeno područje	0,28
Uobičajeni pejzaž (livade sa šumarcima)	0,25
More	0,16

- Djelovanje vjetra

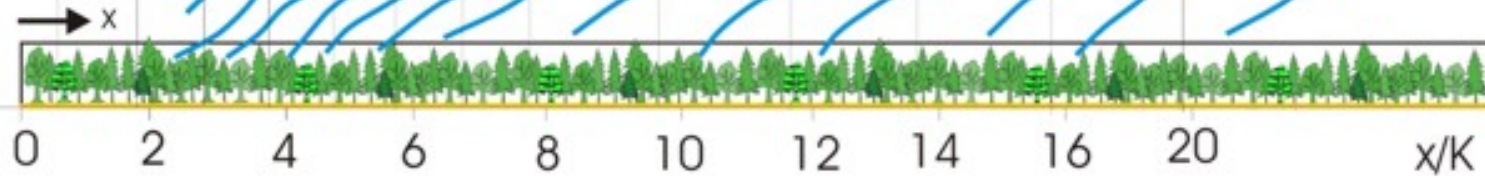
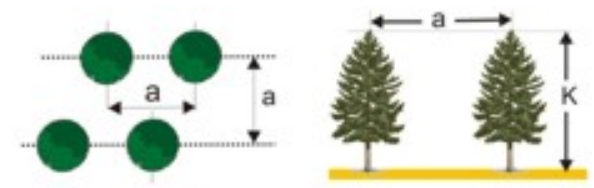
y/K

wind velocity profile shaping

10  
8  
6  
4  
2  
0

$u/u_{equ} = 1$

$a/K=0.5; K/\delta=0.1$

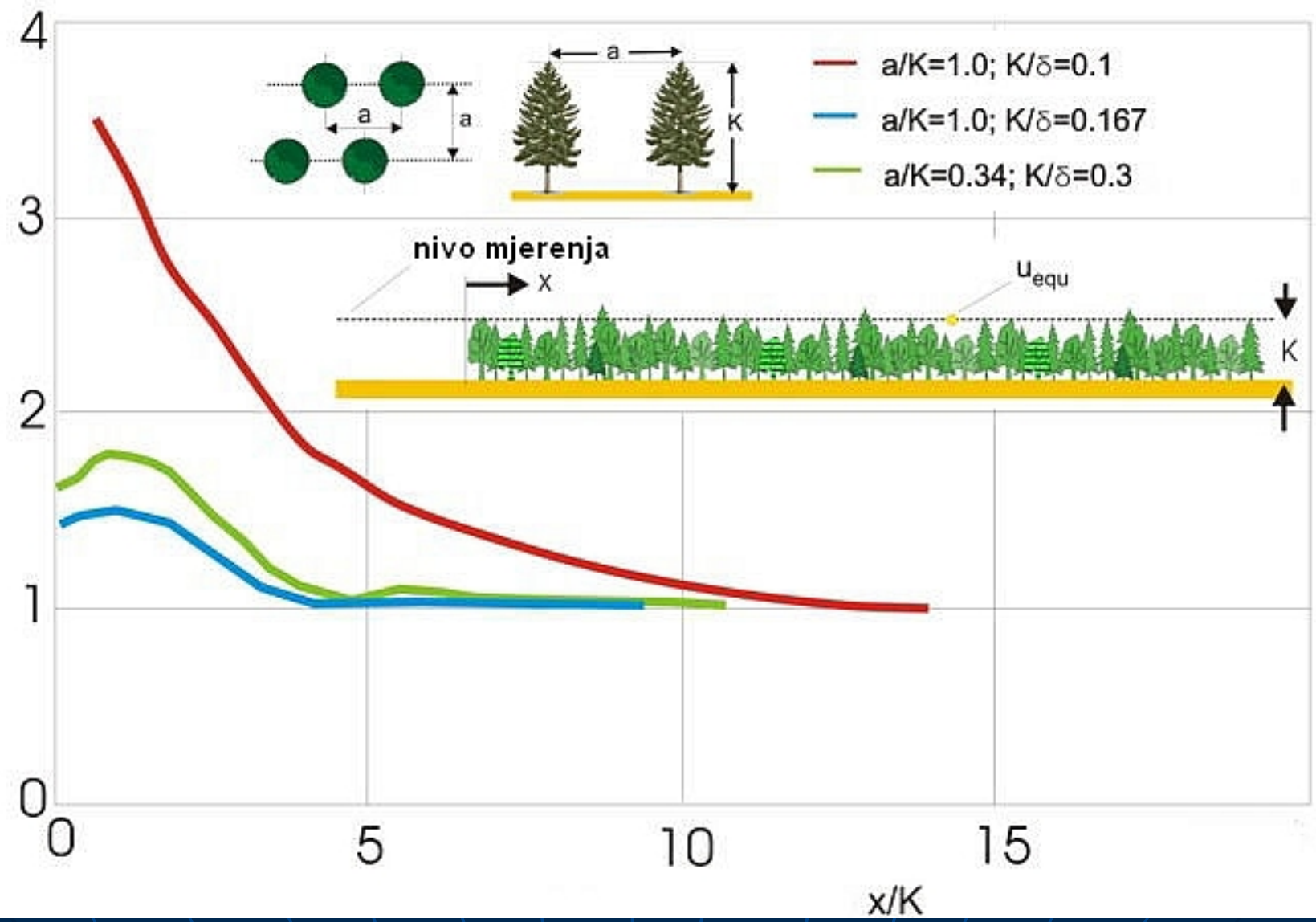


Mean wind velocity as a function of streamwise distance

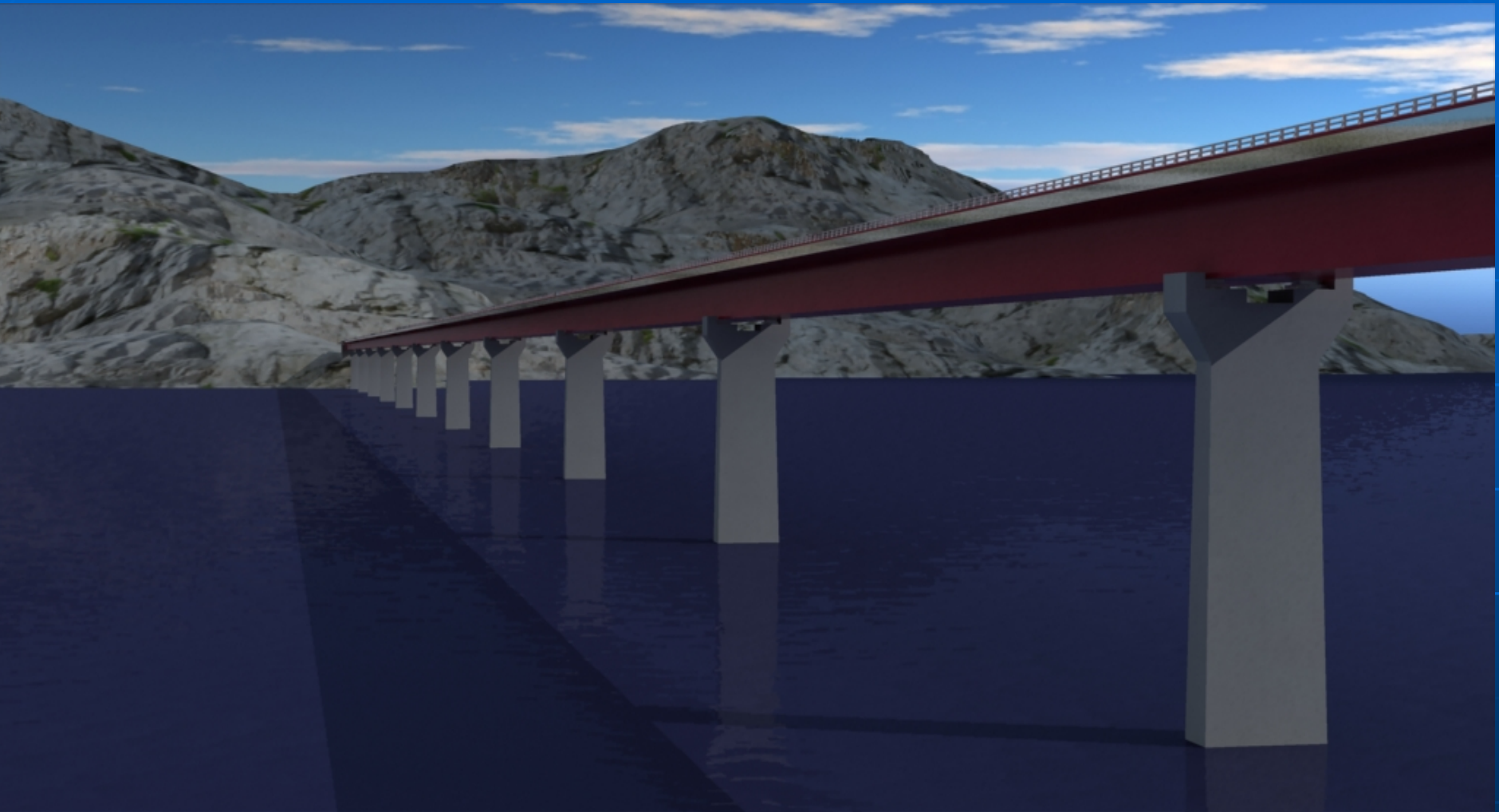
from: Ruck, B, Adams, E. 1991: 'Fluid mechanical effects of the pollutant transport to coniferous trees', Boundary-Layer Meteorology 56, 163-195

© B. Ruck

$u/u_{equ}$



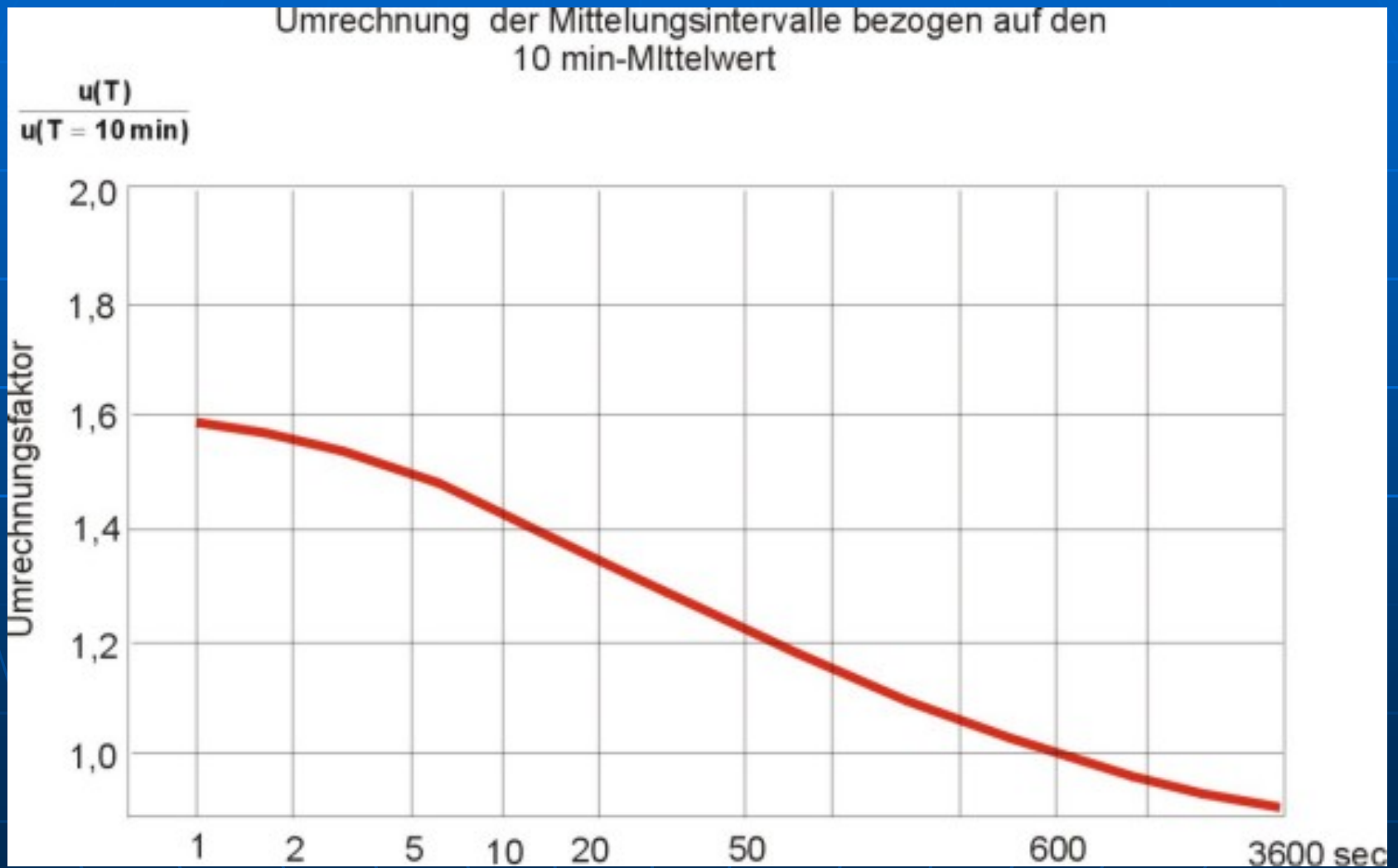
# Most na Pelješac



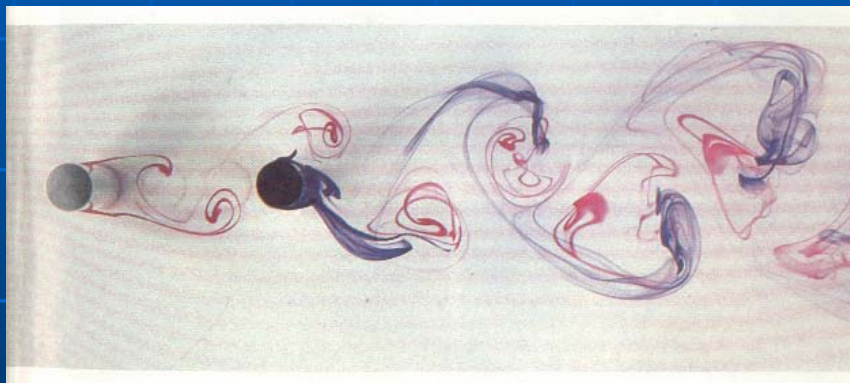
$$v_M = v_{10} \left( \frac{z_M}{z_{10}} \right)^\alpha = 25,3 \left( \frac{40}{10} \right)^{0,16} = 31,25 \text{ m/s}$$

nje vjetra

# Utjecaj osrednjavanja brzine vjetra



# Karmanovi vrtlozi



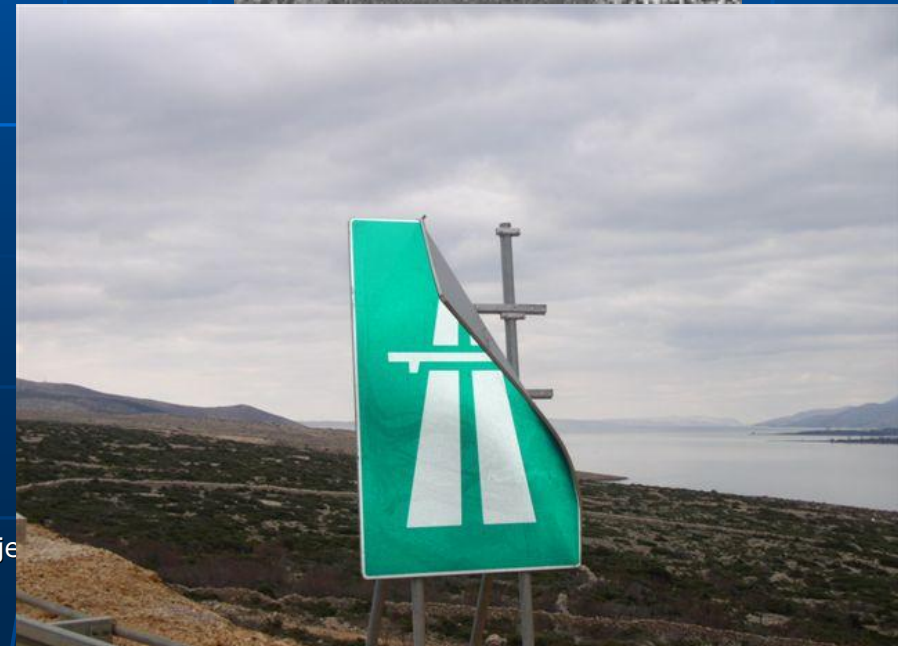
Film: vort.mpg

Film: most\_tacoma.avi

Film: most\_Dubrovnik1 i 2

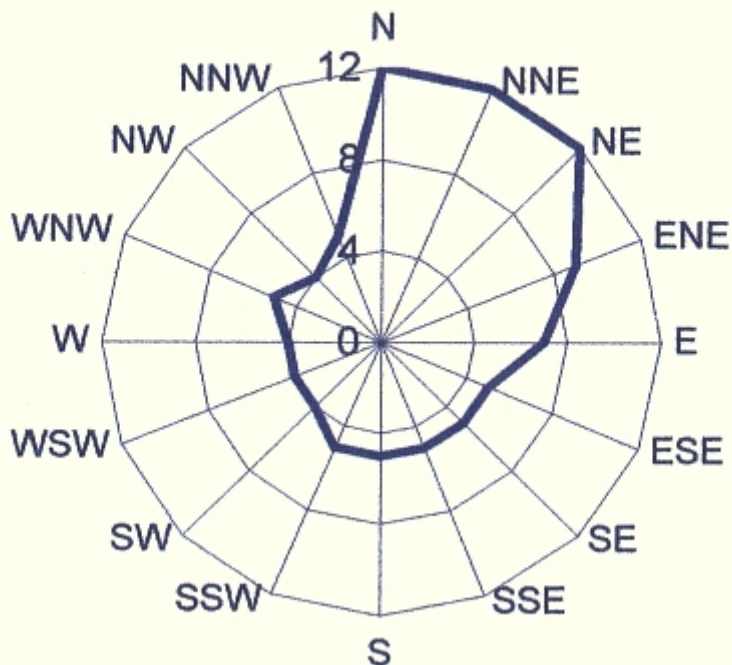
Film: Auto 1

# Bura



Gjetvaj - hidraulika - Dje

## Ruža najvećih srednjih satnih jačina vjetra u Bf (1998.)



## Beauforova ljestvica

Bf	Opisni naziv	Srednja brzina		
		čv	ms <sup>-1</sup>	kmh <sup>-1</sup>
0	Tišina	<1	0-0.2	<1
1	Lahor	1-3	0.3-1.5	1-5
2	Povjetarac	4-6	1.6-3.3	6-11
3	Slabi vjetar	7-10	3.4-5.4	12-19
4	Umjereni vjetar	11-16	5.5-7.9	20-28
5	Oštri vjetar	17-21	8.0-10.7	29-38
6	Jaki vjetar	22-27	10.8-13.8	39-49
7	Žestoki vjetar	28-33	13.9-17.1	50-61
8	Olujni vjetar	34-40	17.2-20.7	62-74
9	Jaki olujni vjetar	41-47	20.8-24.4	75-88
10	Oluja	48-55	24.5-28.4	89-102
11	Žestoka oluja	56-63	28.5-32.6	103-117
12	Orkan	>64	> 32.7	>118

Kategorija	1	2	3	4	5
Tlak u središtu ciklone (hPa)	> 980	965-979	945-964	920-944	< 920
Brzina vjetra (m/sec)	33-42	43-49	50-58	59-69	> 69
Brzina vjetra (km/sat)	119-153	154-177	178-209	210-249	> 249
Visina valova (m)	do 1,5	do 2,4	do 3,7	do 5,5	> 5,5
Šteta	mala	umjerenjena	velika	vrlo velika	katastrofalna

Gjetvaj - hidraulika - Djelovanje vjetra

## Saffir-Simpsonova ljestvica ciklona

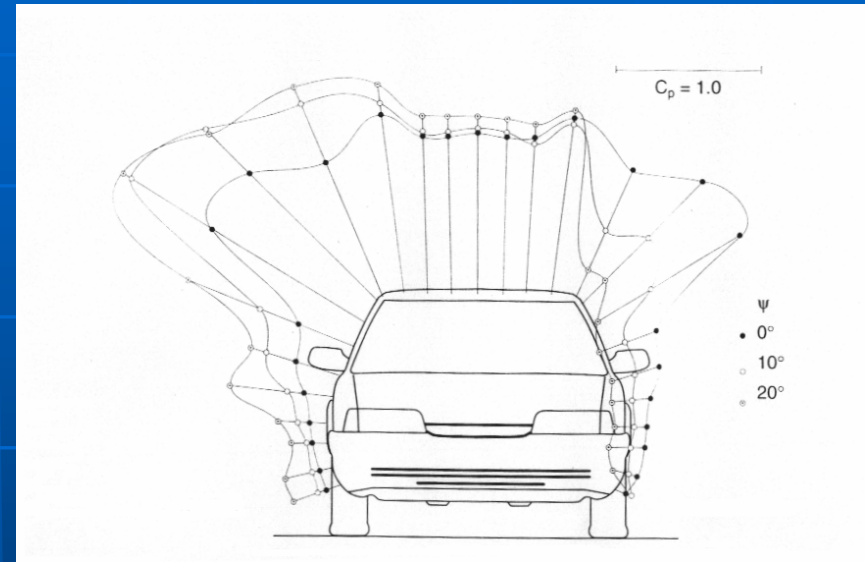
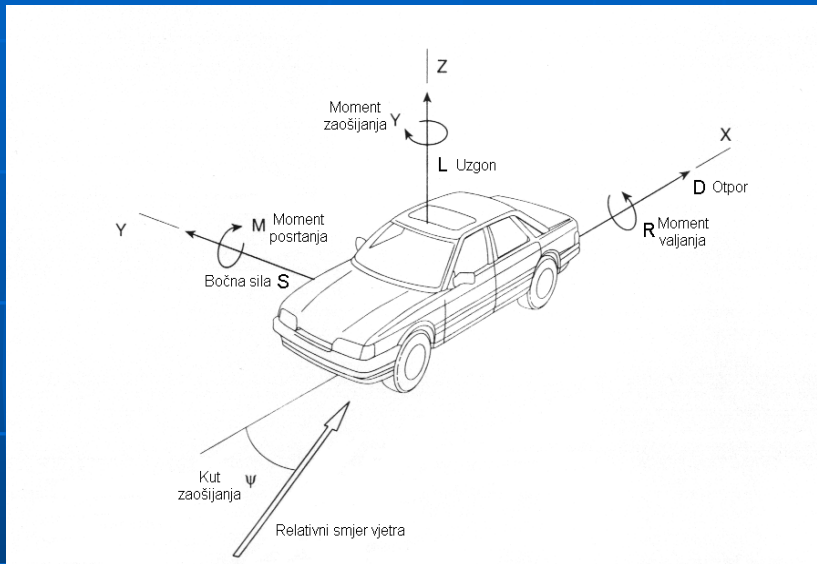




**Film: Vjetar na mostu 1**  
**Film: Vjetar na mostu 2**

Vjetar - hidraulika - Djelovanje vjetra

# Sile i momenti na vozilo usljed djelovanja vjetra



Uvjet prevrtanja

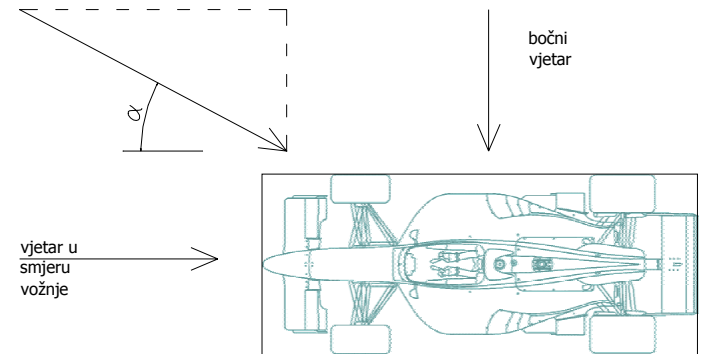
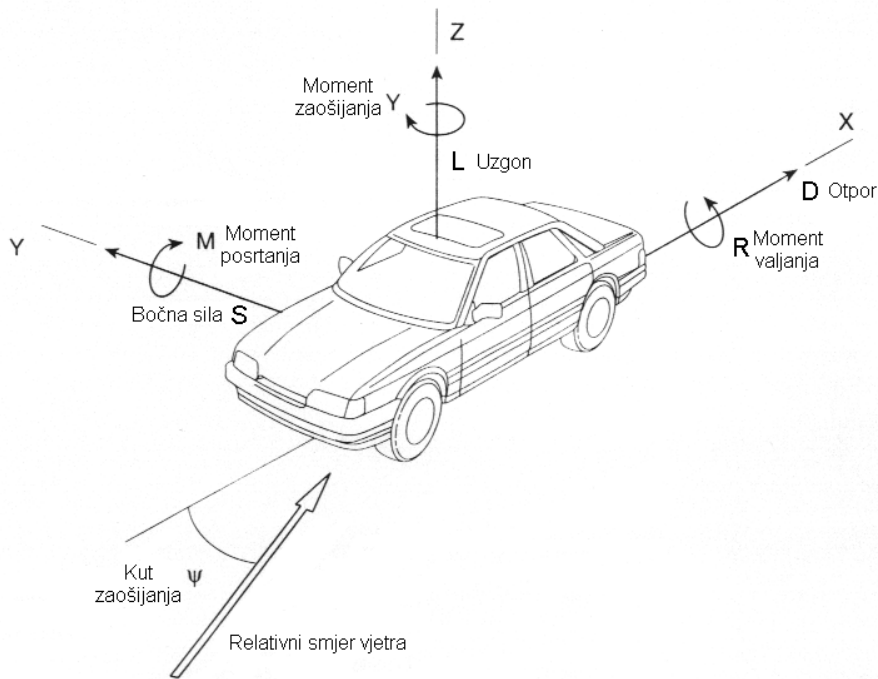
$$\frac{\rho}{2} v_r^2 A \left( C_L \frac{t}{2} + C_R l \right) \geq W \frac{t}{2}$$

Uvjet zaošijanja

$$v_w = v_r \sin \psi = \sqrt{\frac{2W}{A \rho \left( C_L + 2 \frac{l}{t} C_R \right)}} \sin \psi$$

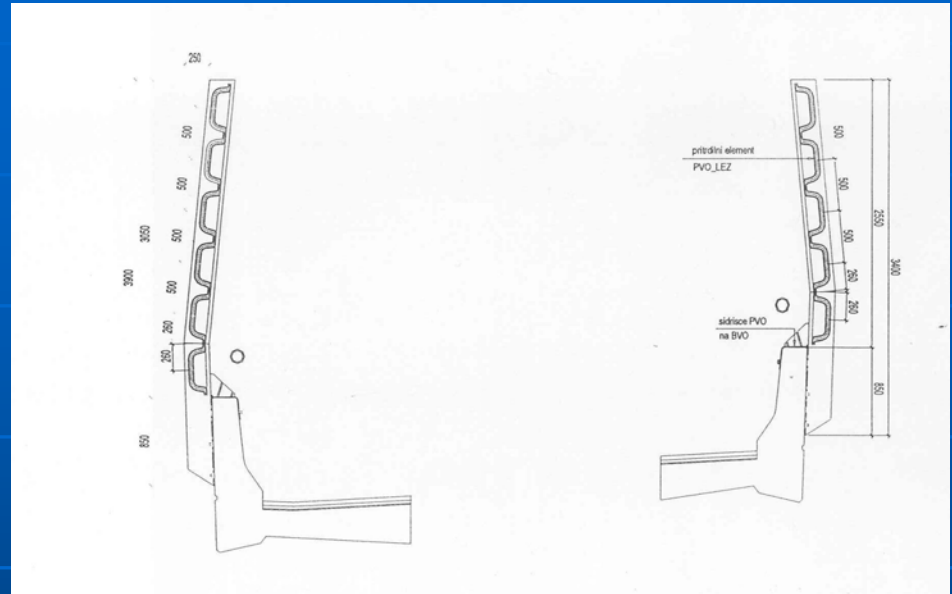
Djelovanje vjetra

# Homogenizirane brzine

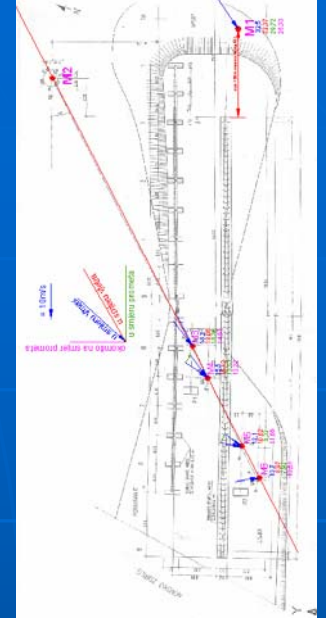


$$v_{HOM} = c_B \cdot (0,5 \cdot v_{MAX} + 0,5 \cdot v_{MAX} \cdot \sin \alpha) \leq 30m / s$$

# Vjetrobran (propusni)



# Vjetrobran (segmentni)



Gjetvaj - hidraulika - Djelovanje vjetra

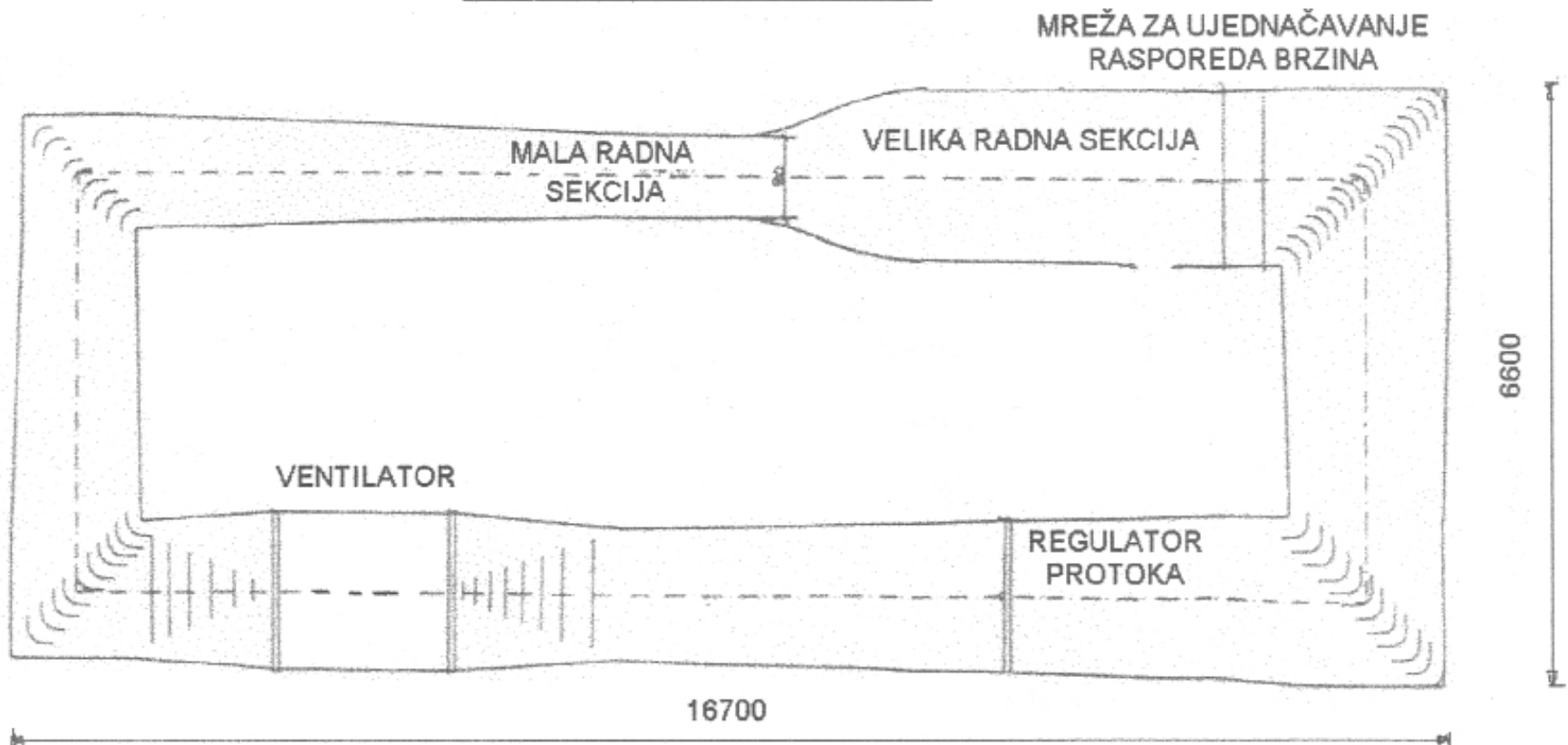
# Vjetrobran (nasip)

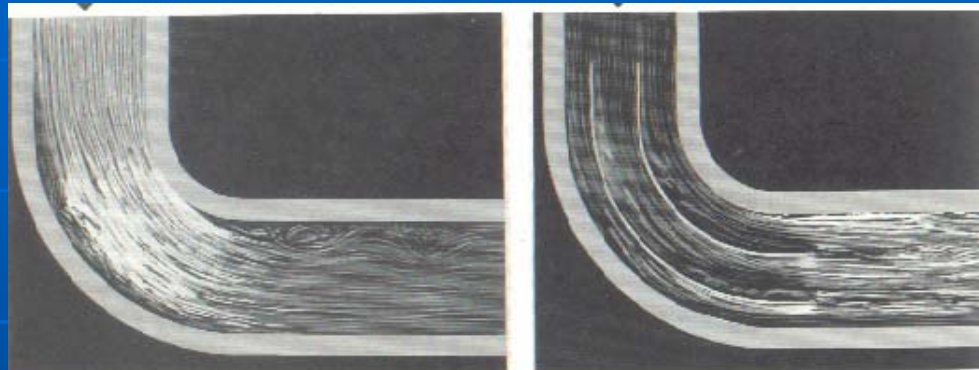


# Ispitivanja u zračnom tunelu

Hidrotehničkog laboratorija Građevinskog fakulteta u Zagrebu.

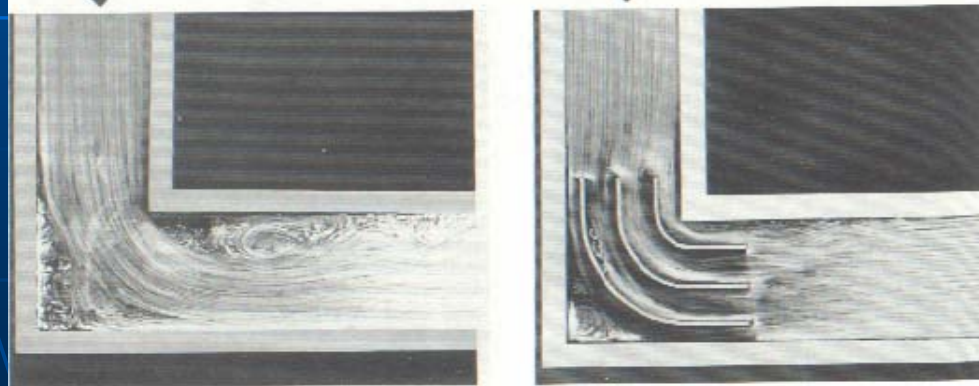
## TLOCRT ZRAČNOG TUNELA





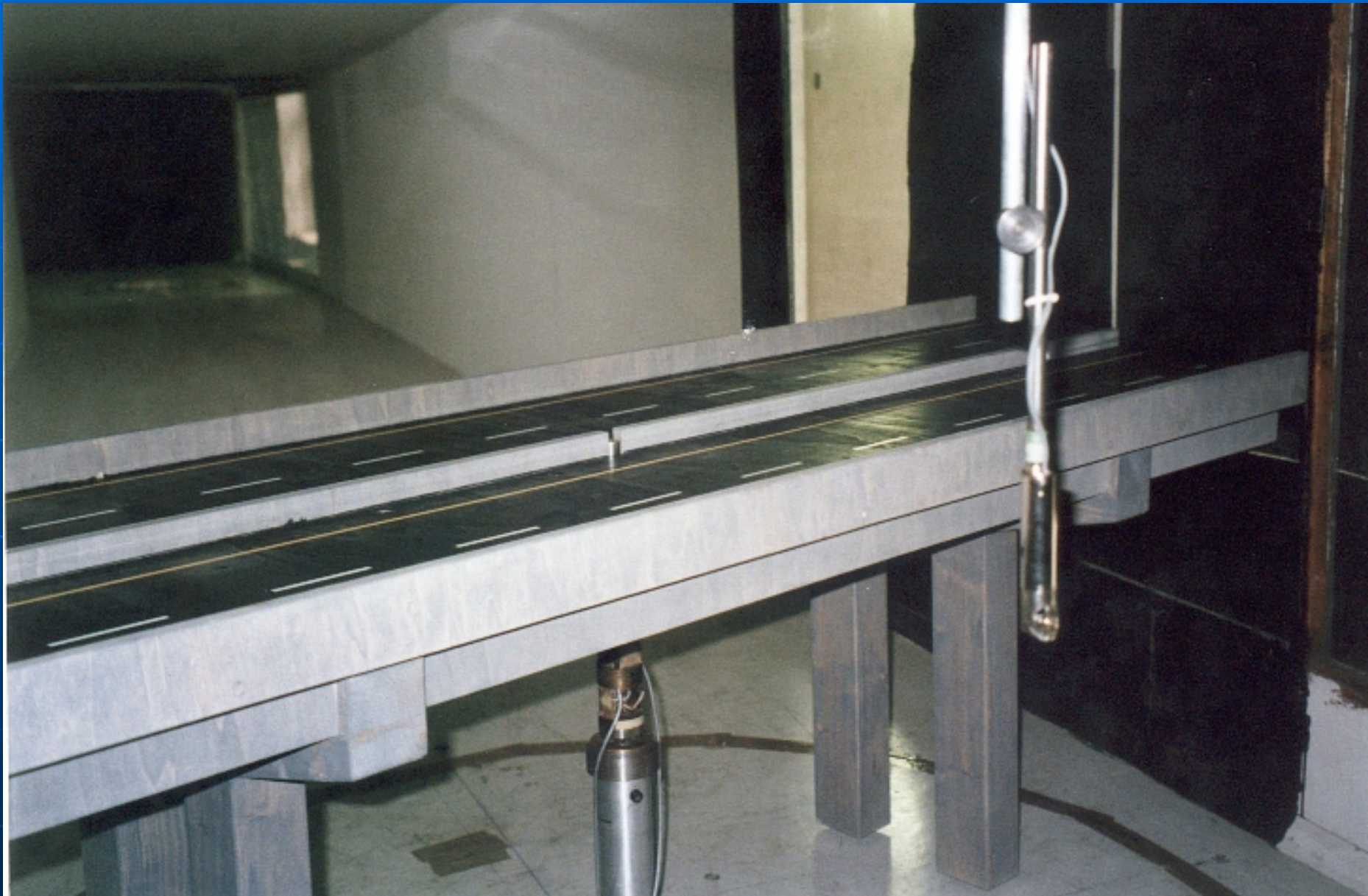
Figs. 108 and 109. Flow through a turning passage with and without guide vanes (water, velocity = 10 cm/s, passage width = 20 mm,  $Re = 2 \times 10^3$ , surface tracer method)

Figs. 110 and 111. Passages connected in right angle with and without guide vanes (water, velocity = 10 cm/s, passage width = 20 mm,  $Re = 2 \times 10^3$ , surface tracer method)





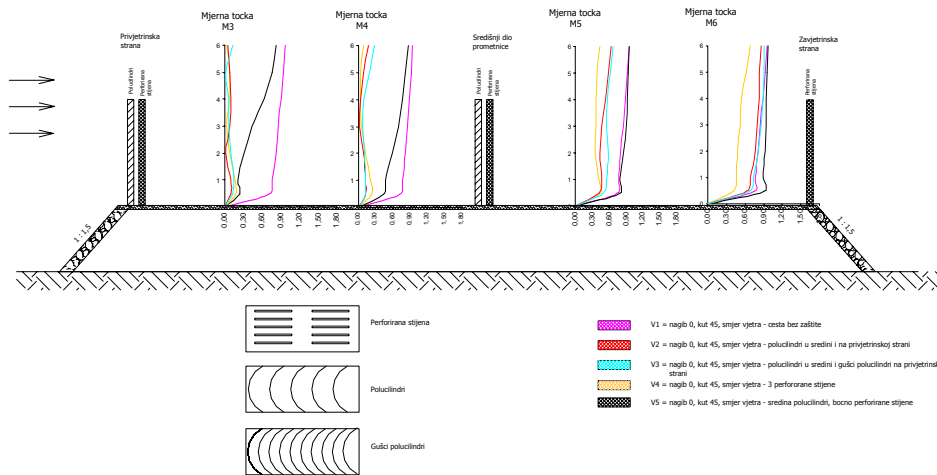
# Model mosta u zračnom tunelu



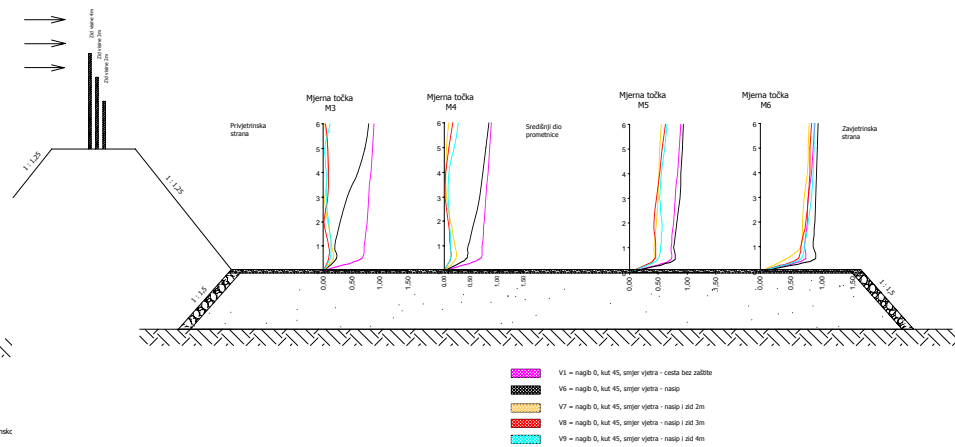




Relativna brzina u smjeru vjetra



Rezultati u smjeru vjetra



- Filmovi:

vort.mpeg

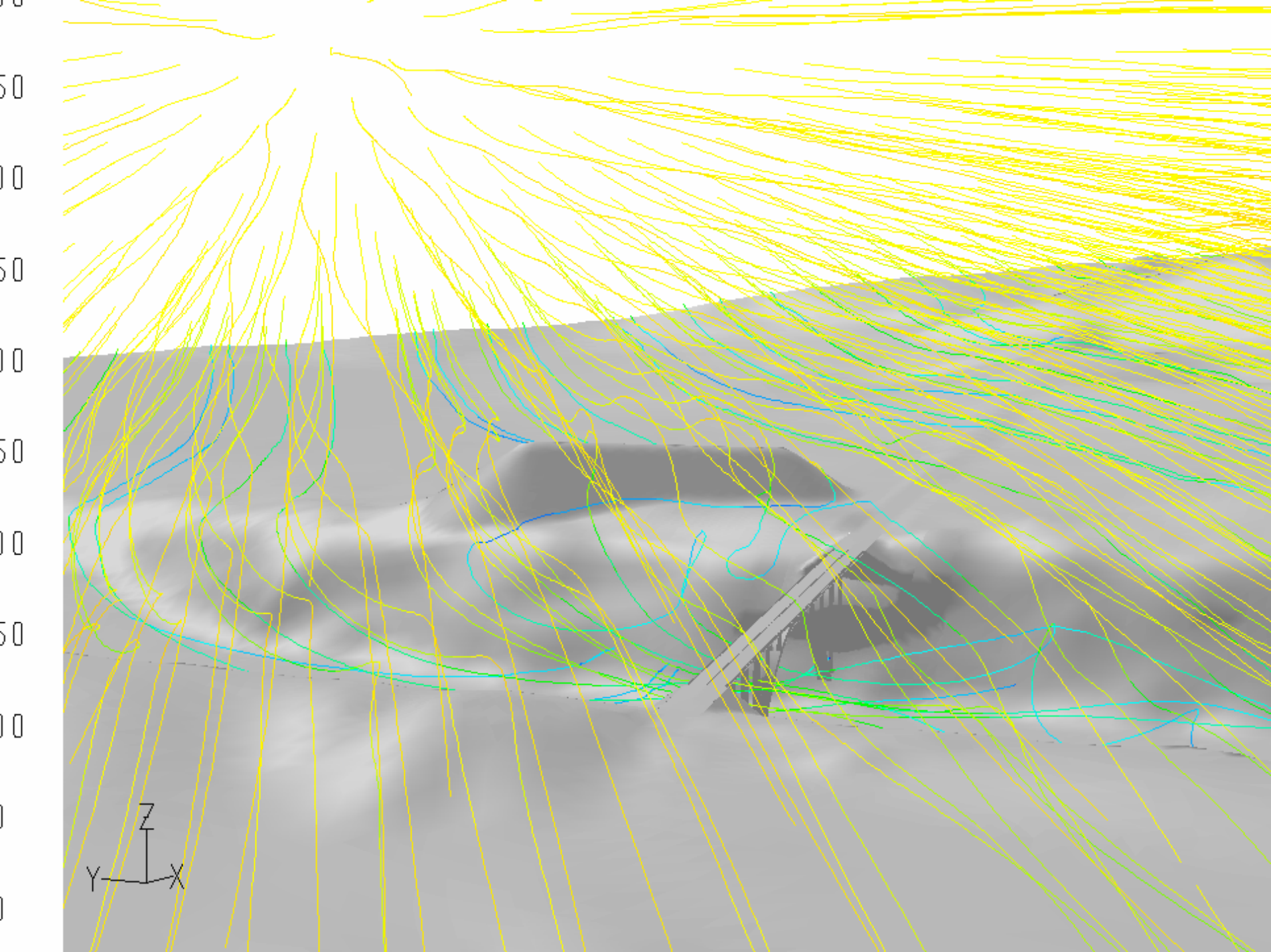
win2fire.mpg

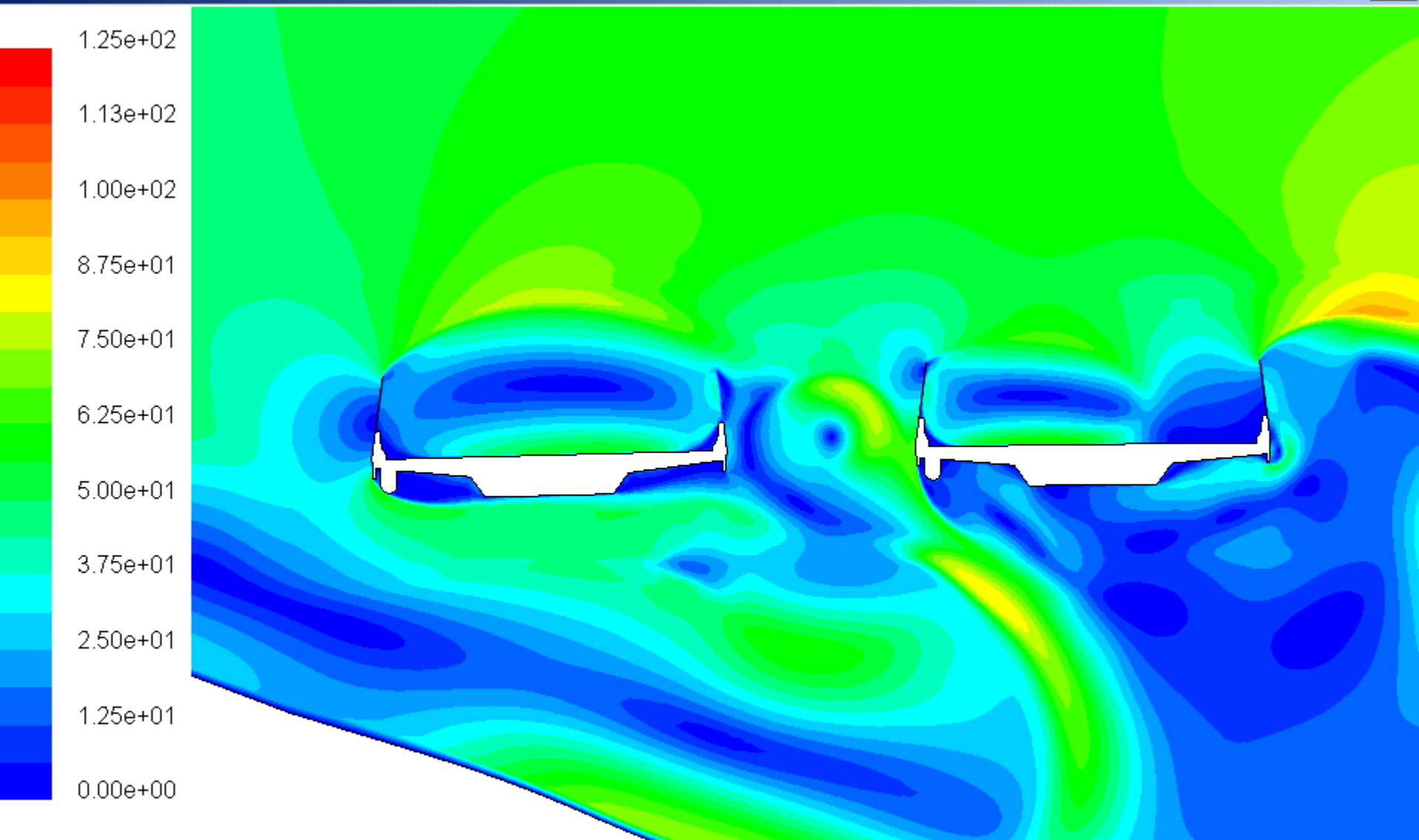
auto1.mpeg (možda negdje drugdje")

auto2.mpeg





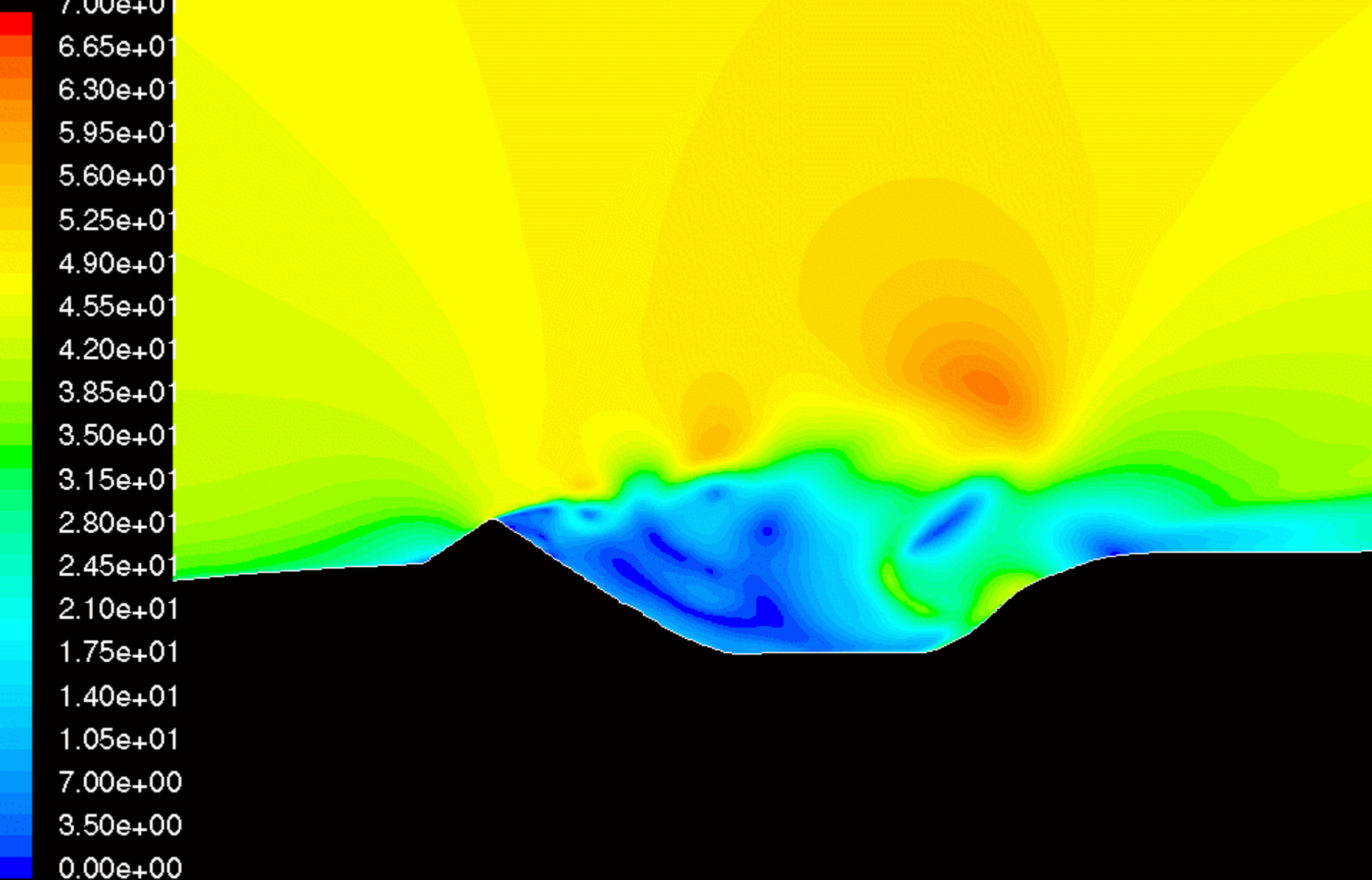




Contour brzine (m/s) (Time=4.0000e-03)

Viadukt Baricevici



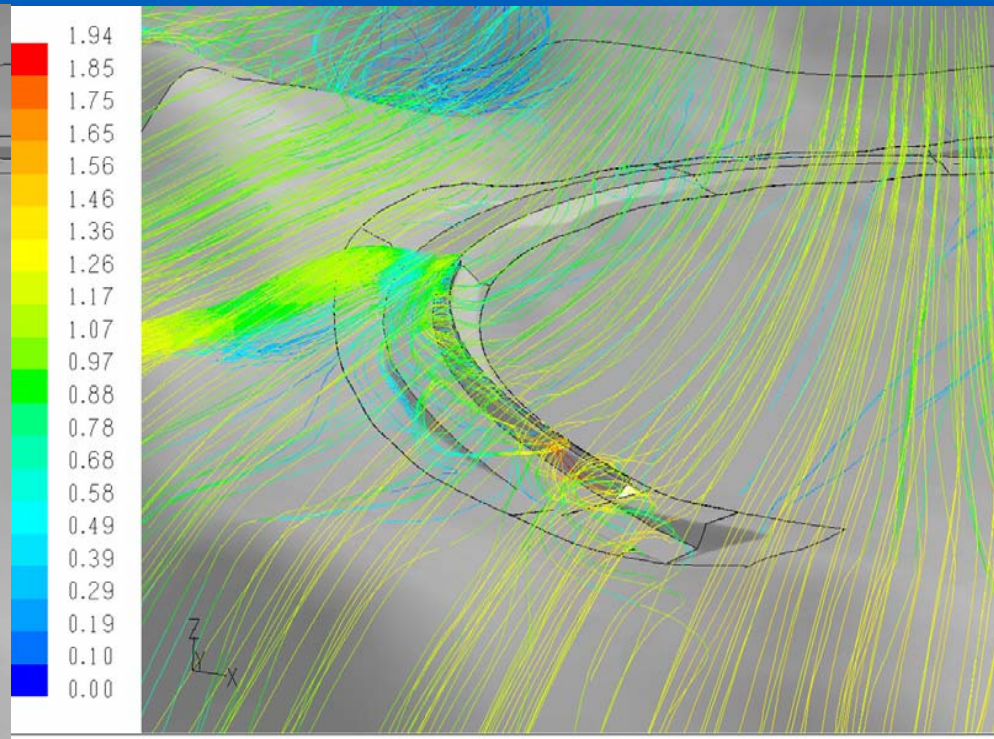
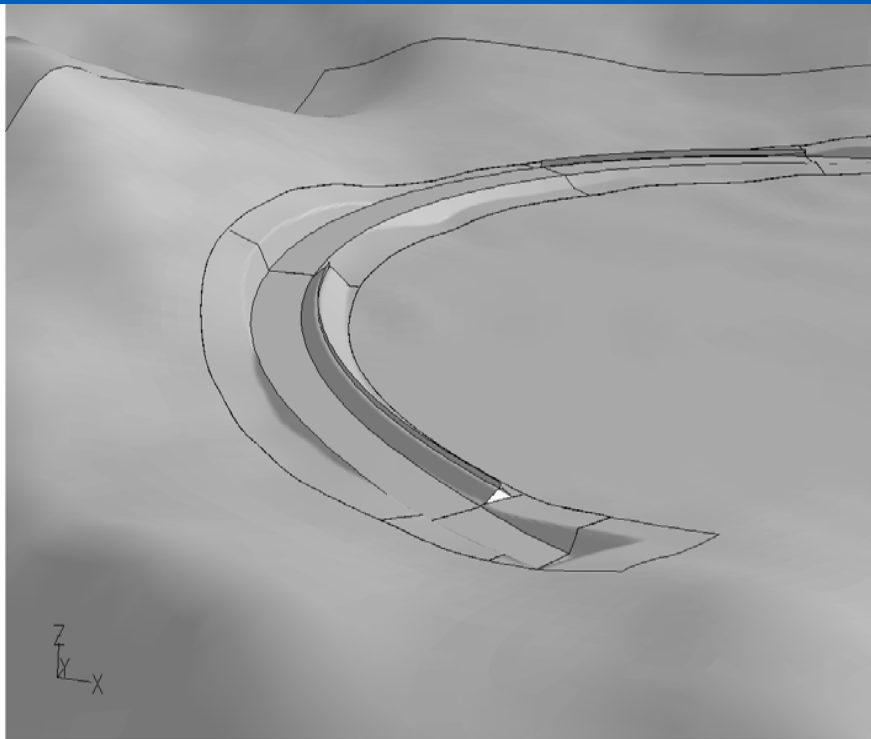


Contours of Velocity Magnitude (m/s) (Time=2.8800e+00)

Dec 15, 200

FLUENT 6.0 (2d, segregated, BSM, unsteady)

# Zaštita krivine Vučipolje skraćenim nasipom



Jun 23, 2004  
FLUENT 6.1 (3d, segregated, rngke)

Path Lines Colored by u\_norm

Jun 21, 2004  
FLUENT 6.1 (3d, segregated, rngke)

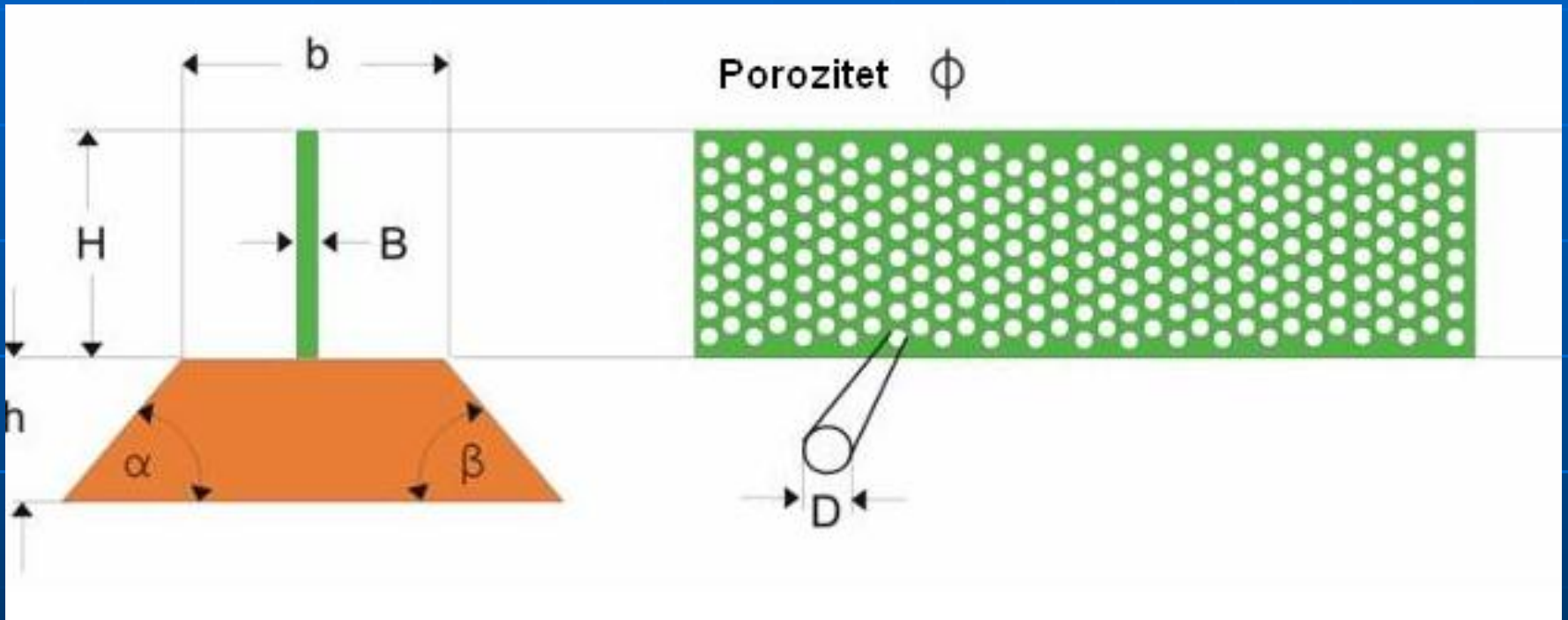
# Probno polje kod Maslenice



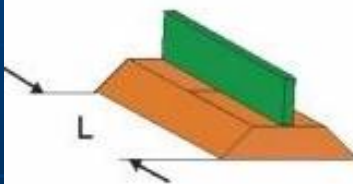
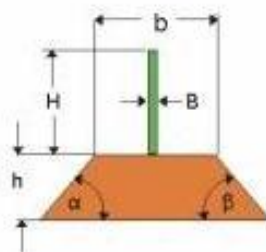
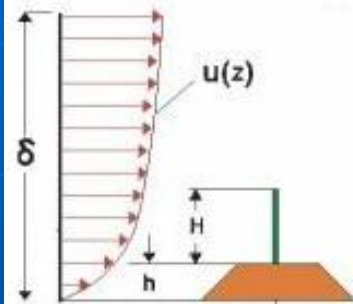
Na riječkoj strani Masleničkog mosta 23.XII 04  $v = 42,7 \text{ m/s}$

Na probnom polju 23.XII 04  $v = 24,2 \text{ m/s} < v_{\text{dop}} = 30 \text{ m/s}$

Gjetvaj - hidraulika Djelovanje vjetra



# Učinkovitost vjetrobrana

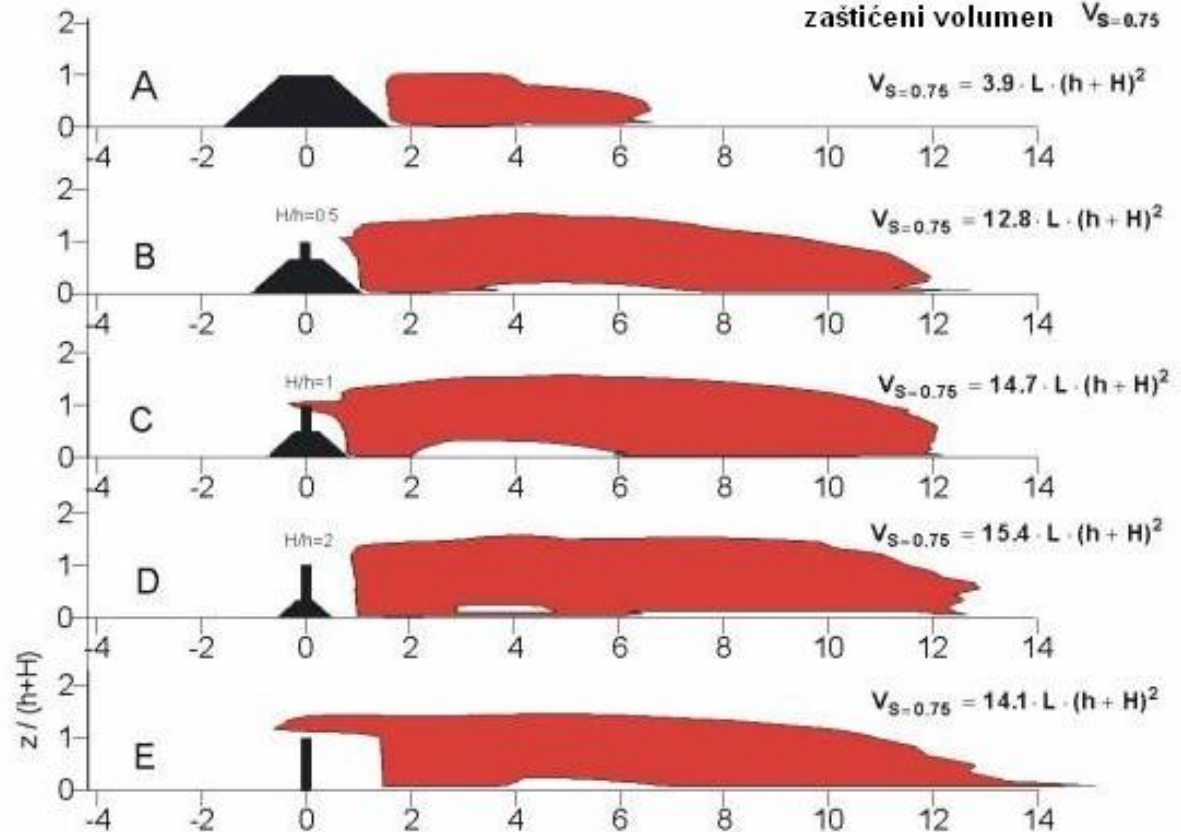


$\alpha = \beta = 40^\circ \text{ Grad}$   
 $\phi = 0\%$   
 $B_{\text{exp}} = 6 \text{ mm}; b/h = 1; \delta_{\text{sin}} / (h+H) = 20$   
 $n = 0.22$

hier:  $S_u(x,z) = \left[1 - \frac{[u_2(x,z)]^2}{[u_1(z)]^2}\right] = 0.75$

$\phi = 0\%$

zaštićeni volumen  $V_{S=0.75}$



## ZAŠTIĆENI VOLUMEN

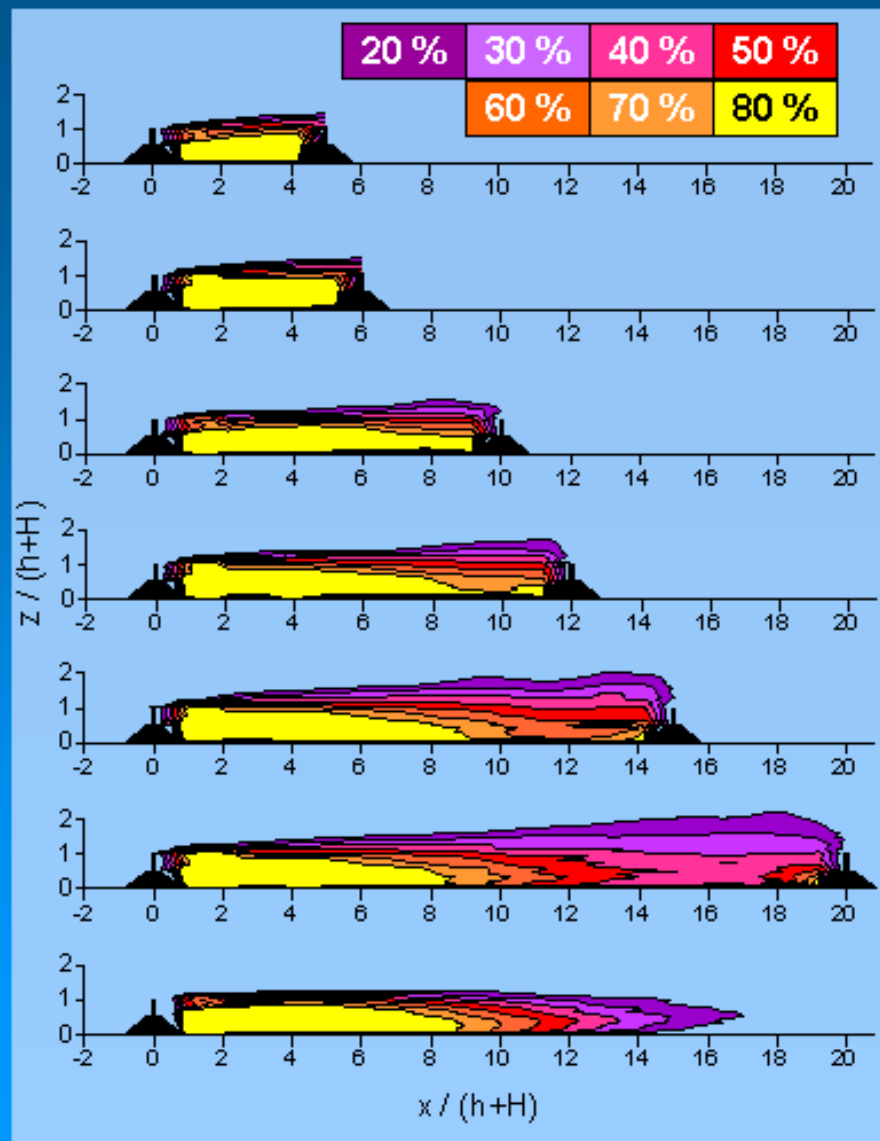
 $V_{su}$ 

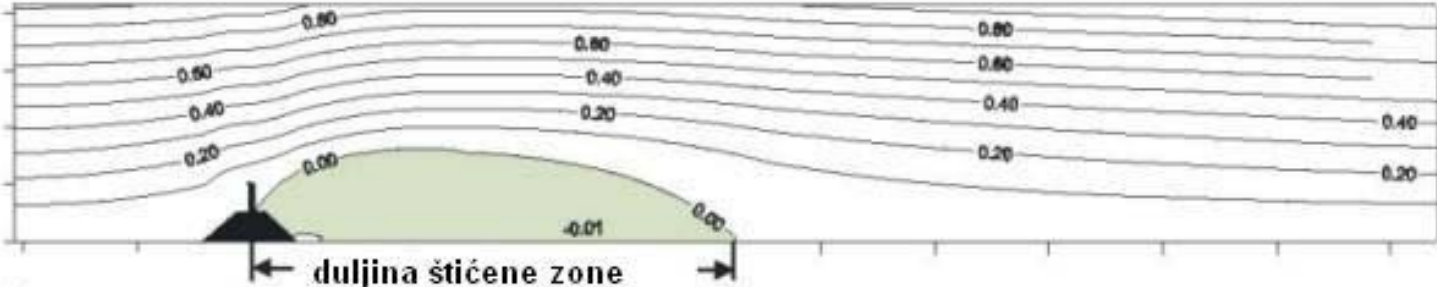
( $\alpha = 40^\circ$ ,  $\Phi = 52\%$ ,  $h/H = 1$ )

$$S_u(x, z) = 1 - \frac{u_2(x, z)^2}{u_1(z)^2}$$

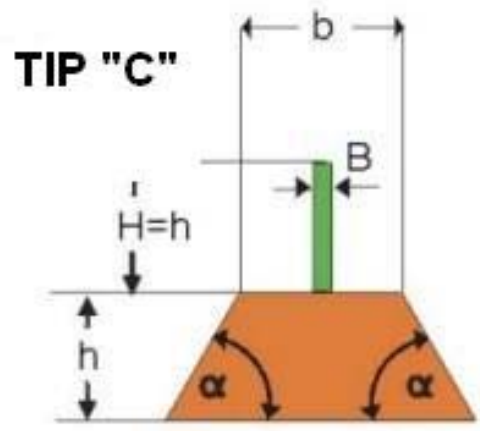
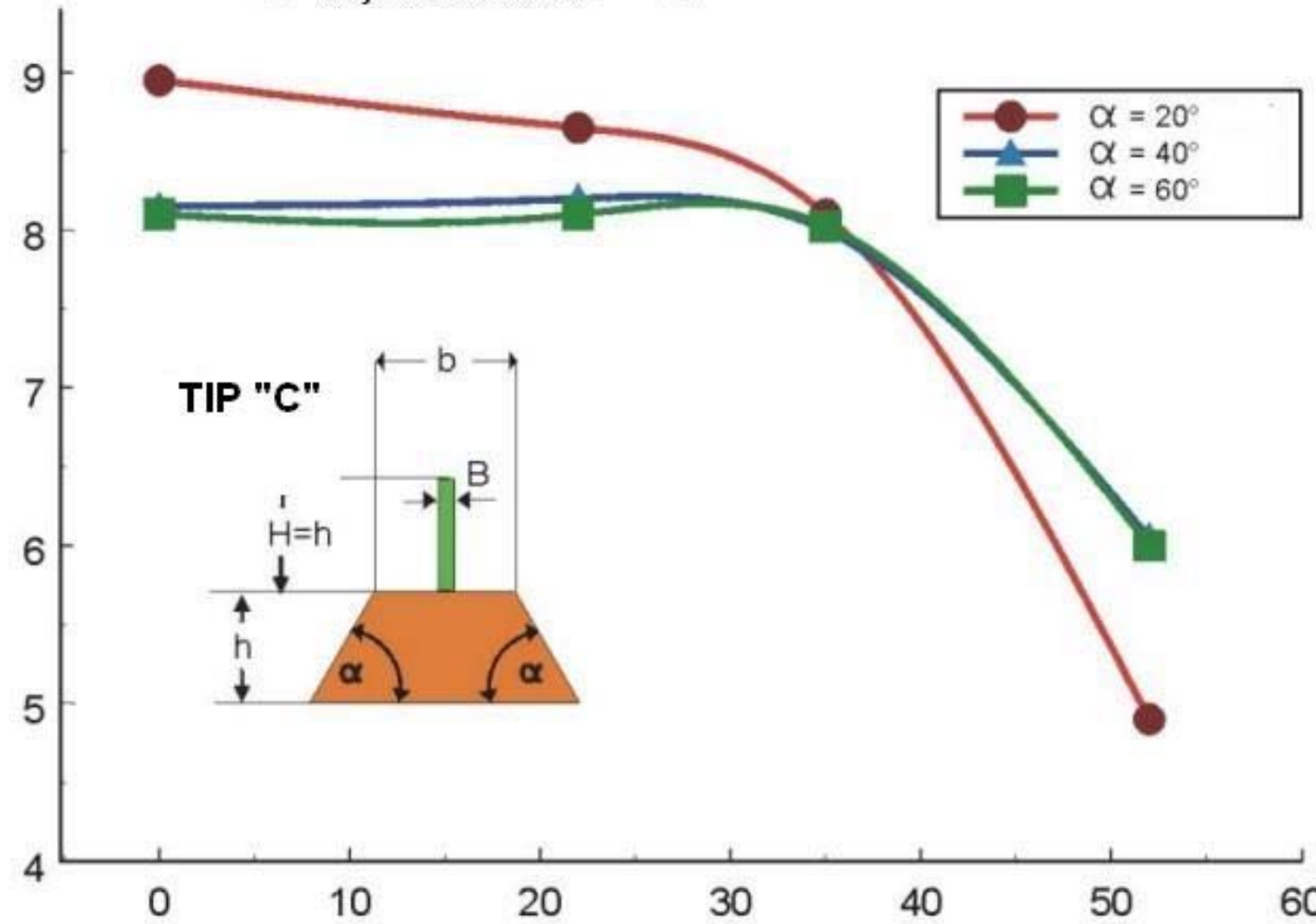
$S_u > 0$ : smanjenje utjecaja vjetra

$S_u < 0$ : povećanje utjecaja vjetra





$X_{dim} = X_R / (h+H)$



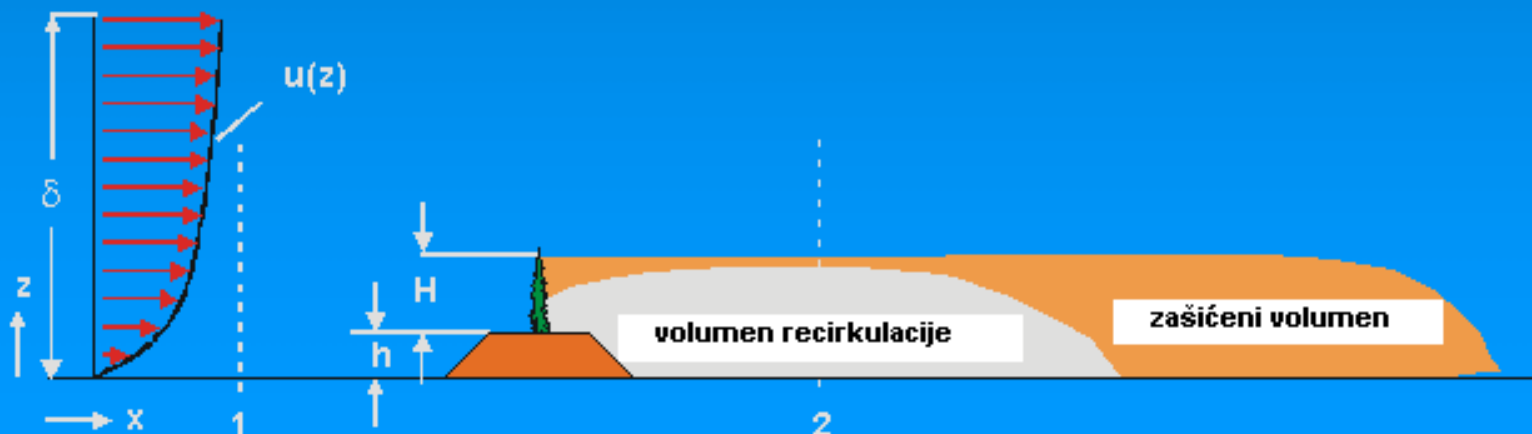
## PROCJENA VJETROVNE ZAŠTITE

### Parametri učinka zaštite

- $S_u$ : relativna promjena strujnog impulsa i djelovanja aerodinamičkih sila (faktor zaštite)
- $f$ : komforni parametar prema Gandemer-u
- $S_{u'w'}$ : vertikalni tok impulsa (vertikalni faktor zaštite)

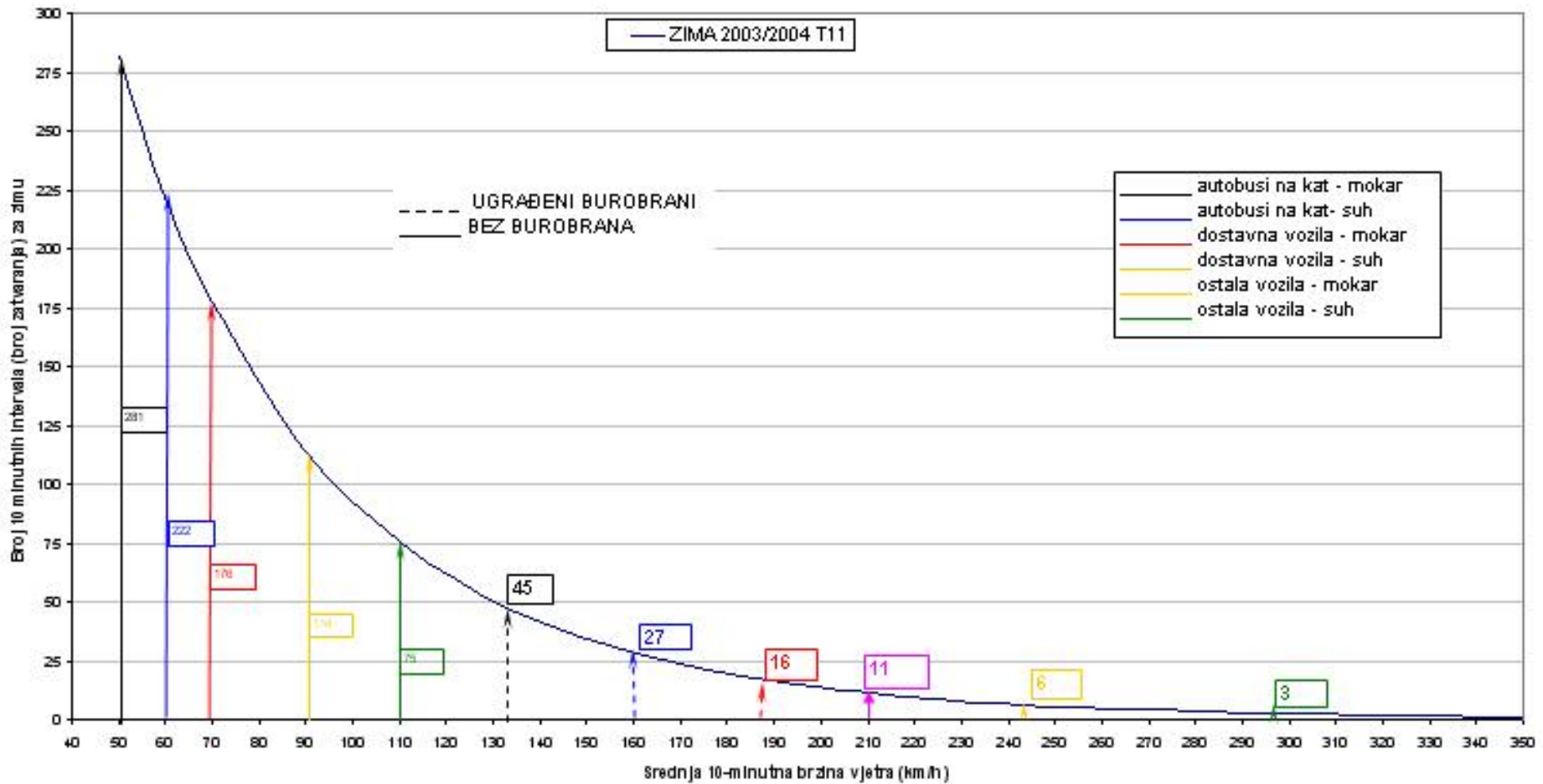
→ Određivanje zaštitnog volumena

$$S_u(x,z) = 1 - \frac{u_2(x,z)^2}{u_1(z)^2}$$
$$f(x,z) = \frac{u_1(z) + \sigma(u_1(z))}{u_2(x,z) + \sigma(u_2(x,z))}$$
$$S_{u'w'}(x,z) = 1 - \frac{u'w'_2(x,z)}{u'w'_1(z)}$$





# Trajanje olujnih vjetrova



Očekivano trajanje bure pri kojoj se zatvora promet osobnih vozila (sa i bez izgradnje burobrana)

## **Windgeschwindigkeit nach DIN 1055**

Bei der vereinfachten Auslegung nicht schwingungsfähiger Bauten wird eine Windgeschwindigkeit in unterschiedlichen Höhen vorgegeben ("Treppenlinie" aus DIN 1055, Teil 4, Tabelle 1). Diese Treppenlinie kann näherungsweise als Einhüllende der möglichen Nennböenprofile betrachtet werden.

$$v(z) = v(10) \left[ \frac{z}{10} \right]^{0,11}$$