

OTPORNOST MATERIJALA 1

1. kolokvij, 17. studenoga 2021.

Prezime i ime:

Grupa
C



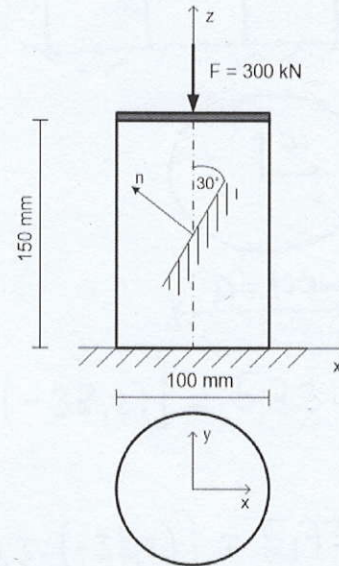
1.

Valjak od izotropnog i homogenog materijala opterećen je prema slici. Treba odrediti:

- A) tenzor naprezanja i deformacija za koordinatni sustav xyz
- B) apsolutnu i relativnu promjenu volumena valjka
- C) vektor punog naprezanja za ravninu s normalom n označenom na slici

$$E = 2 \cdot 10^5 \text{ MPa}$$

$$\nu = 0.3$$



2.

Apsolutno kruta greda ABC pričvršćena je zglobno u točki B i pridržana štapovima 1 i 2 u točki A.

Štap 2 je izveden kraći od svoje potrebne duljine za $\Delta = 3 \text{ mm}$.

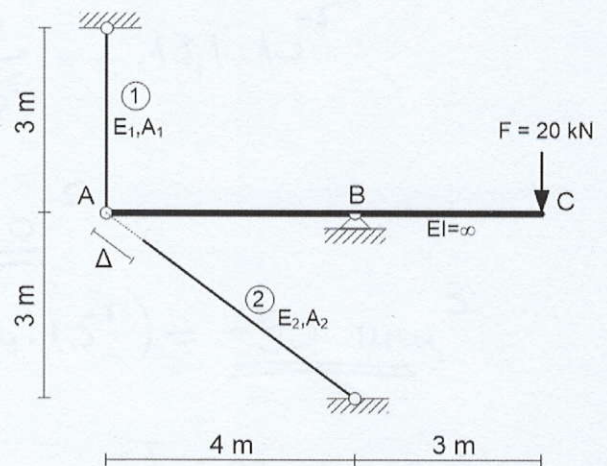
Treba odrediti naprezanja u štapovima 1 i 2 nakon spajanja štapa 2 i grede u točki A, te pomak točke C.

Zadano:

$$E_1 = E_2 = 200 \text{ GPa}$$

$$A_1 = 120 \text{ mm}^2$$

$$A_2 = 200 \text{ mm}^2$$



3.

Na spoj drvenog elementa 1 i čeličnog moždanika 2 djeluje sila F.

Treba odrediti dopuštenu veličinu sile F ako su zadane vrijednosti dopuštenih naprezanja.

Za drvo:

$$\sigma_{vl,dop} = 10 \text{ MPa}$$

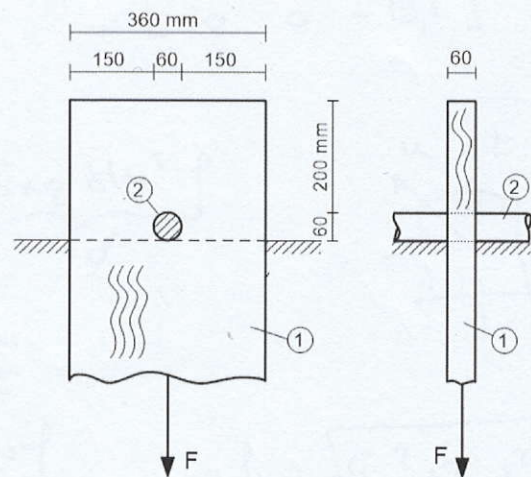
$$\sigma_{tl,dop} = 12 \text{ MPa}$$

$$\tau_{dop} = 2 \text{ MPa}$$

Za čelik:

$$\sigma_{o,dop} = 210 \text{ MPa}$$

$$\tau_{dop} = 110 \text{ MPa}$$



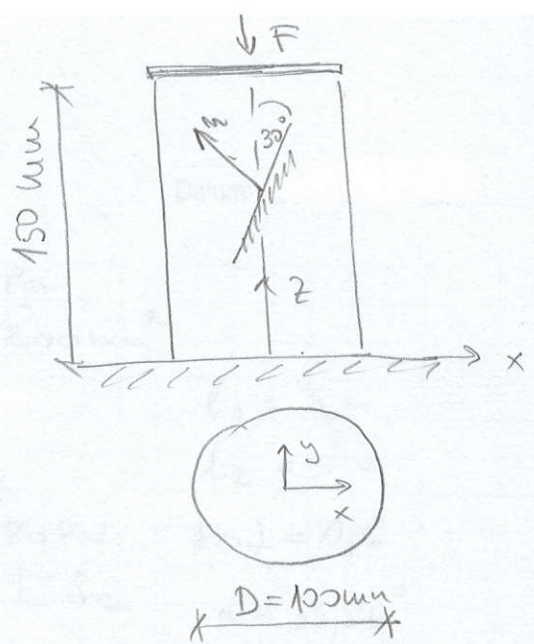
$$① E = 2 \cdot 10^5 \text{ MPa}$$

$$\nu = 0,3$$

$$F = 300 \text{ kN}$$

$$\sigma_z = \frac{F}{A} = \frac{-300 \cdot 10^3}{\frac{100^2 \pi}{4}} = -38,2 \text{ MPa}$$

$$\sigma_x = \sigma_y = \phi$$



$$\epsilon_x = \frac{1}{E} [\sigma_x - \nu(\sigma_y + \sigma_z)] = \frac{1}{2 \cdot 10^5} [-0,3 \cdot (-38,2)] = 5,73 \cdot 10^{-5}$$

$$\epsilon_y = \frac{1}{E} [\sigma_y - \nu(\sigma_x + \sigma_z)] = \frac{1}{2 \cdot 10^5} [-0,3 \cdot (-38,2)] = 5,73 \cdot 10^{-5}$$

$$\epsilon_z = \frac{1}{E} [\sigma_z - \nu(\sigma_x + \sigma_y)] = \frac{-38,2}{2 \cdot 10^5} = -19,1 \cdot 10^{-5}$$

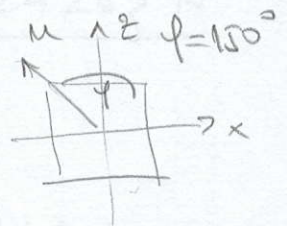
$$\epsilon_v = \epsilon_x + \epsilon_y + \epsilon_z = \underline{\underline{-7,64 \cdot 10^{-5}}}$$

$$\Delta V = V \cdot \epsilon_v = \frac{100^2 \pi}{4} \cdot 150 \cdot (-7,64 \cdot 10^{-5}) = \underline{\underline{-90 \text{ mm}^3}}$$

$$\sigma_{ij} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & -38,2 \end{bmatrix} \text{ MPa}$$

$$\epsilon_{ij} = \begin{bmatrix} 5,73 & 0 & 0 \\ 0 & 5,73 & 0 \\ 0 & 0 & -19,1 \end{bmatrix} \cdot 10^{-5}$$

$$\begin{aligned} \sigma_n &= \underbrace{\sigma_x \cdot \cos^2 \varphi}_{\phi} + \sigma_z \sin^2 \varphi + \underbrace{\tau_{xz} \sin^2 \varphi}_{\phi} \\ &= \sigma_z \cdot \sin^2 \varphi = \underline{\underline{-9,55 \text{ MPa}}} \end{aligned}$$



$$\begin{aligned} \tau_{cut} &= \frac{\sigma_z - \sigma_x}{2} \sin 2\varphi + \underbrace{\tau_{xz} \cdot \cos \varphi}_{\phi} \\ &= \frac{\sigma_z}{2} \sin 2\varphi = \underline{\underline{16,54 \text{ MPa}}} \end{aligned}$$

$$\begin{aligned} \rho_n &= \sqrt{\sigma_n^2 + \tau_{cut}^2} \\ &= \underline{\underline{19,1 \text{ MPa}}} \end{aligned}$$



2.B

$E_1 = E_2 = E = 2 \cdot 10^5 \text{ MPa}$

$A_1 = 120 \text{ mm}^2 \quad A_2 = 200 \text{ mm}^2$

$\Delta = 3 \text{ mm}$

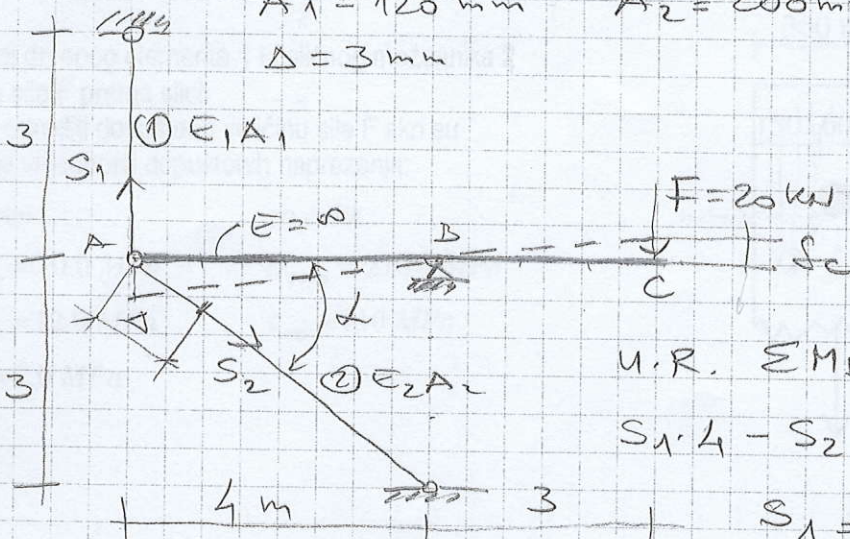
$l_1 = 3 \text{ m}$

$l_2 = 5 \text{ m}$

$F = 20 \text{ kN}$

$\sin \alpha = 0,6$

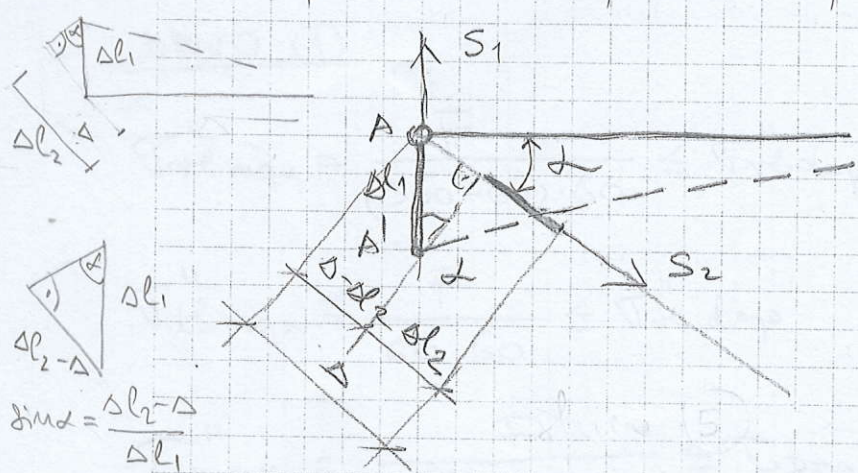
$\alpha = 36,86^\circ$



U.R. $\sum M_B = 0$

$S_1 \cdot 4 - S_2 \cdot \sin \alpha \cdot 4 + F \cdot 3 = 0$

$S_1 = S_2 \cdot \sin \alpha - \frac{3}{4} F \quad (1)$



UNIET. DEF.

$\sin \alpha = \frac{\Delta - \Delta l_2}{\Delta l_1} \quad (2)$

$\Delta l_1 \cdot \sin \alpha = \Delta - \Delta l_2 \quad (2')$

$\frac{S_1 \cdot l_1}{EA_1} \cdot \sin \alpha = \Delta - \frac{S_2 \cdot l_2}{EA_2} \quad (2'')$

$(1) \rightarrow (2'') \quad \left(S_2 \cdot \sin \alpha - \frac{3}{4} F \right) \frac{l_1 \cdot \sin \alpha}{EA_1} + \frac{S_2 \cdot l_2}{EA_2} = \Delta \frac{EA_1}{l_1}$

$S_2 \cdot \sin^2 \alpha - \frac{3}{4} F \cdot \sin \alpha + S_2 \frac{A_1 \cdot l_2}{A_2 \cdot l_1} = \Delta \frac{EA_1}{l_1}$

$S_2 = \frac{\frac{3}{4} F \cdot \sin \alpha + \Delta \frac{EA_1}{l_1}}{\sin^2 \alpha + \frac{A_1 \cdot l_2}{A_2 \cdot l_1}} = \frac{3000 + 24000}{1,36} = \underline{24265 \text{ N}}$

$S_2 = +24,265 \text{ kN vlač}$

$S_1 = S_2 \cdot \sin \alpha - \frac{3}{4} F = 14,559 - 15,00 = \underline{-0,441 \text{ kN tlač}}$

$\sigma_{(1)} = \frac{S_1}{A_1} = \underline{-3,675 \text{ MPa}}$

$\Delta l_1 = \frac{S_1 \cdot l_1}{EA_1} = \underline{-0,055 \text{ mm}}$

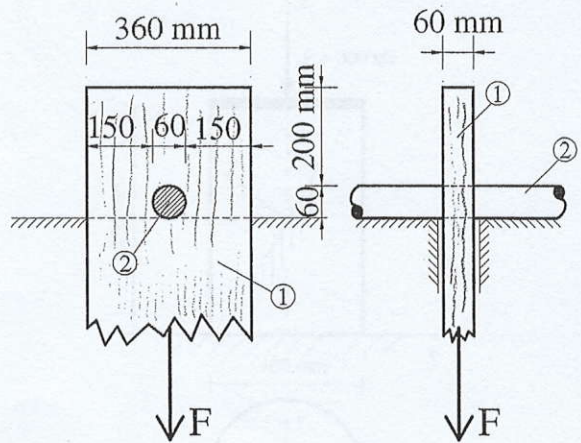
$\sigma_{(2)} = \frac{S_2}{A_2} = \underline{+121,325 \text{ MPa}}$

$\delta_C = \Delta l_1 \cdot \frac{3}{4} = \underline{+0,0413 \text{ mm}}$

3. C.

Na spoj drvenog elementa 1 i čeličnog moždanika 2 djeluje sila F prema slici. Treba odrediti dopuštenu veličinu sile F ako su zadane vrijednosti dopuštenih naprezanja:

- | | |
|---|--------------------------------------|
| za drvo: | za čelik: |
| $\sigma_{vl,dop}^{II} = 10,0 \text{ MPa}$ | $\sigma_{o,dop} = 210,0 \text{ MPa}$ |
| $\sigma_{tl,dop}^{II} = 12,0 \text{ MPa}$ | $\tau_{dop} = 110 \text{ MPa}$ |
| $\tau_{dop}^{II} = 2,0 \text{ MPa}$ | |



DRVO (1)

$$\sigma_{vl,max}^{II} = \frac{F}{(360 - 60) \cdot 60} \leq \sigma_{vl,dop}^{II} \rightarrow F \leq 180,0 \text{ kN}$$

$$\sigma_{tl,max}^{II} = \frac{F}{60 \cdot 60} \leq \sigma_{tl,dop}^{II} \rightarrow F \leq 43,20 \text{ kN}$$

MJERODAVNO!

$$\tau_{max}^{II} = \frac{F}{(200 + 30) \cdot 60 \cdot 2} \leq \tau_{dop}^{II} \rightarrow F \leq 55,20 \text{ kN}$$

43 kN

ČELIK (2)

$$\sigma_{o,max} = \frac{F}{60 \cdot 60} \leq \sigma_{o,dop} \rightarrow F \leq 756,0 \text{ kN}$$

$$\tau_{max} = \frac{F}{2 \cdot \frac{60^2 \pi}{4}} \leq \tau_{dop} \rightarrow F \leq 622,04 \text{ kN}$$

$F_{dop} = 43,0 \text{ kN}$