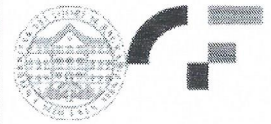


Otpornost materijala 2

2. kolokvij

18. svibnja 2016.

C



Ime i prezime: _____

1. Za zadani sustav odredite i nacrtajte M, T i N dijagrame primjenom principa o minimumu potencijalne energije deformacije.

35

Zadano:

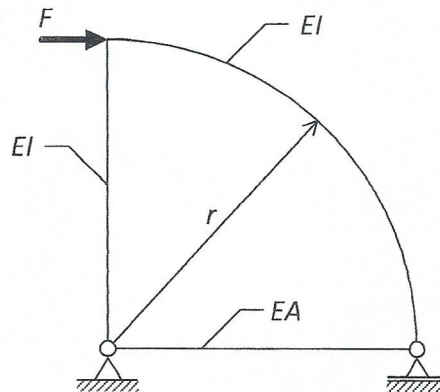
$$F = 20 \text{ kN}$$

$$I = 5,2 \cdot 10^5 \text{ mm}^4$$

$$A = 78,5 \text{ mm}^2$$

$$r = 2 \text{ m}$$

$$E = 210 \text{ GPa}$$



2. Za zadani sustav odredite dopušteno opterećenje iz uvjeta čvrstoće i uvjeta stabilnosti štapova.

35

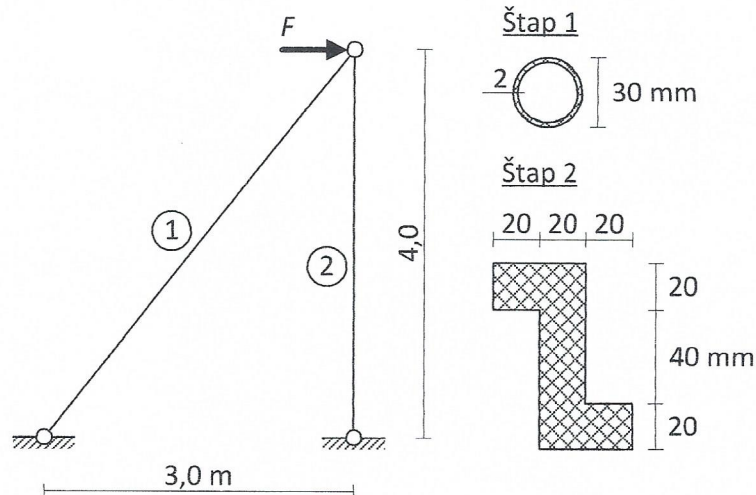
Zadano:

$$\sigma_{vl,dop} = 160 \text{ MPa}$$

$$\sigma_p = 210 \text{ MPa}$$

$$E = 200 \text{ GPa}$$

$$k_{izvijanje} = 2,1$$



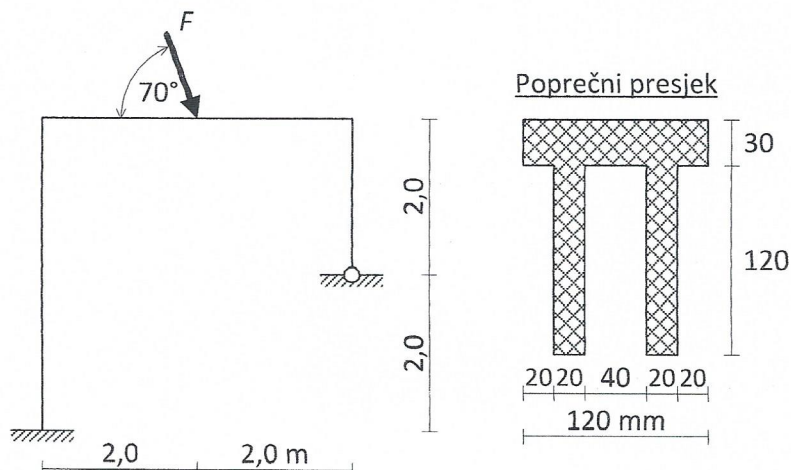
3. Za zadani sustav odredite dopušteno opterećenje prema teoriji plastičnosti.

30

Zadano:

$$\sigma_T = 210 \text{ MPa}$$

$$k = 1,2$$



ZADATAK 1

Zadano:

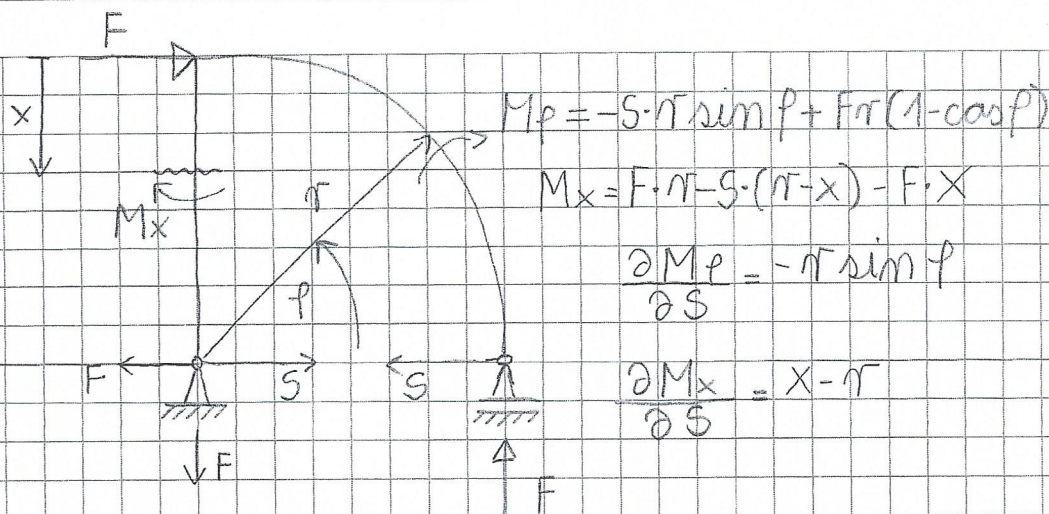
$$F = 20 \text{ kN}$$

$$A = 78,5 \text{ mm}^2$$

$$J = 5,2 \cdot 10^5 \text{ mm}^4$$

$$r = 2 \text{ m}$$

$$E = 210 \text{ GPa}$$



$$M_\phi = -S \cdot r \sin \phi + F r (1 - \cos \phi)$$

$$M_x = F \cdot r - S \cdot (r - x) - F \cdot x$$

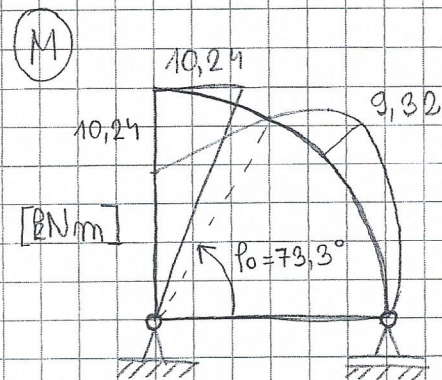
$$\frac{\partial M_\phi}{\partial S} = -r \sin \phi$$

$$\frac{\partial M_x}{\partial S} = x - r$$

$$\frac{\partial U}{\partial x} = -\frac{S \cdot r}{E \cdot A}$$

$$\frac{1}{EJ} \int_0^{\pi/2} [-S r \sin \phi + F r (1 - \cos \phi)] \cdot (-r \sin \phi) r d\phi + \frac{1}{EJ} \int_0^{\pi} [F r - S (r - x) - F \cdot x] \cdot (x - r) dx = -\frac{S \cdot r}{E \cdot A}$$

$$S = \frac{\frac{5}{6} F}{\frac{1}{3} + \frac{\pi}{4} + \frac{J}{A r^2}} = 0,744 F \Rightarrow S = 14,88 \text{ kN} \Rightarrow \sigma = 189,6 \text{ MPa}$$



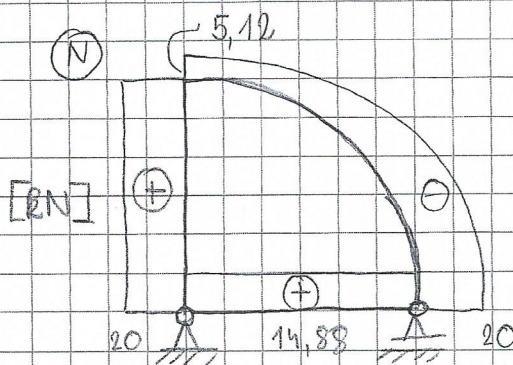
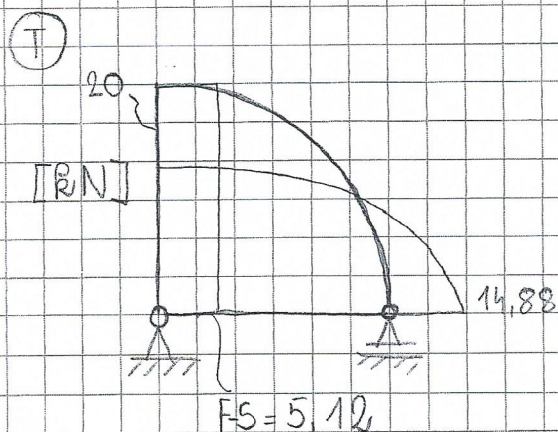
$$M_\phi = -S r \sin \phi + F r (1 - \cos \phi)$$

$$M(\phi = 90^\circ) = 10,24 \text{ kNm}$$

$$M(\phi = 45^\circ) = -9,32 \text{ kNm}$$

$$M_x = F r - S (r - x) - F x$$

$$M(x = 0) = 10,24 \text{ kNm}$$



$$\begin{aligned}\sigma_{ul, dop} &= 160 \text{ MPa} \\ G_P &= 210 \text{ MPa} \\ E &= 2 \cdot 10^5 \text{ MPa} \\ R &= 2,1\end{aligned}$$

$$\alpha = 36,87^\circ$$

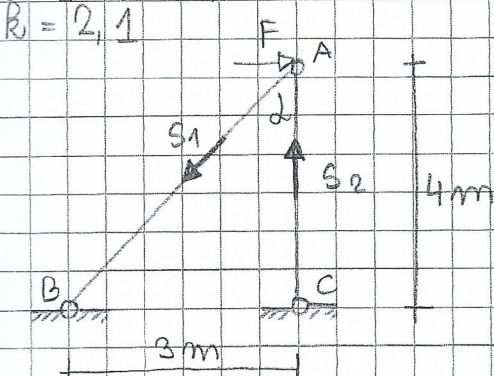
$$\sin \alpha = 0,6$$

$$\cos \alpha = 0,8$$

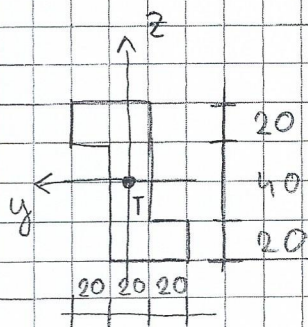
$$\tan \alpha = \frac{3}{4}$$

$$\sum F_H = 0: S_1 = \frac{F}{\sin \alpha}$$

$$\sum F_V = 0: S_2 = S_1 \cos \alpha = \frac{F}{\sin \alpha} \cdot \cos \alpha = \frac{F}{\tan \alpha}$$



2-2



$$A = 2400 \text{ mm}^2$$

$$J_y = 1,6 \cdot 10^6 \text{ mm}^4$$

$$J_z = 0,4 \cdot 10^6 \text{ mm}^4$$

$$J_{yz} = 0,48 \cdot 10^6 \text{ mm}^4$$

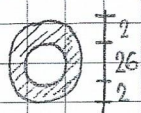
$$J_u = 1,768 \cdot 10^6 \text{ mm}^4$$

$$J_w = 0,232 \cdot 10^6 \text{ mm}^4 = J_{\min}$$

$$i_{\min} = \sqrt{\frac{J_{\min}}{A}}$$

$$i_{\min} = 9,83 \text{ mm}$$

1-1



$$A = \frac{(30^2 - 26^2) \cdot \pi}{4} = 175,93 \text{ mm}^2$$

ŠTAP AB → uvjet čvrstoće

$$\sigma = \frac{S_1}{A} \leq \sigma_{ul, dop}; \quad \frac{F}{\sin \alpha} \leq \sigma_{ul, dop} \rightarrow F \leq 16,89 \text{ kN}$$

ŠTAP AC → uvjet stabilnosti

$$e_i = e = 4 \text{ m}$$

$$S_{KR}^{AC} = \frac{\pi^2 EI_{\min}}{e_i^2} = 28,62 \text{ kN}$$

$$\lambda_P = \sqrt{\frac{\pi^2 E}{G_P}} \approx 97$$

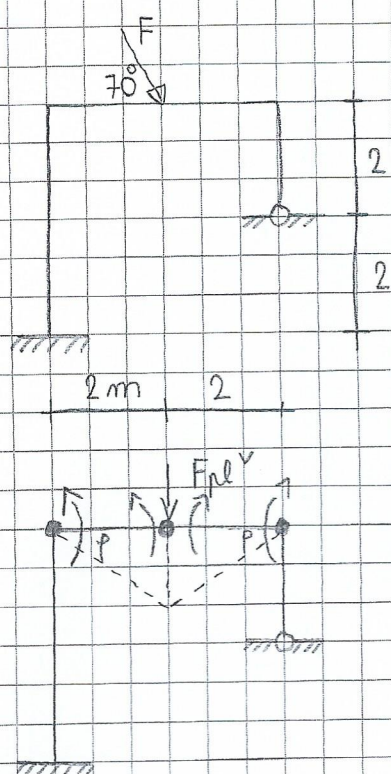
$$S_{dop}^{AC} = \frac{S_{KR}^{AC}}{R_{st}} = 13,63 \text{ kN}$$

$$\lambda = \frac{e_i}{i_{\min}} = 407 > \lambda_P \checkmark$$

$$S_2 = \frac{F}{\tan \alpha} \leq S_{dop}^{AC} \Rightarrow F \leq 10,22 \text{ kN}$$

Mjerodavno!

$\sigma_T = 210 \text{ MPa}$
 $R = 1,2$



$A = 8400 \text{ mm}^2$

$A = \frac{Z_{pl} \cdot 20 \cdot 2}{2}$

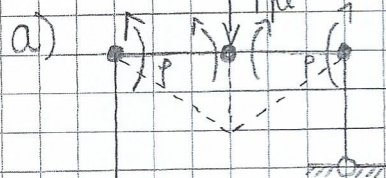
$Z_{pl} = 105 \text{ mm}$

$S_1 = 220500 \text{ mm}^3$

$S_2 = 112500 \text{ mm}^3$

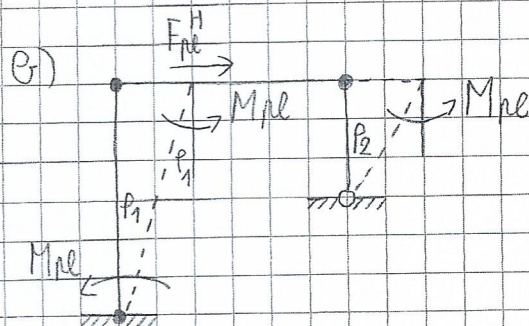
$W_{pl} = S_1 + S_2 = 333000 \text{ mm}^3$

$M_{pl} = W_{pl} \cdot \sigma_T = 69,93 \text{ kNm}$



$F_{pl}^v \cdot 2 = 4 M_{pl} \cdot 2$; $F_{pl}^v = F_{pl} \sin 70^\circ = 0,94 F_{pl}$

$F_{pl} = 2,13 M_{pl} = 148,95 \text{ kN}$

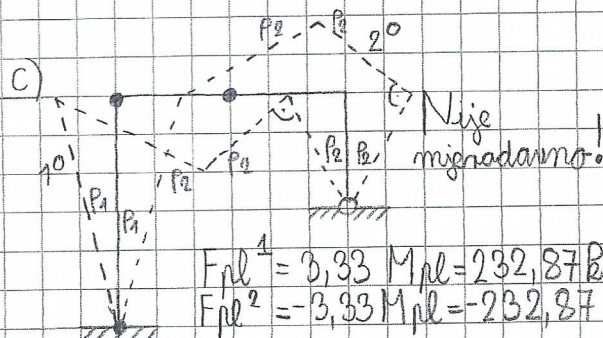


$P_1 \cdot 4 = P_2 \cdot 2$; $P_1 = 0,5 P_2$; $P_2 = 2 P_1$

$F_{pl}^h \cdot P_1 \cdot 4 = 2 M_{pl} P_1 + M_{pl} P_2$; $F_{pl}^h = F_{pl} \cos 70^\circ = 0,34 F_{pl}$

$1,36 F_{pl} \cdot P_1 = 2 M_{pl} P_1 + 2 M_{pl} P_1 = 4 M_{pl} P_1$

$F_{pl} = 2,94 M_{pl} = 205,59 \text{ kN}$



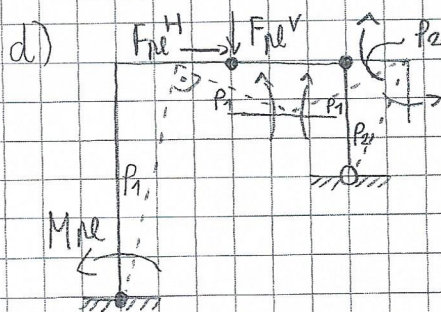
$F_{pl}^1 = 3,33 M_{pl} = 232,87 \text{ kN}$

$F_{pl}^2 = -3,33 M_{pl} = -232,87 \text{ kN}$

$\textcircled{1} - F_{pl}^h \cdot P_1 \cdot 4 + F_{pl}^v \cdot P_2 \cdot 2 = 2 M_{pl} P_1 + 3 M_{pl} P_2$

$- F_{pl}^h \cdot 2 P_2 + F_{pl}^v \cdot 2 P_2 = M_{pl} P_2 + 3 M_{pl} P_2$

$F_{pl}^1 = 3,33 M_{pl}$



$F_{pl}^h \cdot P_1 \cdot 4 + F_{pl}^v \cdot P_1 \cdot 2 = 4 M_{pl} P_1 + M_{pl} P_2$

$0,34 F_{pl} \cdot 4 P_1 + 0,94 F_{pl} \cdot 2 P_1 = 4 M_{pl} P_1 + 2 M_{pl} P_1$

$F_{pl} = 1,85 M_{pl} = 129,37 \text{ kN} = F_{pl, \min}$

$F_{\text{dop}} = F_{pl, \min} / R = 107,81 \text{ kN}$