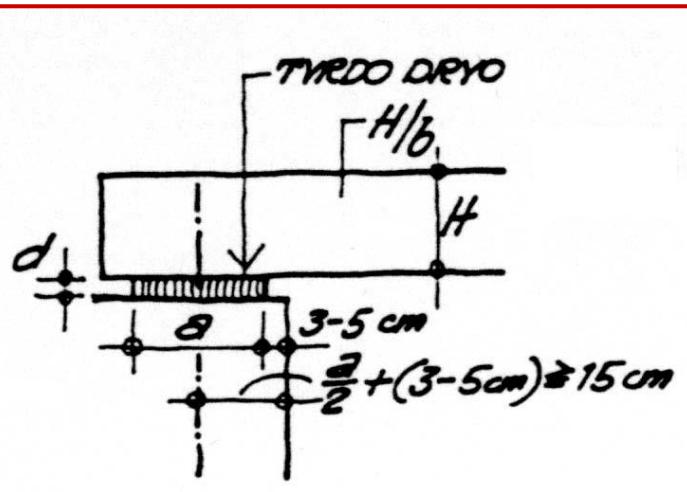


Osnove oblikovanja

ležajeva greda i stupova



Oslanjanje drvenih greda malog i srednjeg raspona na armiranobetonsku potkonstrukciju



Jednostavni ležaj nalijeganjem gredu malih do srednjih raspona na:

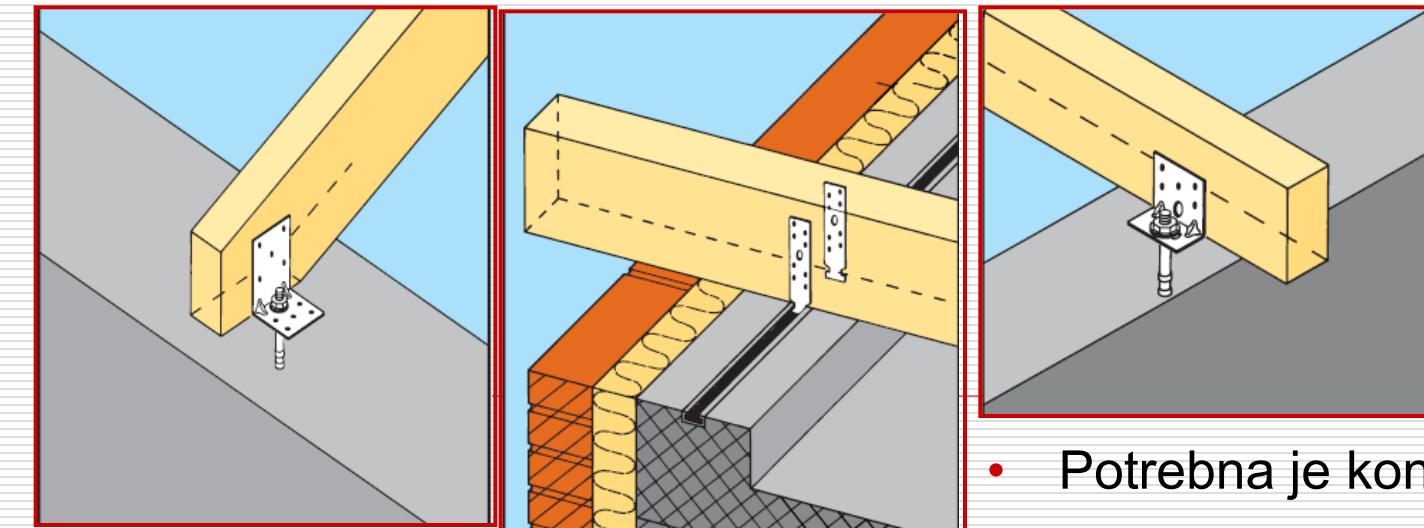
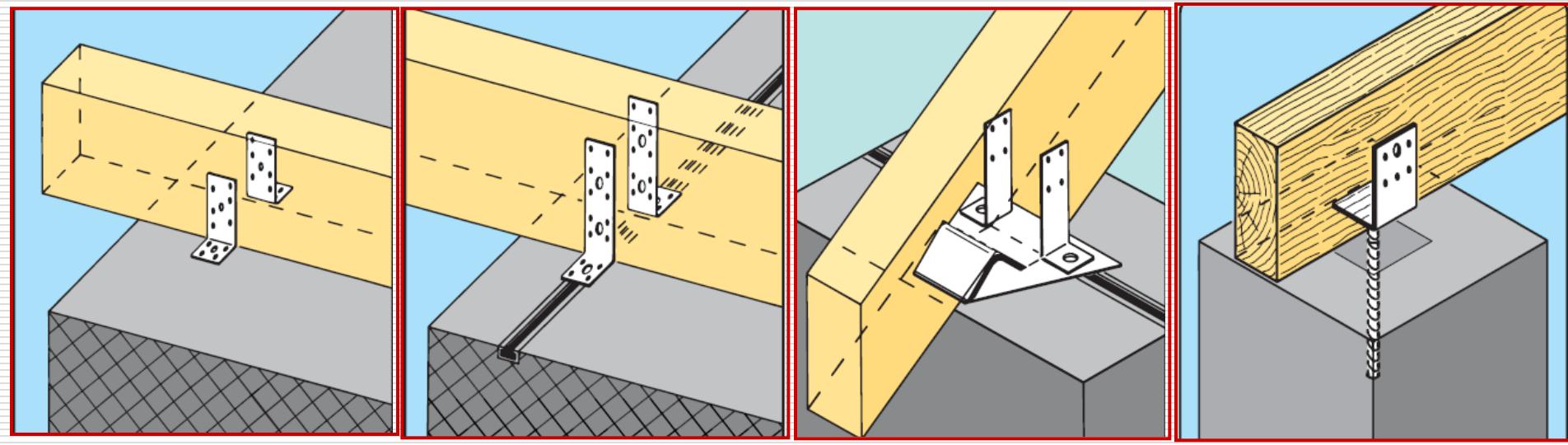
- Kladicu / podložnu gredu (tvrdi drvo)
 - osiguranje kutnicima i sidrenim vijcima ili U-profilima sidara
- Čeličnu podložnu ploču



- osiguranje U-profilima sidara ili T-profilima



Oslanjanje drvenih greda malog raspona na armiranobetonsku potkonstrukciju

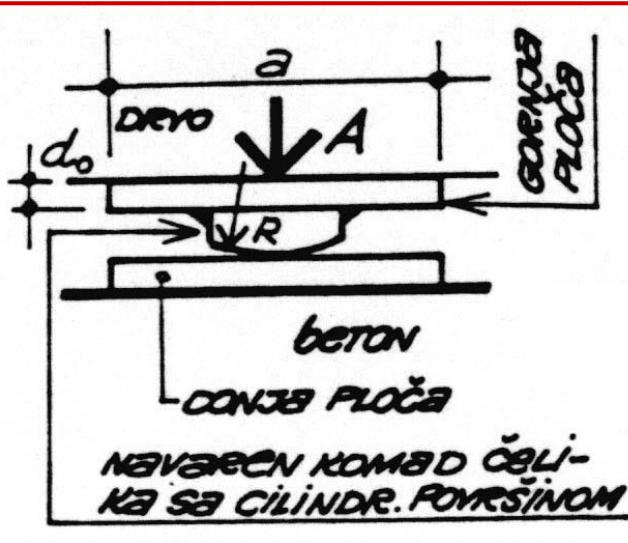


Tipski spojni pribor od tanjih limova – čavlani spojevi

- Potrebna je konstruktivna zaštita³

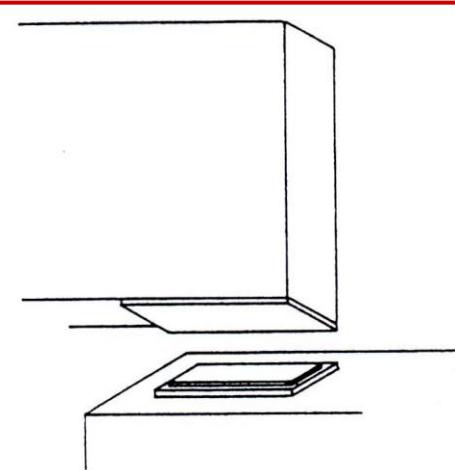
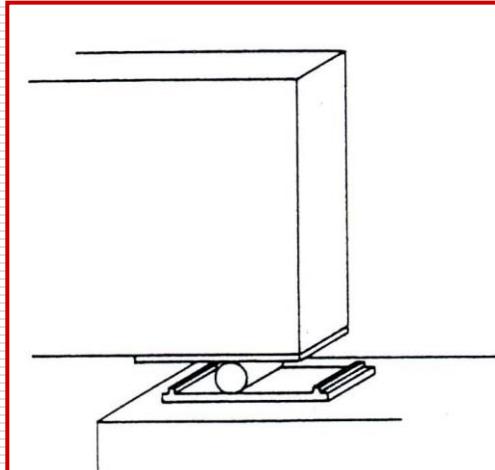
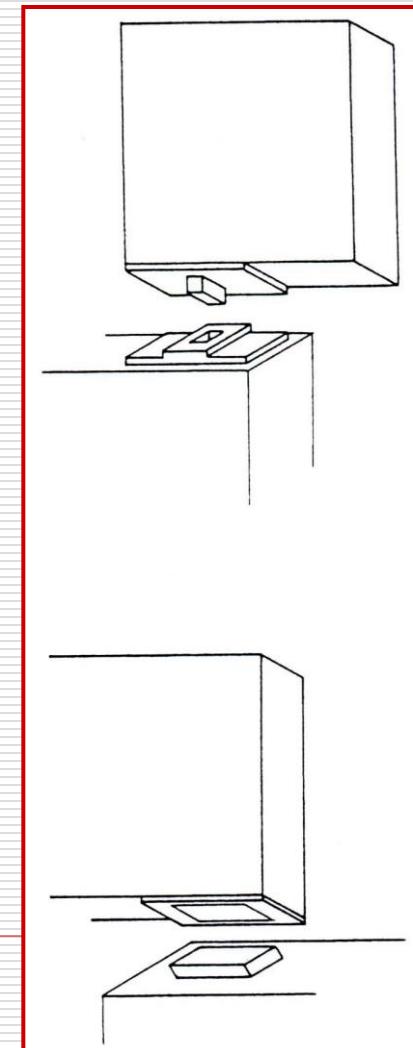


Oslanjanje drvenih greda srednjeg i većeg raspona na armiranobetonsku potkonstrukciju



Ležajevi greda srednjih i većih raspona

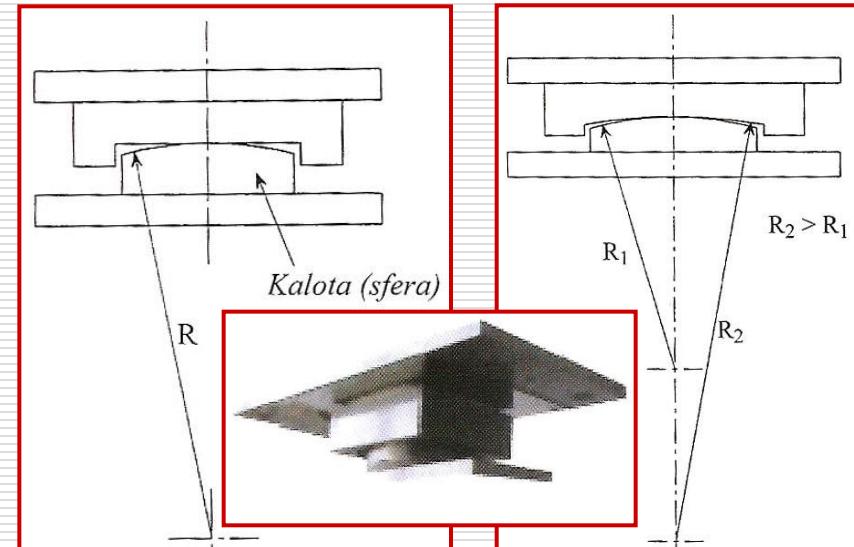
- Linijski ili točkasti ležaj (s gornjom i donjom čeličnom pločom)
- Neoprenski ležaj



Oslanjanje drvenih greda srednjeg i većeg raspona na armiranobetonsku potkonstrukciju

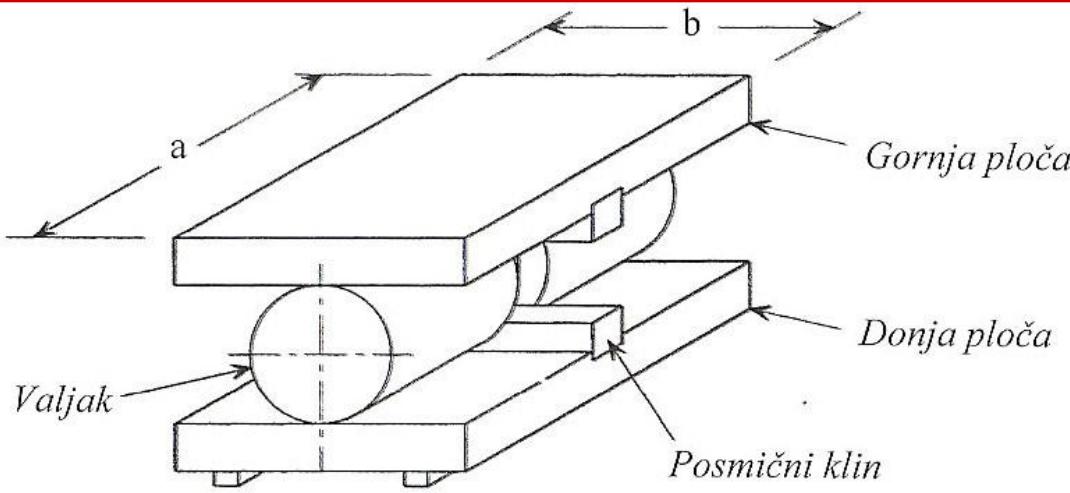


Linijski zaokretni ležaj



Točkasto zaokretni ležajevi s kontaktom ravnina / sfera i sfera / sfera

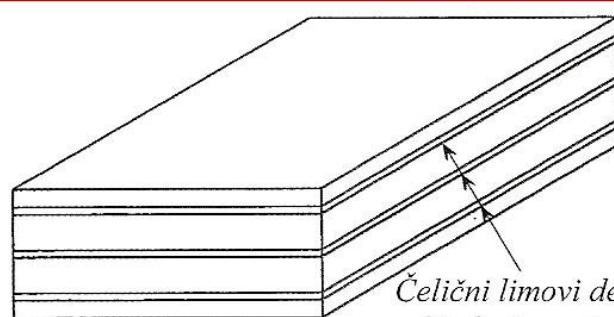
Oslanjanje drvenih greda srednjeg i većeg raspona na armiranobetonsku potkonstrukciju



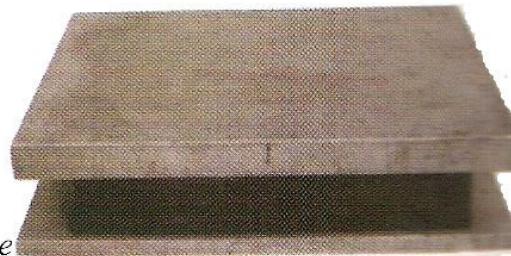
Linijski kotrljajući ležaj – pokretni ležaj



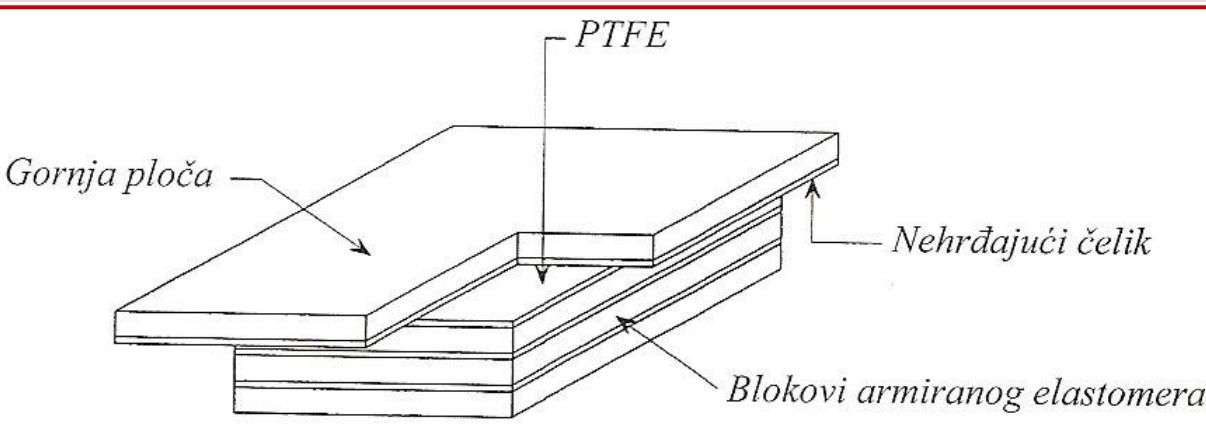
Oslanjanje drvenih greda srednjeg i većeg raspona na armiranobetonsku potkonstrukciju



Čelični limovi debline
od 2 do 5 mm izrađeni
od standardnog ili
nehrđajućeg čelika

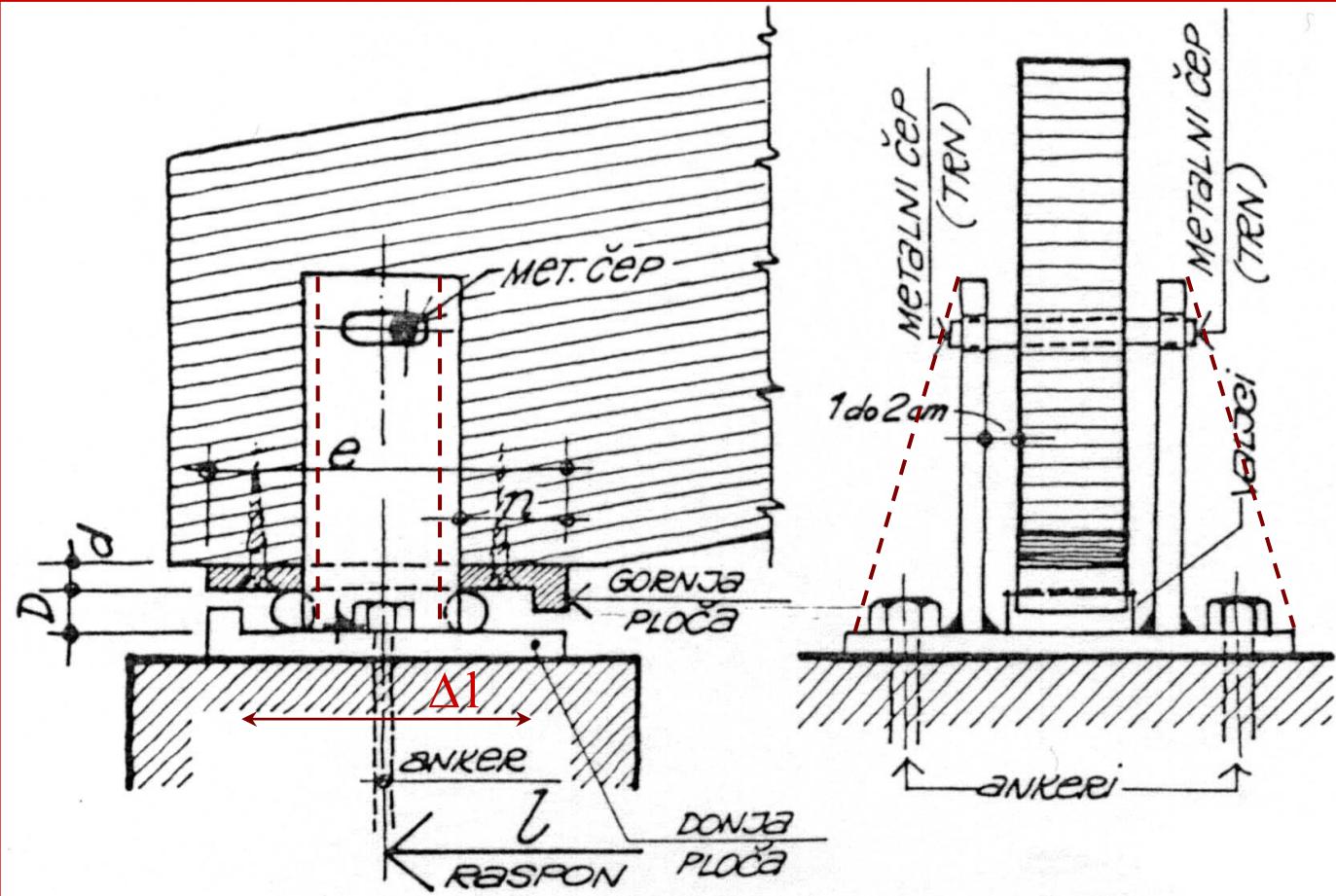


Nepokretni
elastomerni ležaj



Pokretni
elastomerni ležaj

Oslanjanje ljepljenih lameliranih greda velikog raspona na armiranobetonsku potkonstrukciju



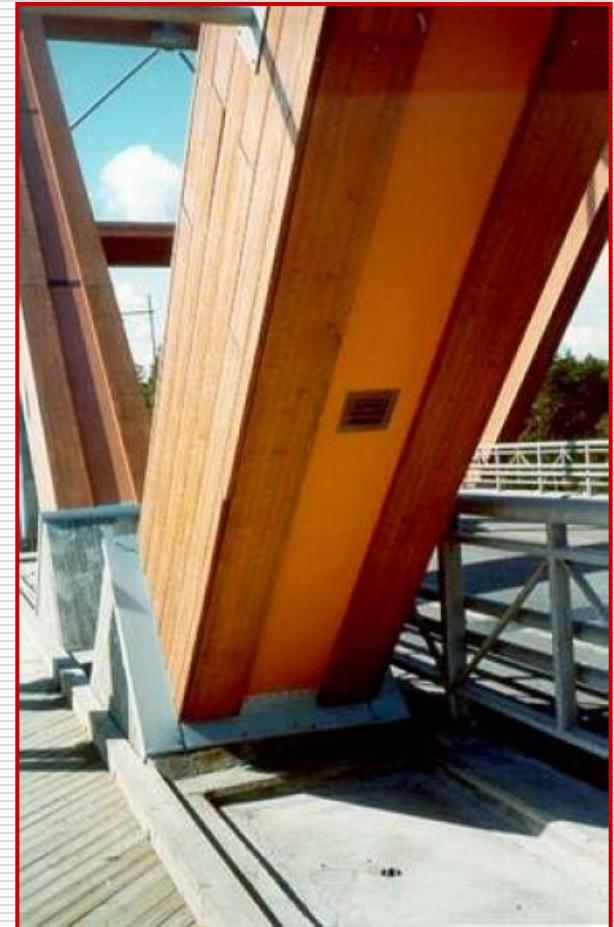
Konstrukcija
pokretnog
linijskog
ležaja

“Zubi”
zavareni na
ležajne ploče
omogućavaju
proračunati
horizontalni
pomak



Oslanjanje drvenih stupova na temelj

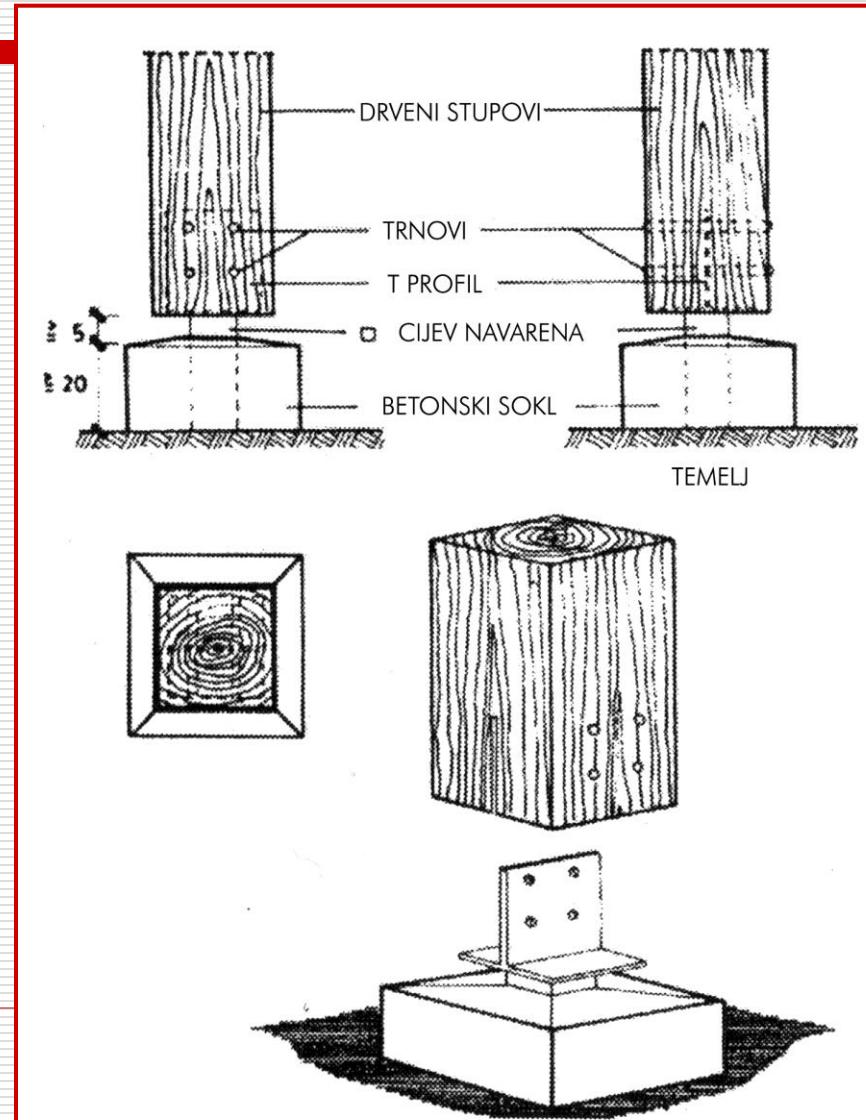
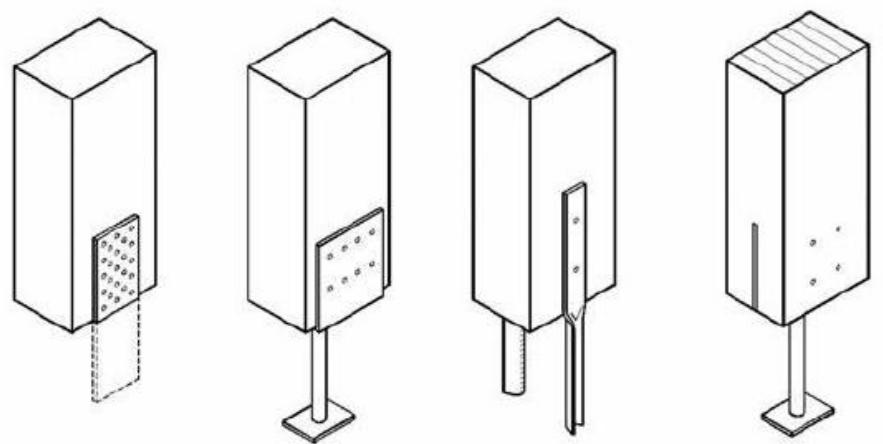
- Mjere konstruktivne i fizičke zaštite su obavezne.





Oslanjanje drvenih stupova sustava manjeg do srednjeg raspona

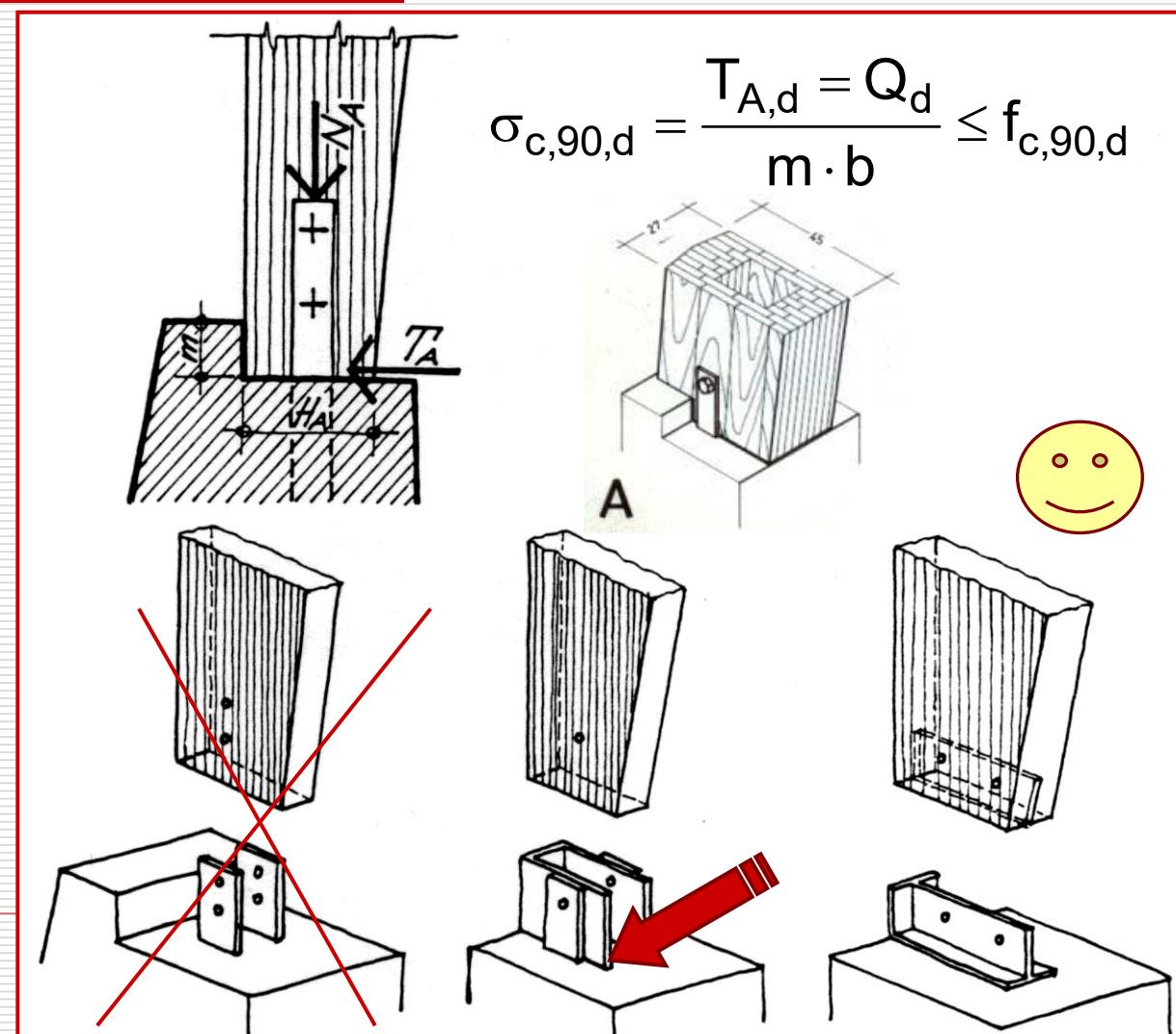
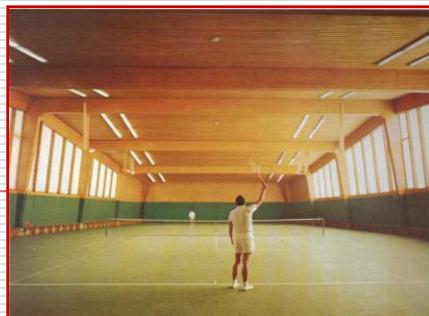
- Vertikalna reakcija prenosi se nalijeganjem (\parallel s vlaknima) na podložnu čeličnu ploču
- Spajala a vezu vertikalnog lima i stupa su konstruktivna –
 - treba ih proračunati u slučaju negativne reakcije.





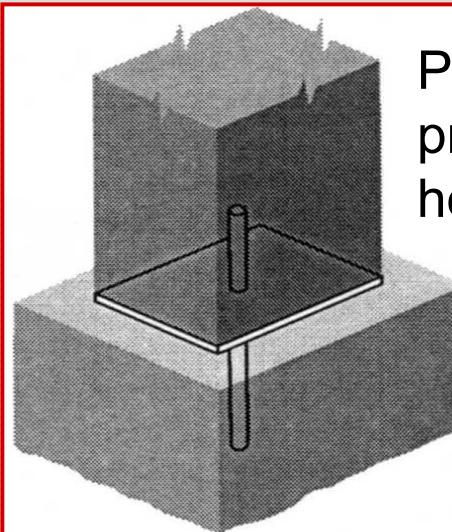
Oslanjanje drvenih stupova sustava manjeg do srednjeg raspona

- Vertikalna reakcija prenosi se nalijegaњem (\parallel s vlaknima) na podložnu čeličnu ploču
- Poprečnu silu prihvata betonski "zub" ili čeona ploča ležaja (\perp na vlakna / površina dodira)

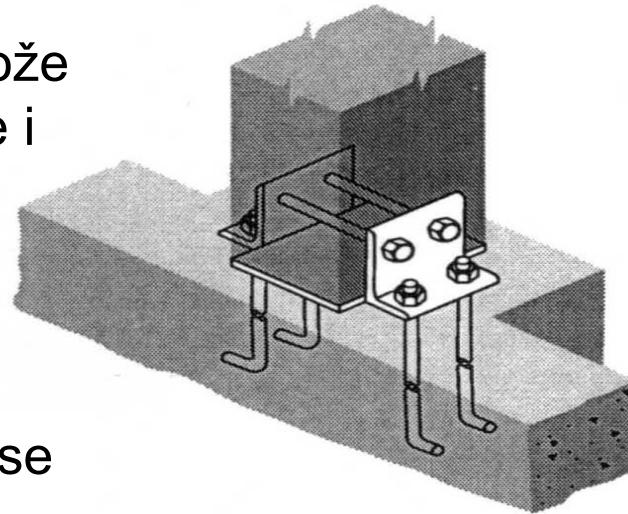




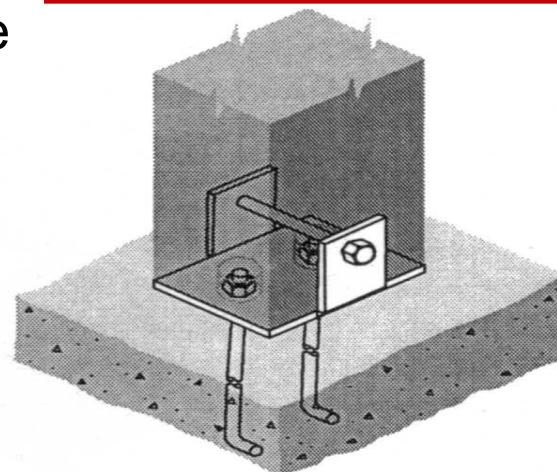
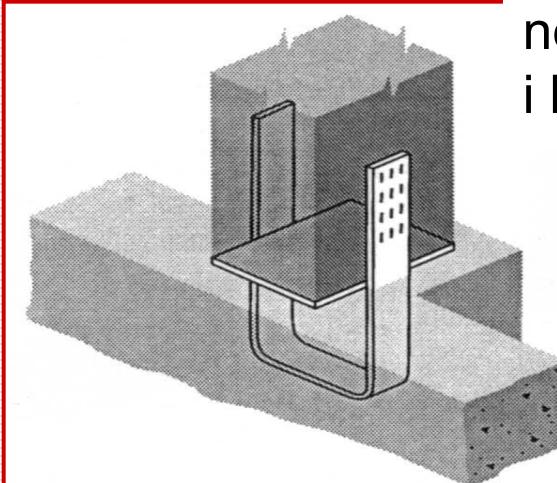
Oslanjanje drvenih stupova sustava manjeg do srednjeg raspona



Priklučak koji ne može
preuzeti odižuće sile i
horizontalne sile



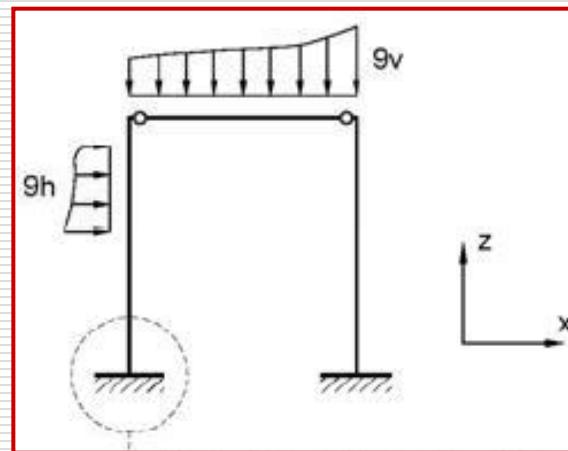
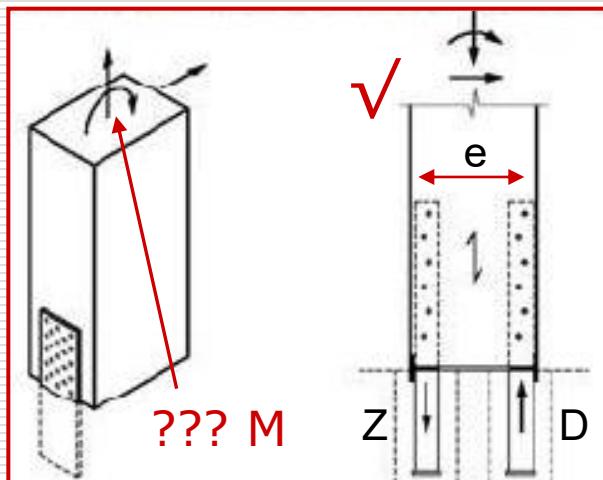
Priklučci kojim se
mogu prihvatiti
negativne reakcije
i horizontalne sile





Upeti oslonci drvenih stupova

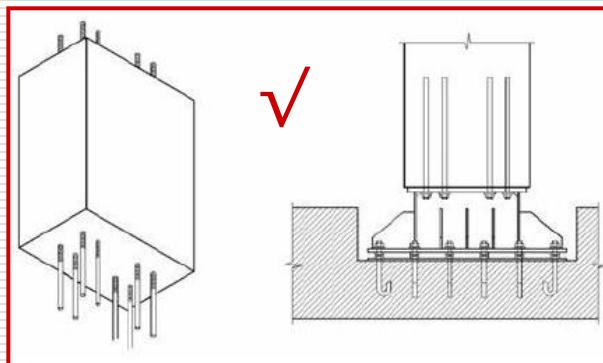
- Načela prijenosa momenta savijanja – spreg sila **Z** (vlačna) i **D** (tlačna) / razmak težišta spajala određuje krak sila, **e**:



$$M_{y,d} = Z_d \cdot e = D_d \cdot e$$

- Vlačnu silu **Z** prihvaćaju spajala

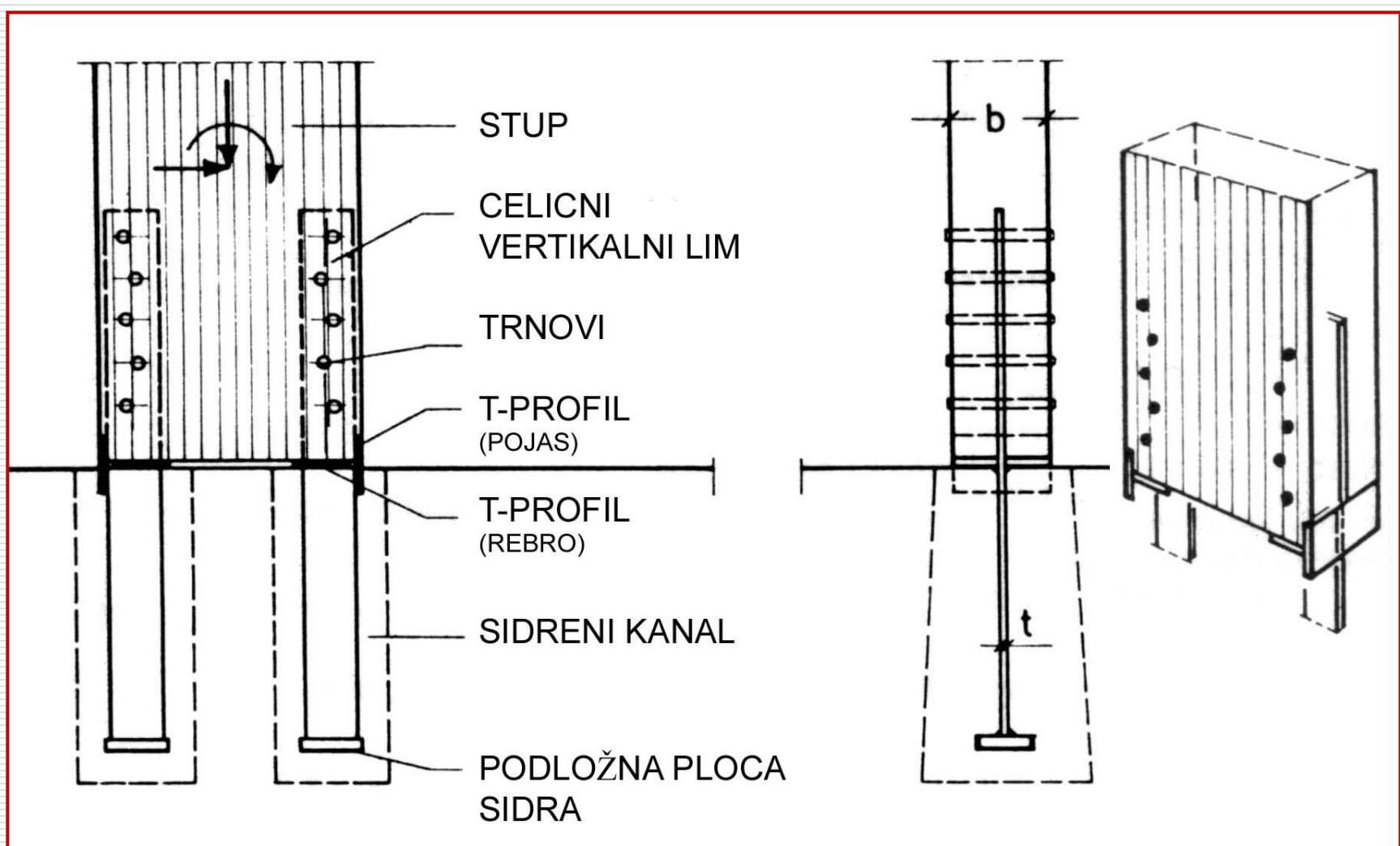
$$Z_d \leq \sum F_{v,R_d(i)}$$



- Tlačna sila **D** prenosi se **nalijeganjem** presjeka stupa na podložnu ploču čeličnog profila (tlakom || s vlaknima).
- Inovativni sustavi – šipke s navojem

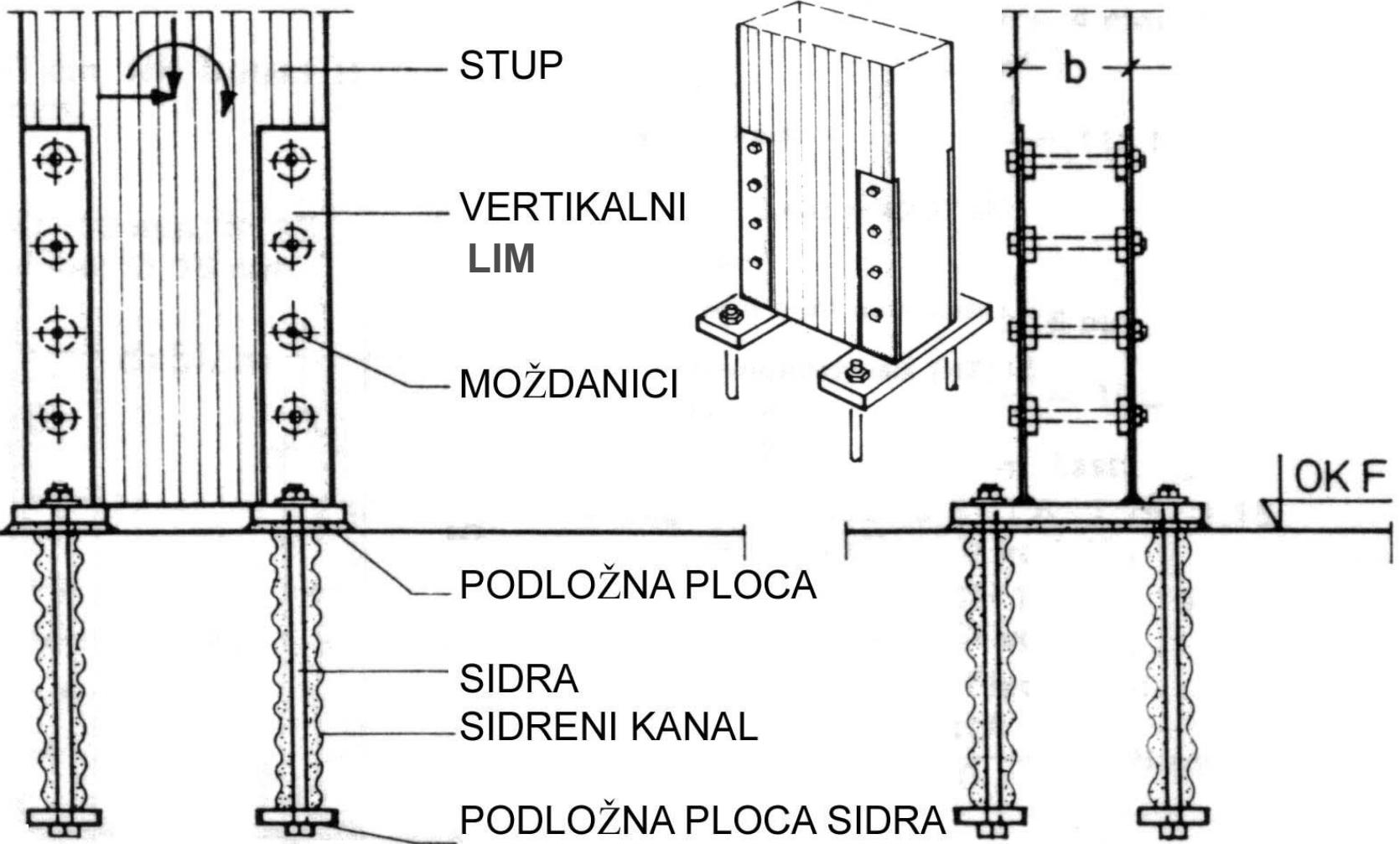


Upeti oslonci drvenih stupova





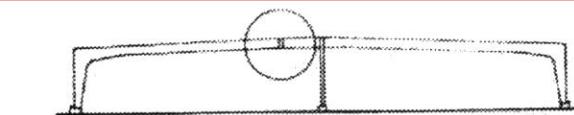
Upeti oslonci drvenih stupova



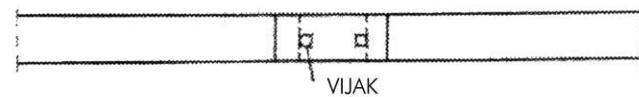
Oblikovanje Gerberovog zgloba



Gerberov zglob u veznim i okvirnim sustavima

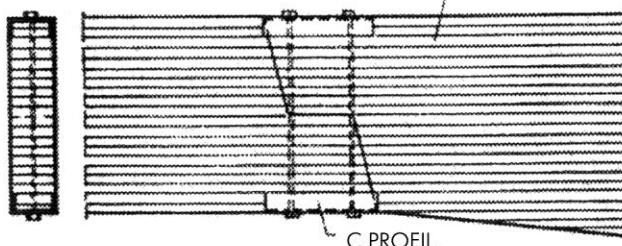


POGLED



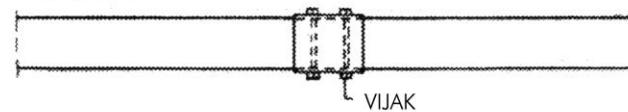
VIJAK

OKIR

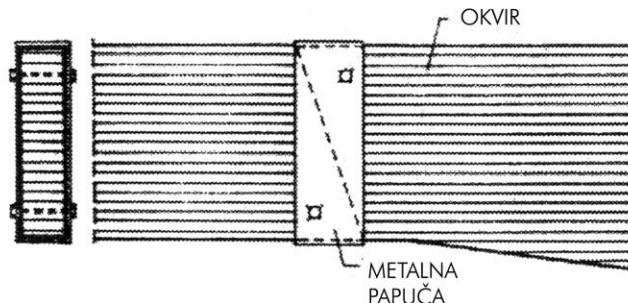


C PROFIL

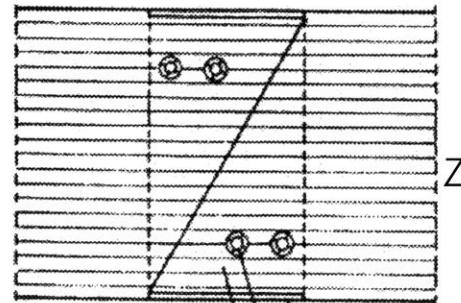
POGLED



VIJAK



METALNA
PAPUČA

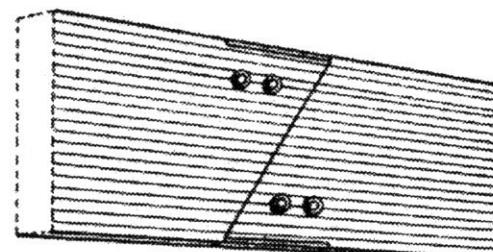


ZGLOBOVI

LEŽAJNA PLOČA

VIJAK

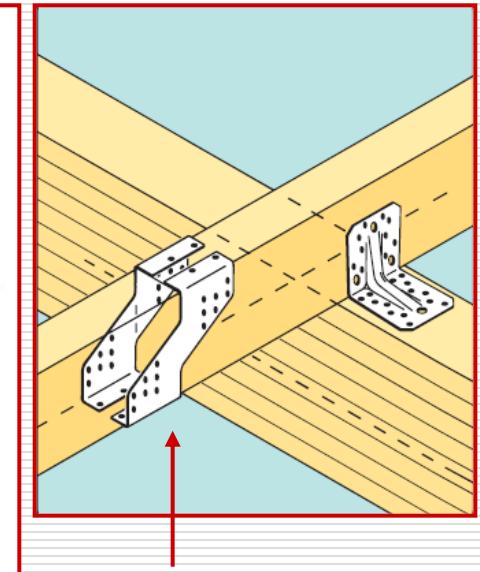
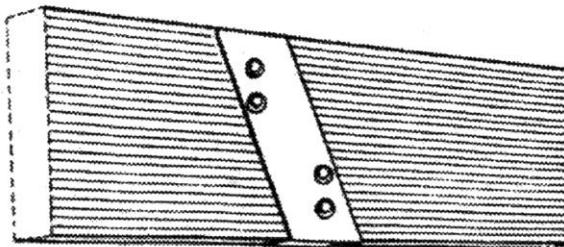
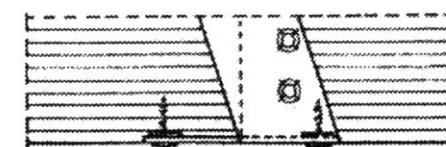
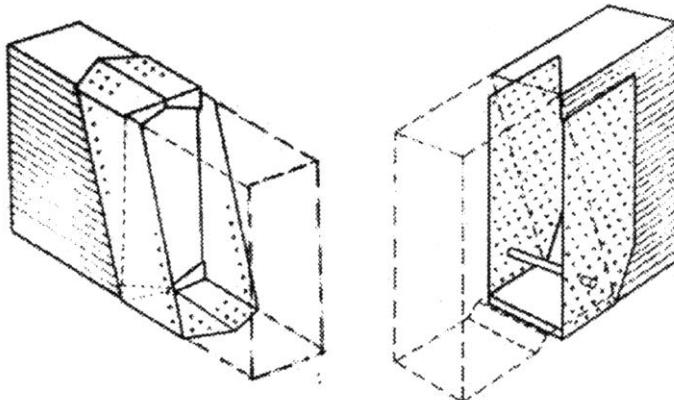
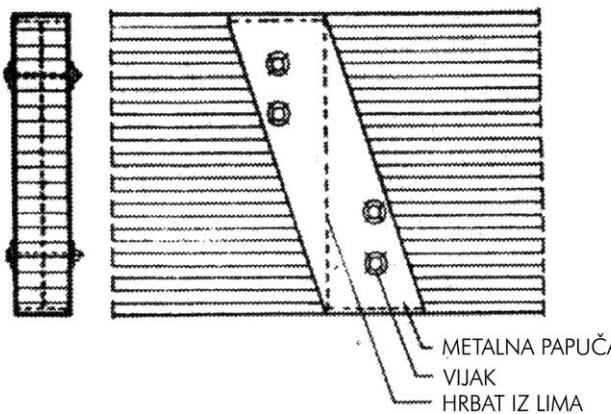
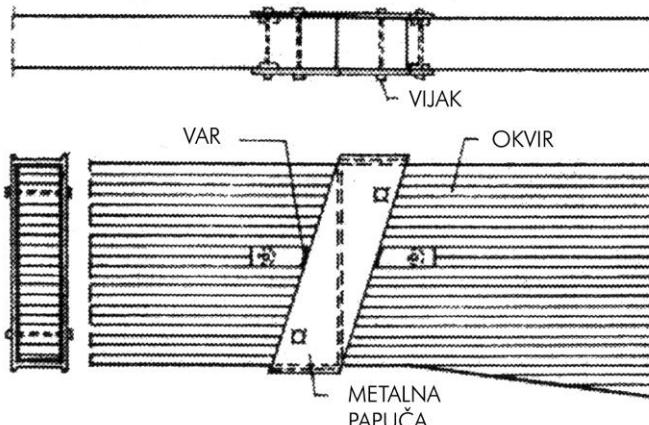
HRBAT IZ PLOSNOG ŽELJEZA





Gerberov zglob u veznim i okvirnim sustavima

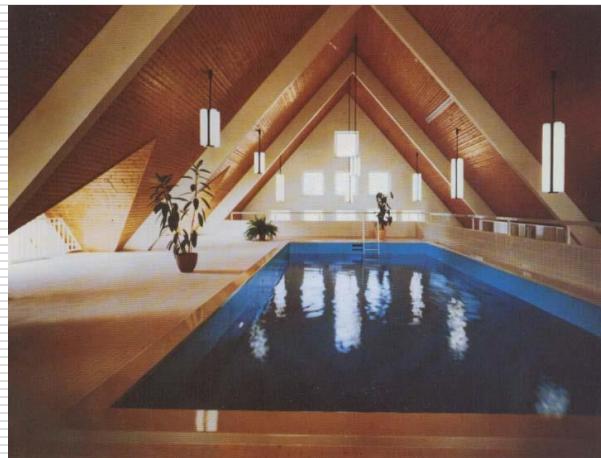
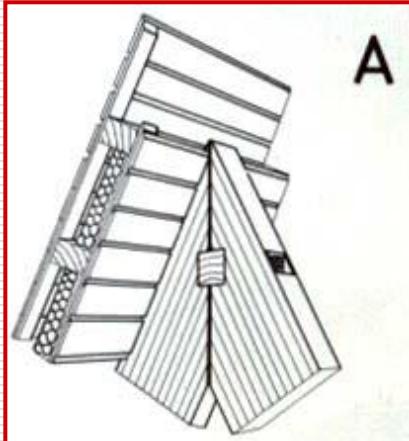
POGLED



Tipsko rješenje
za grede manjeg
raspona

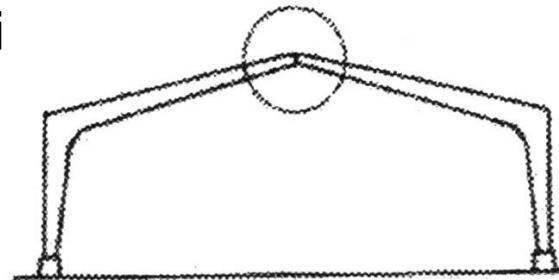
Osnove oblikovanja ležajeva i priključaka u sustavima okvira

Konstrukcije zglobova u tjemenu okvira

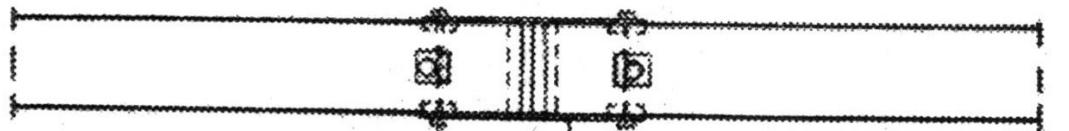


Zglobna
veza greda i
sljemenu za
okvire
manjih
raspona

TJEMENI ZGLOBOVI



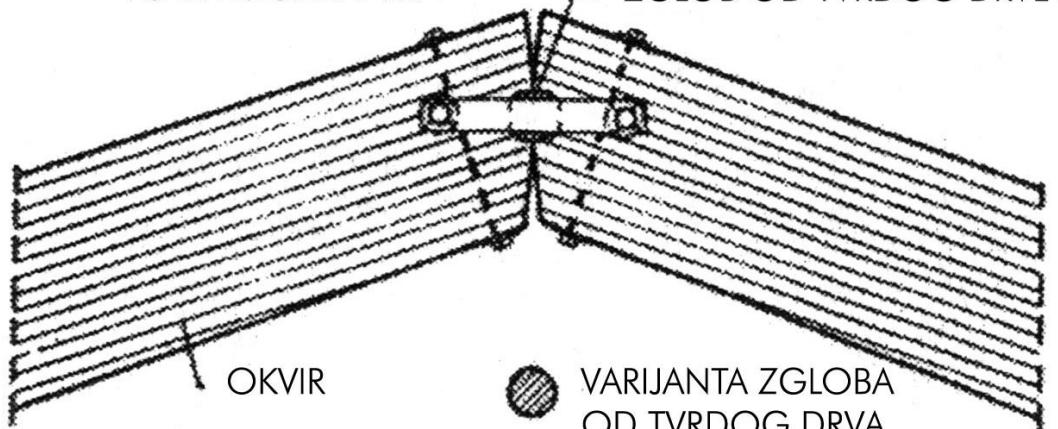
POGLEĐ



VIJAK I MOŽDANIK

METALNE VEZICE

ZGLOB OD TVRDOG DRVETA

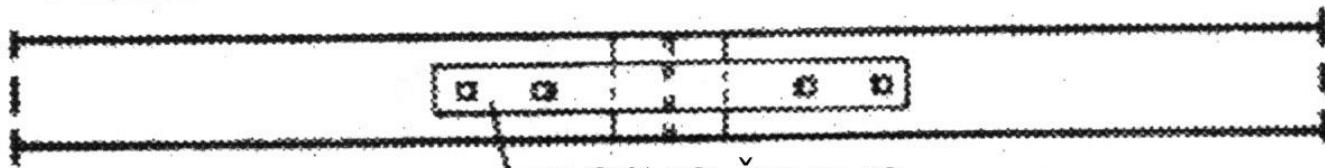


VARIJANTA ZGLOBA
OD TVRDOG DRVA

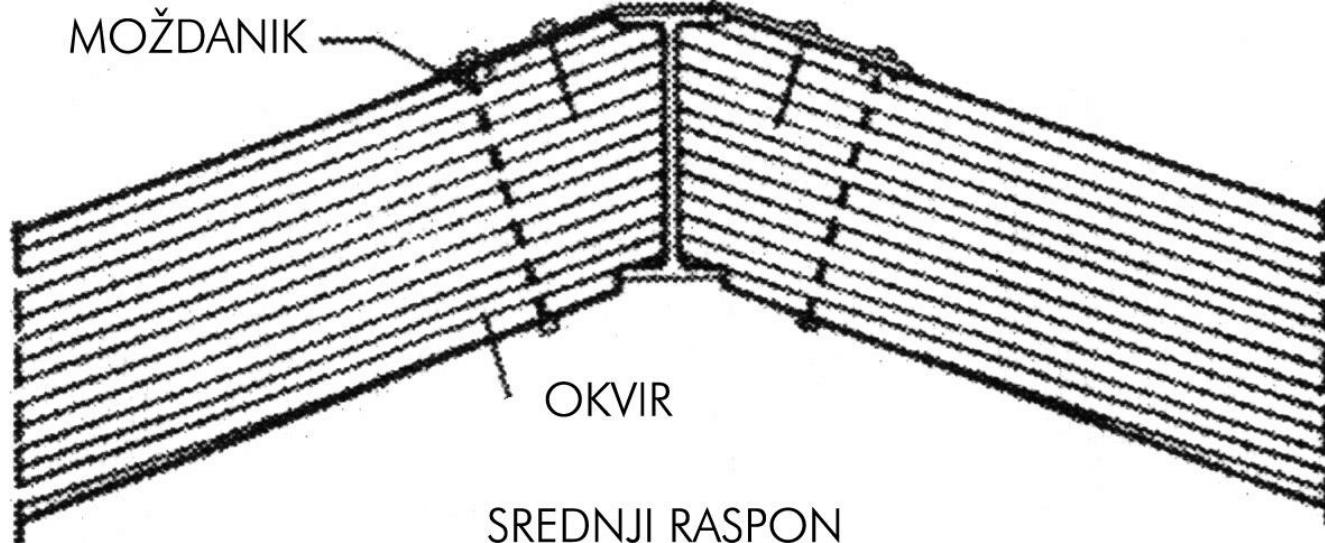


Konstrukcije zglobova u tjemenu okvirnih sustava

POGLED



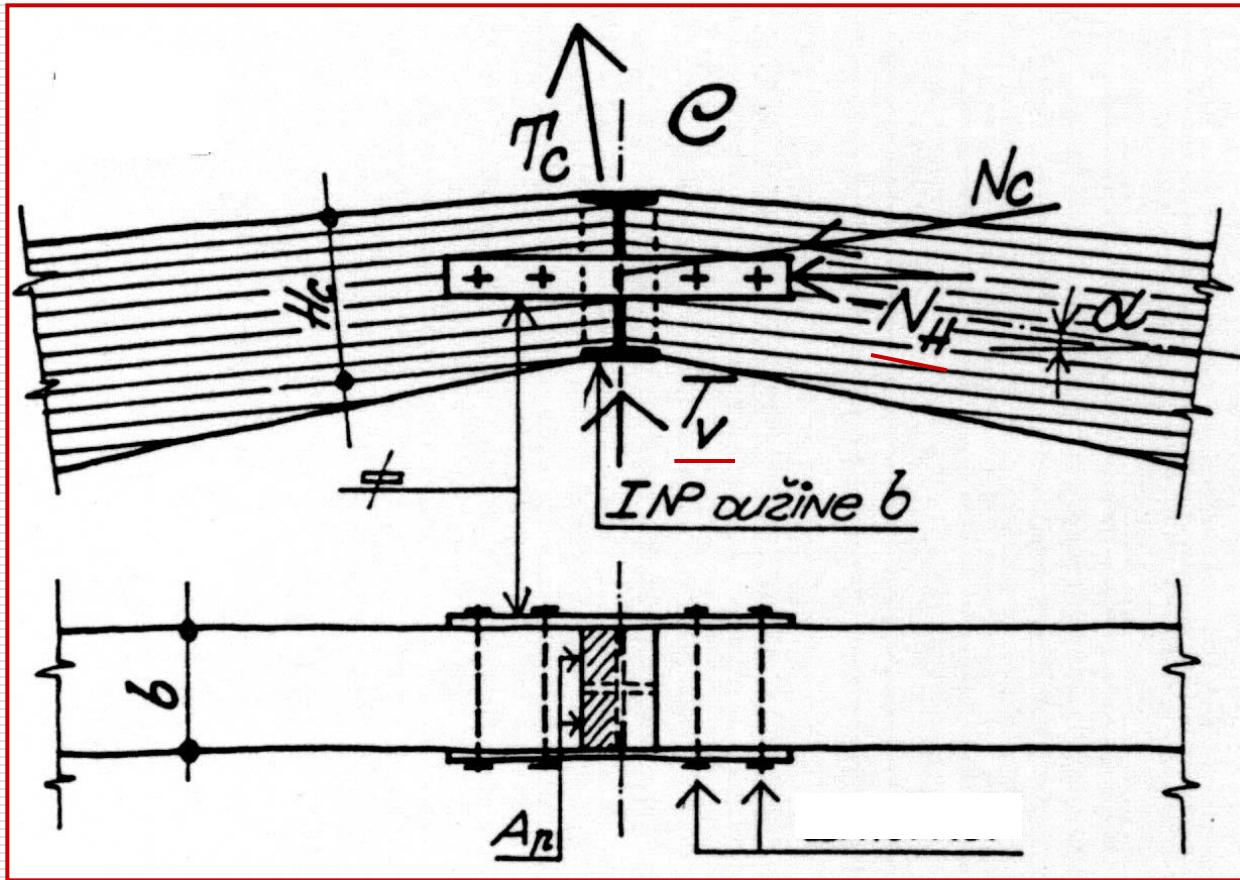
Alternativa gornjim vezicama
su bočne metalne vezice



Zglobna veza greda i sljemenu za
okvire **srednjih raspona**



Konstrukcije zglobova u tjemenu okvirnih sustava



Vijci su konstruktivni ako je osna sila tlačna i ako zadovoljavaju provjere naprezanja na površinama dodira

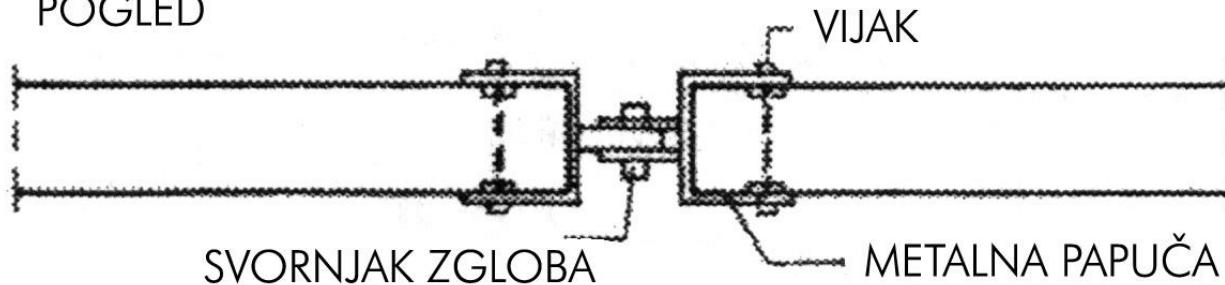
Nosivi su ako ta provjera ne zadovoljava ili je osna sila vlačna

Zglobna veza greda i sljemenu okvira **srednjih raspona**

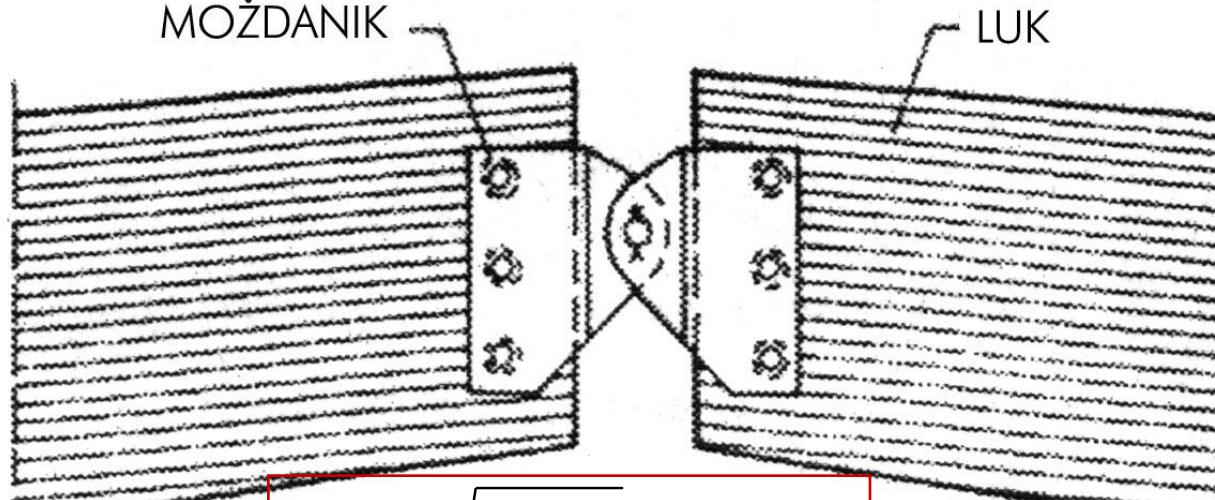


Konstrukcije zglobova u tjemenu lukova i okvira

POGLED



MOŽDANIK



$$\max F_{la} = \sqrt{F_V^2 + F_M^2} \leq \sum F_{v,R_d(i)}$$

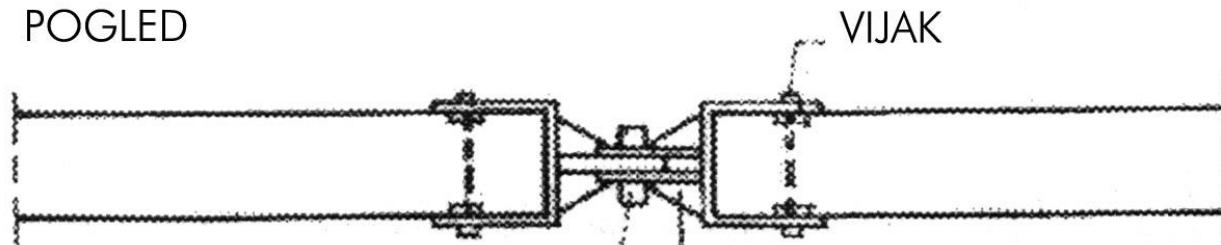
Zglobna veza
greda i
sljemenu lukova
i okvira **većih
raspona**

Varijanta
“bolzen” zgloba

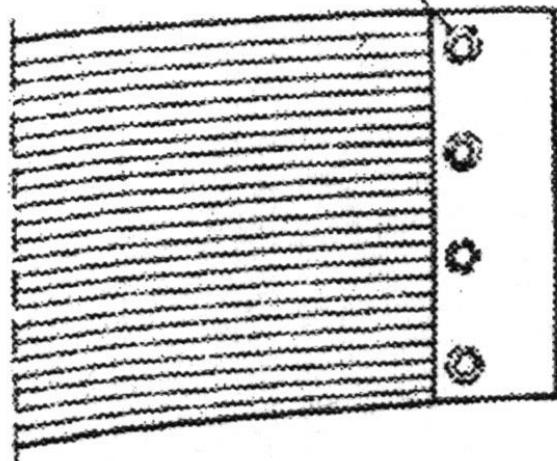


Konstrukcije zglobova u tjemenu lukova i okvira

POGLED

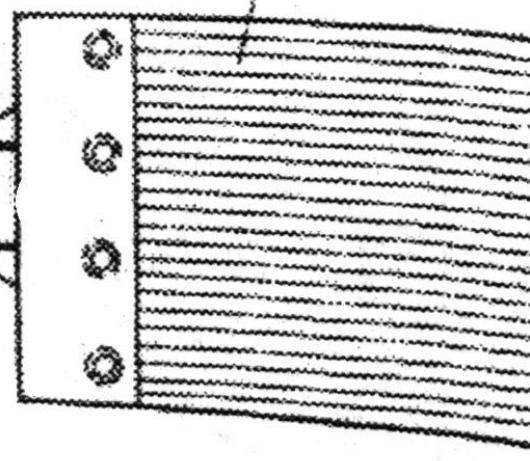


MOŽDANIK



VELIKI RASPONI

LUK

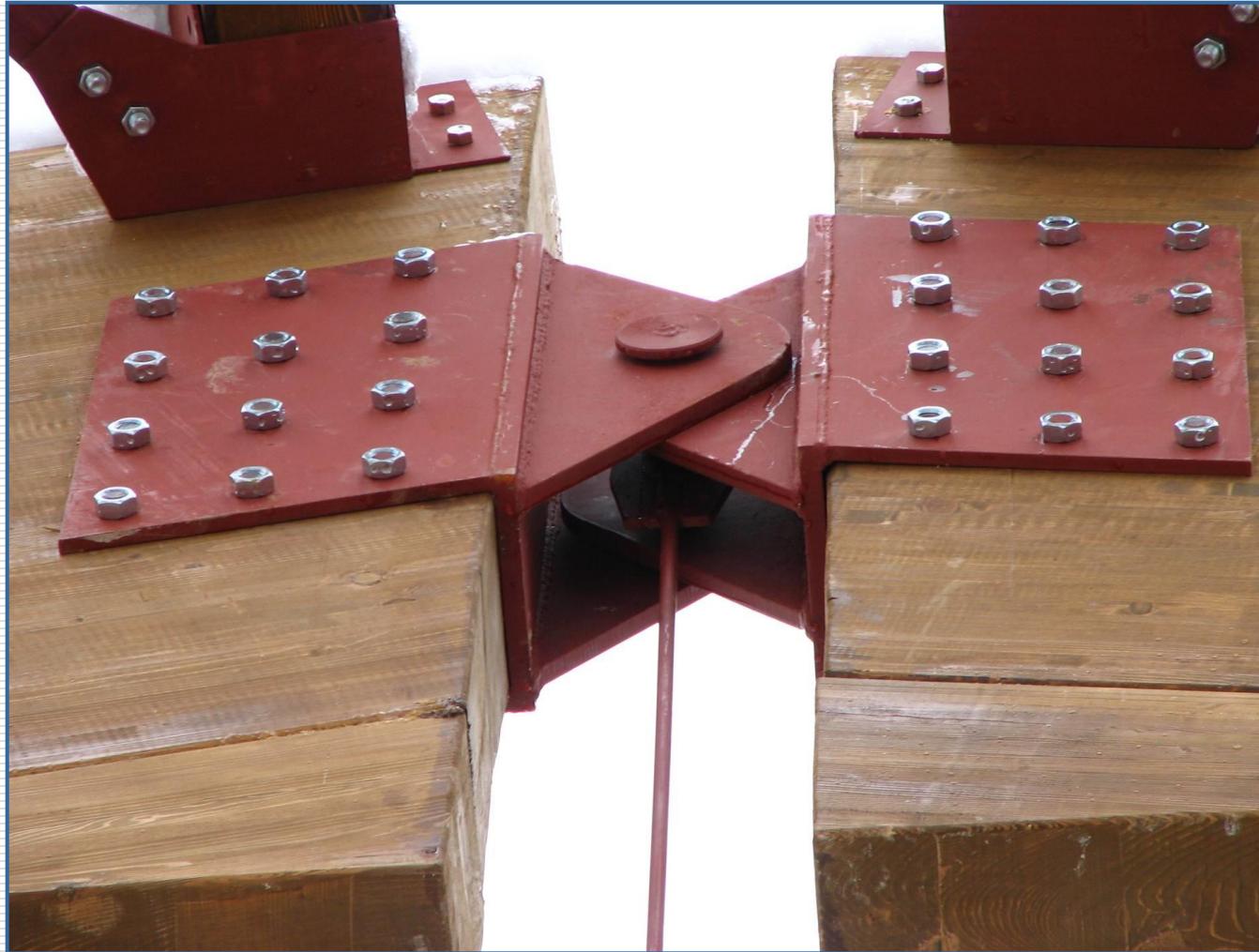


Zglobna veza
greda i
sljemenu
lukova i okvira
većih raspona

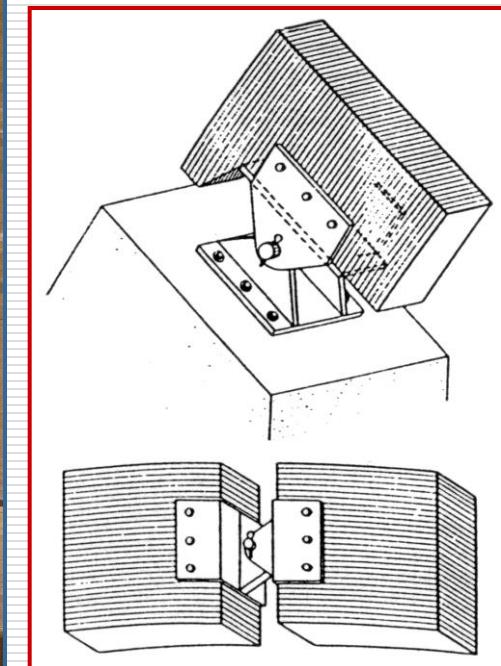
Varijanta
“bolzen” zgloba



Konstrukcije zglobova u tjemenu lukova i okvira

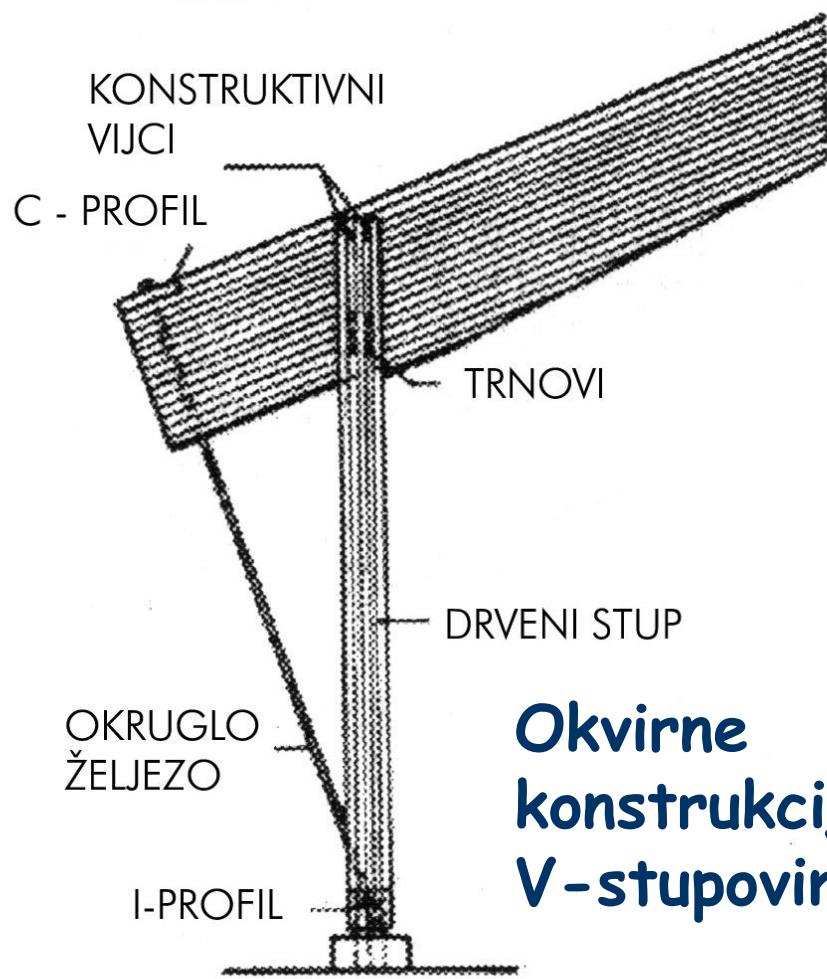


Varijanta
“bolzen” zgloba

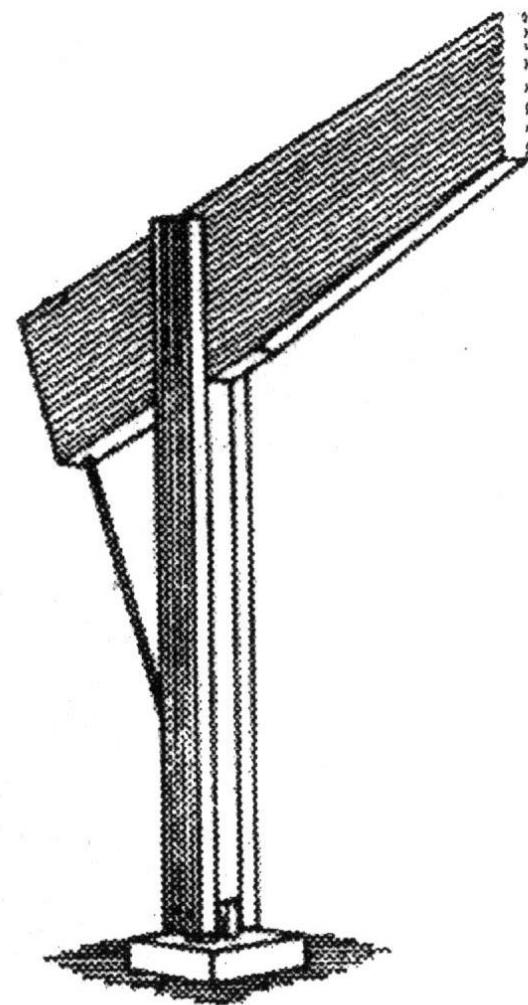




MOGUĆE IZVEDBE STUPOVA



**Okvirne
konstrukcije sa
V-stupovima**

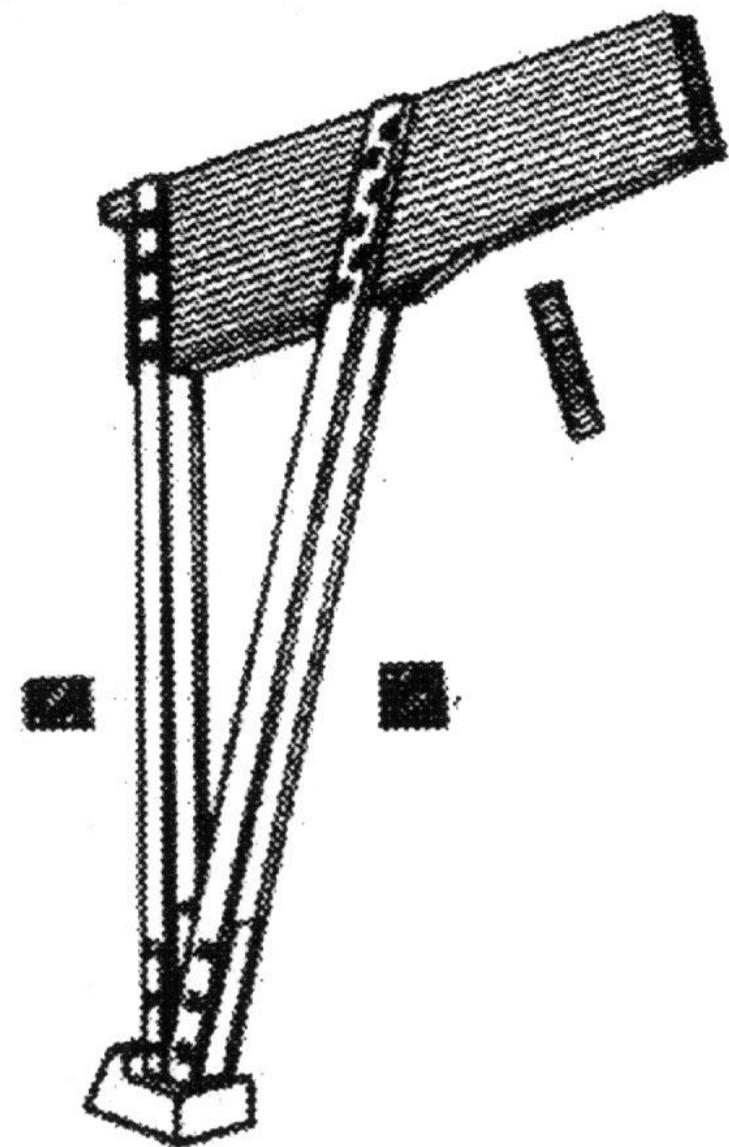


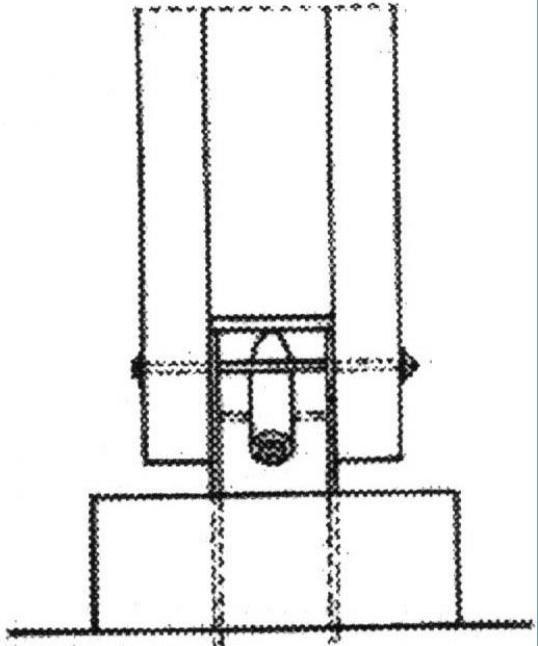
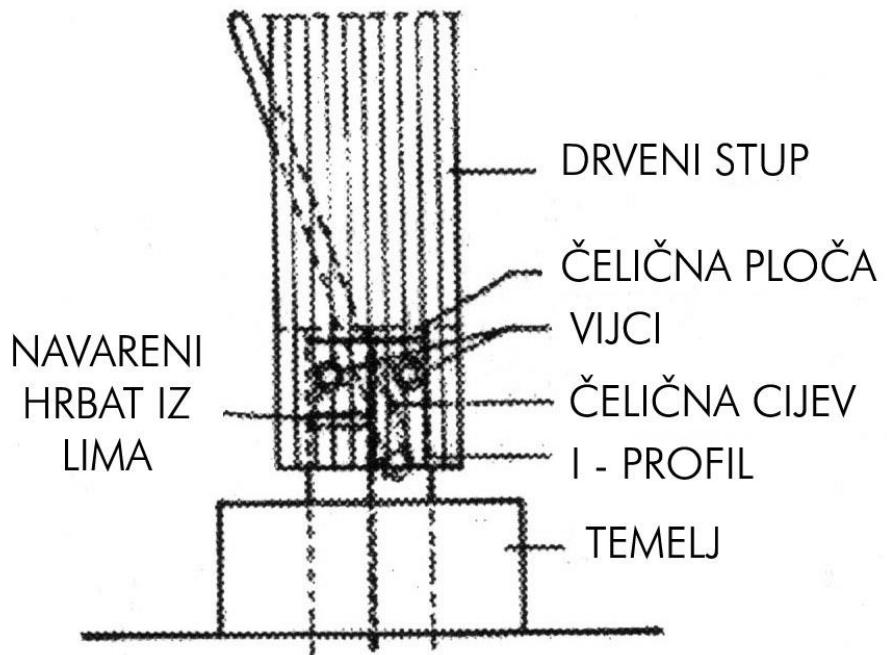


Metalna
papuča
navarena na
čeličnu
podložnu ploču

(naprezanja
pod kutem !!!)

Drveni umetak
između stupova

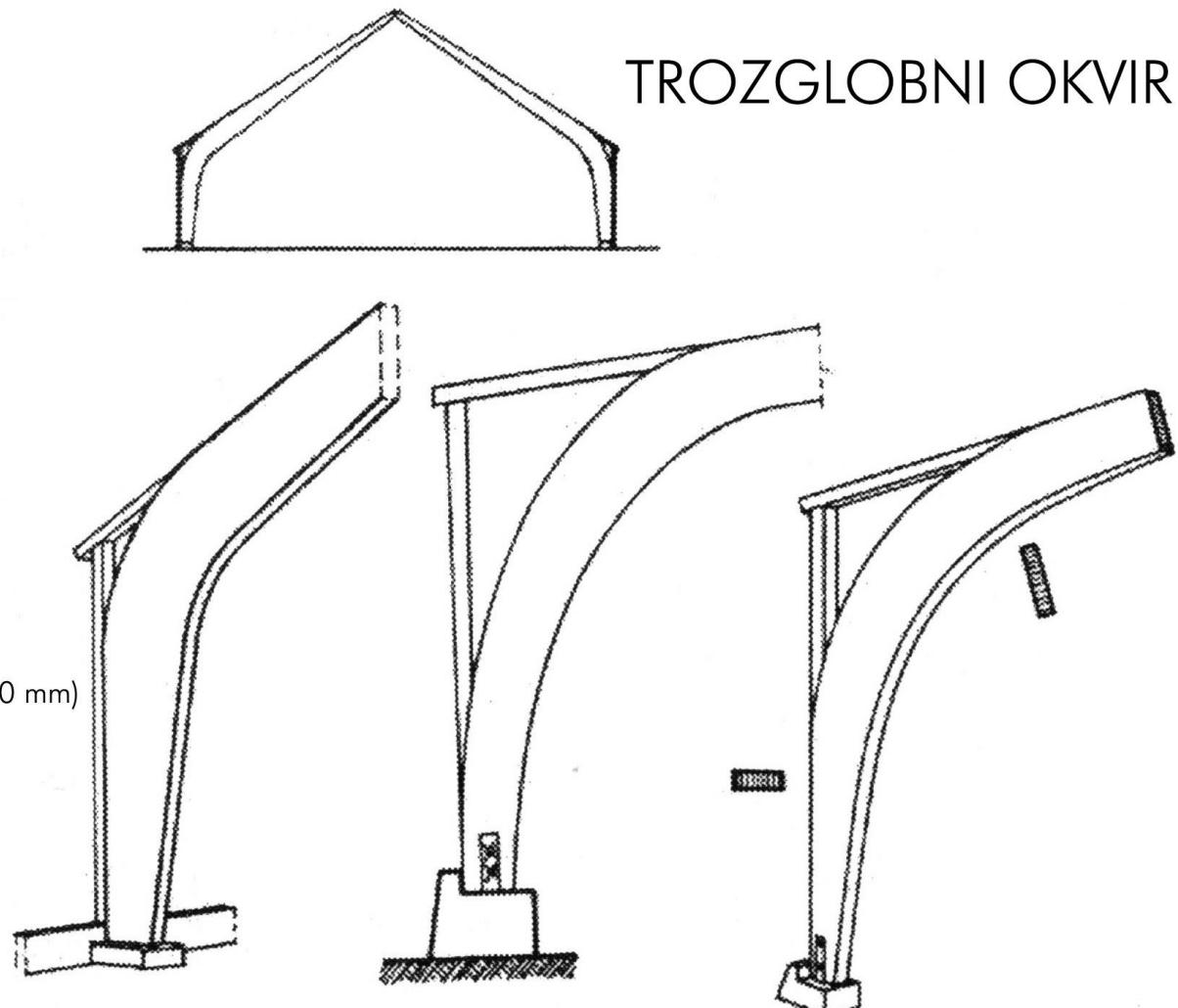
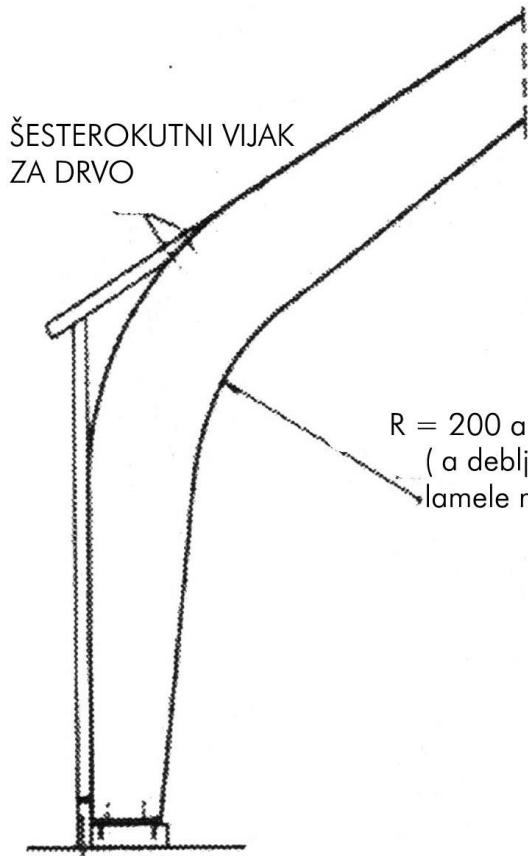




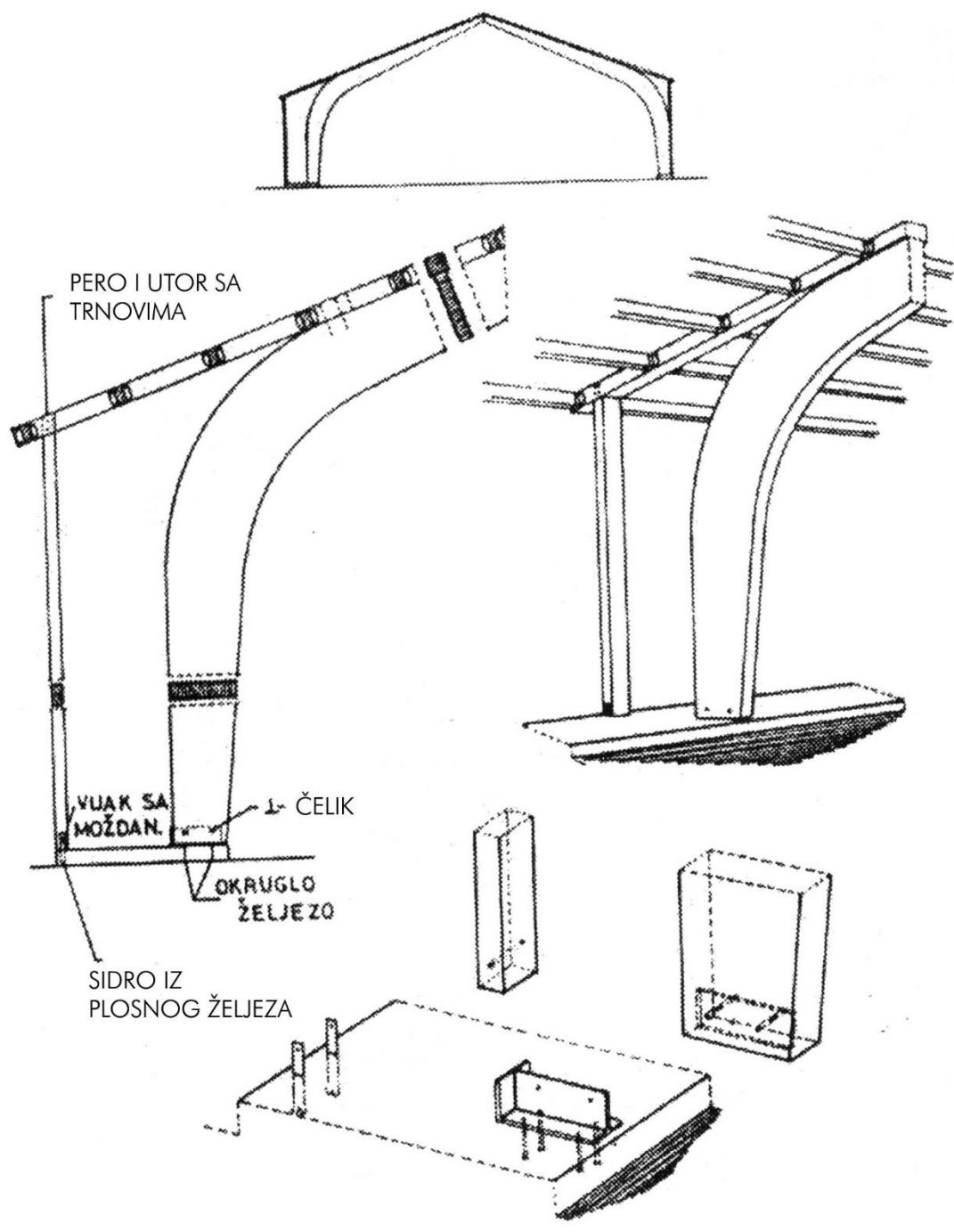
**Slobodna rotacija
(zglob) !!!**

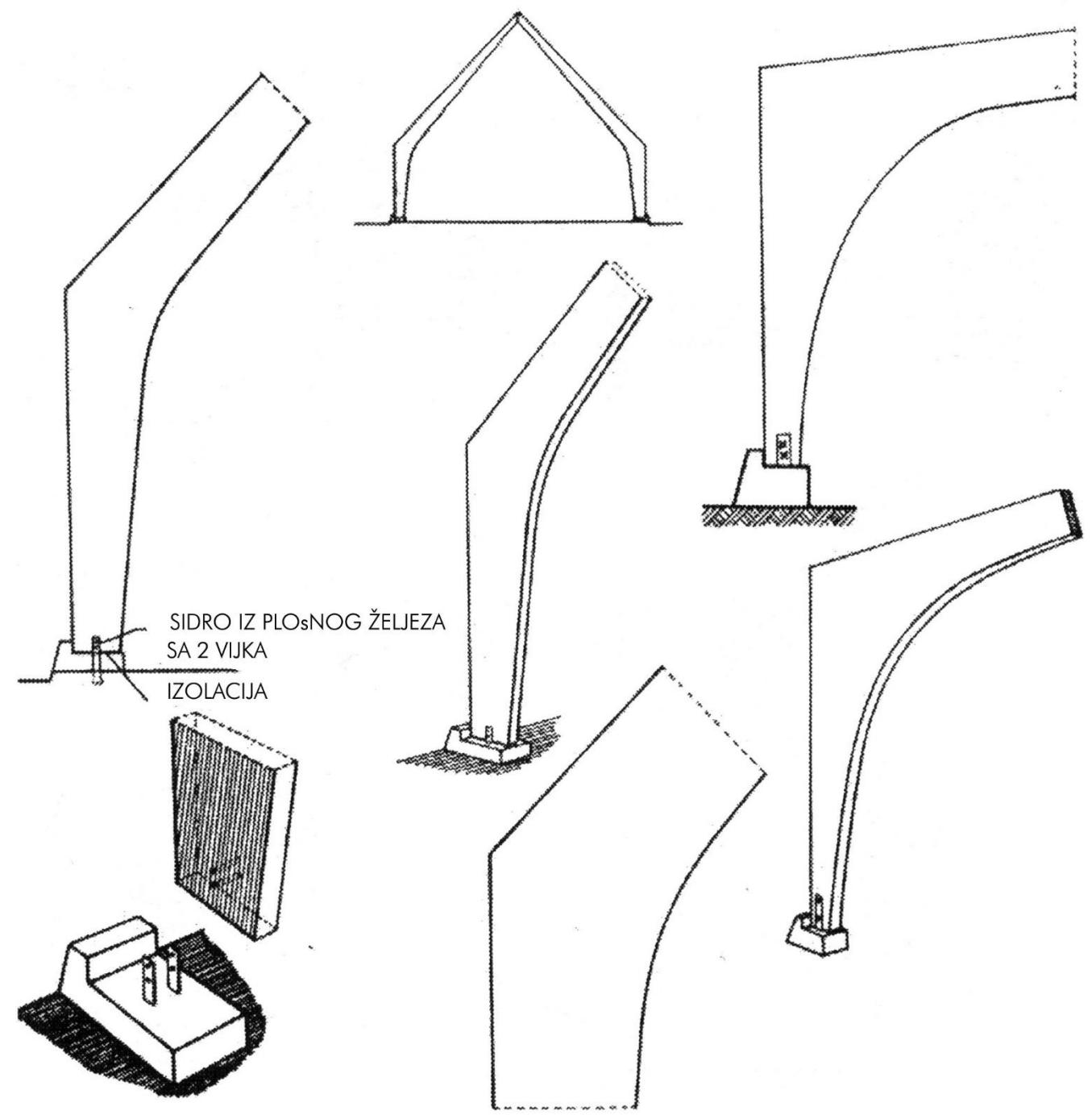


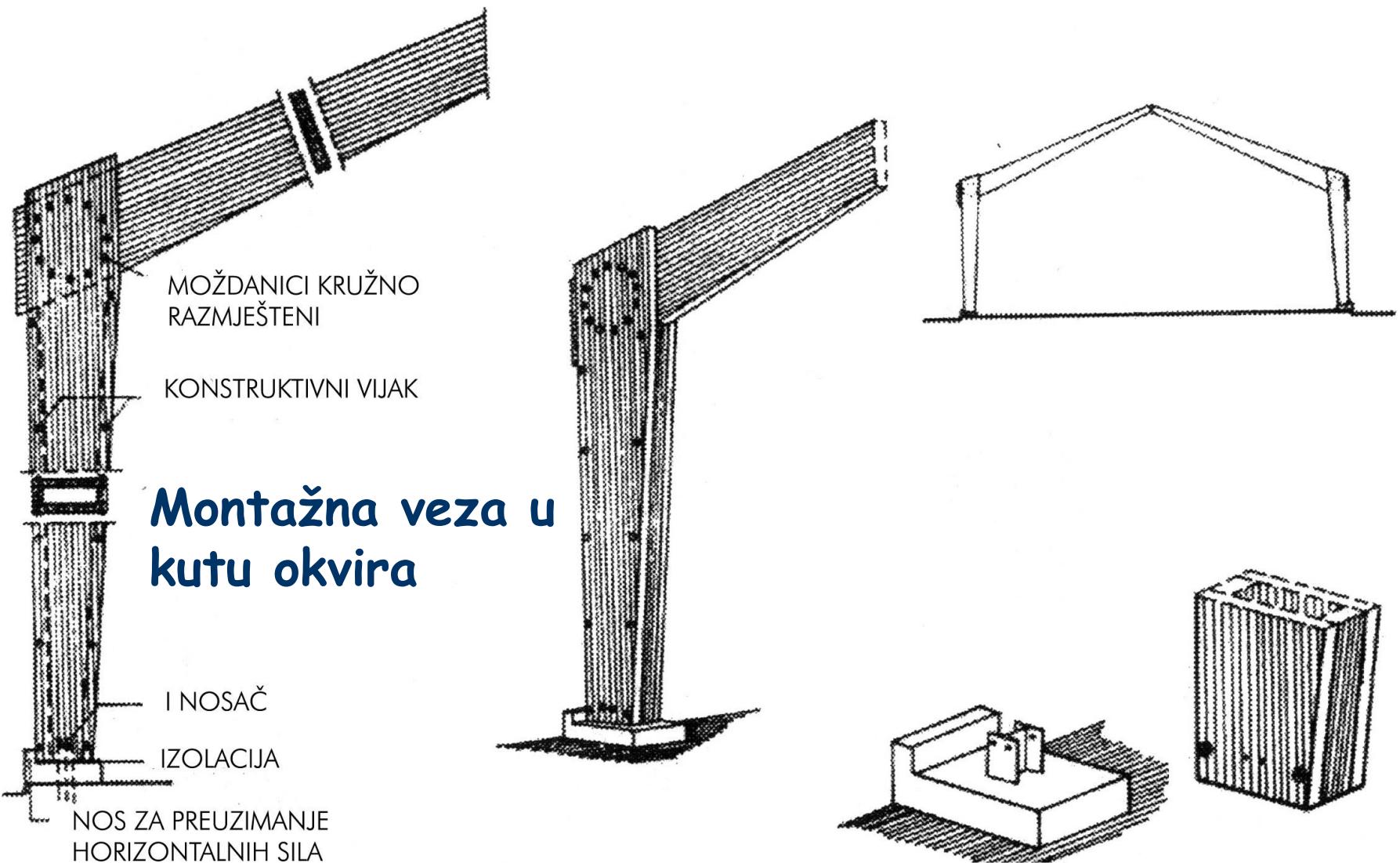
TROZGLOBNI OKVIR



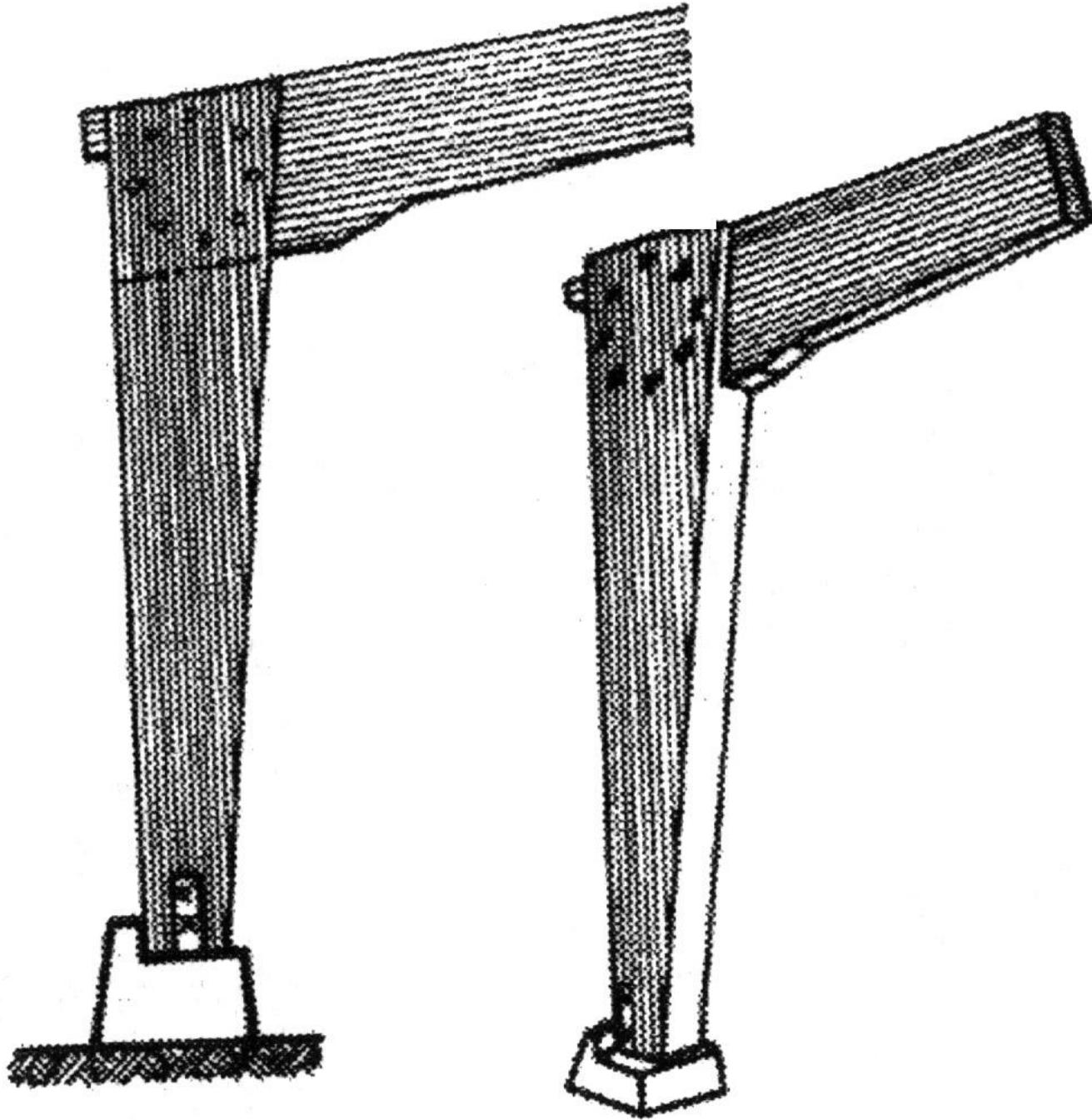
NOS ZA PREUZIMANJE
HORIZONTALNIH SILA

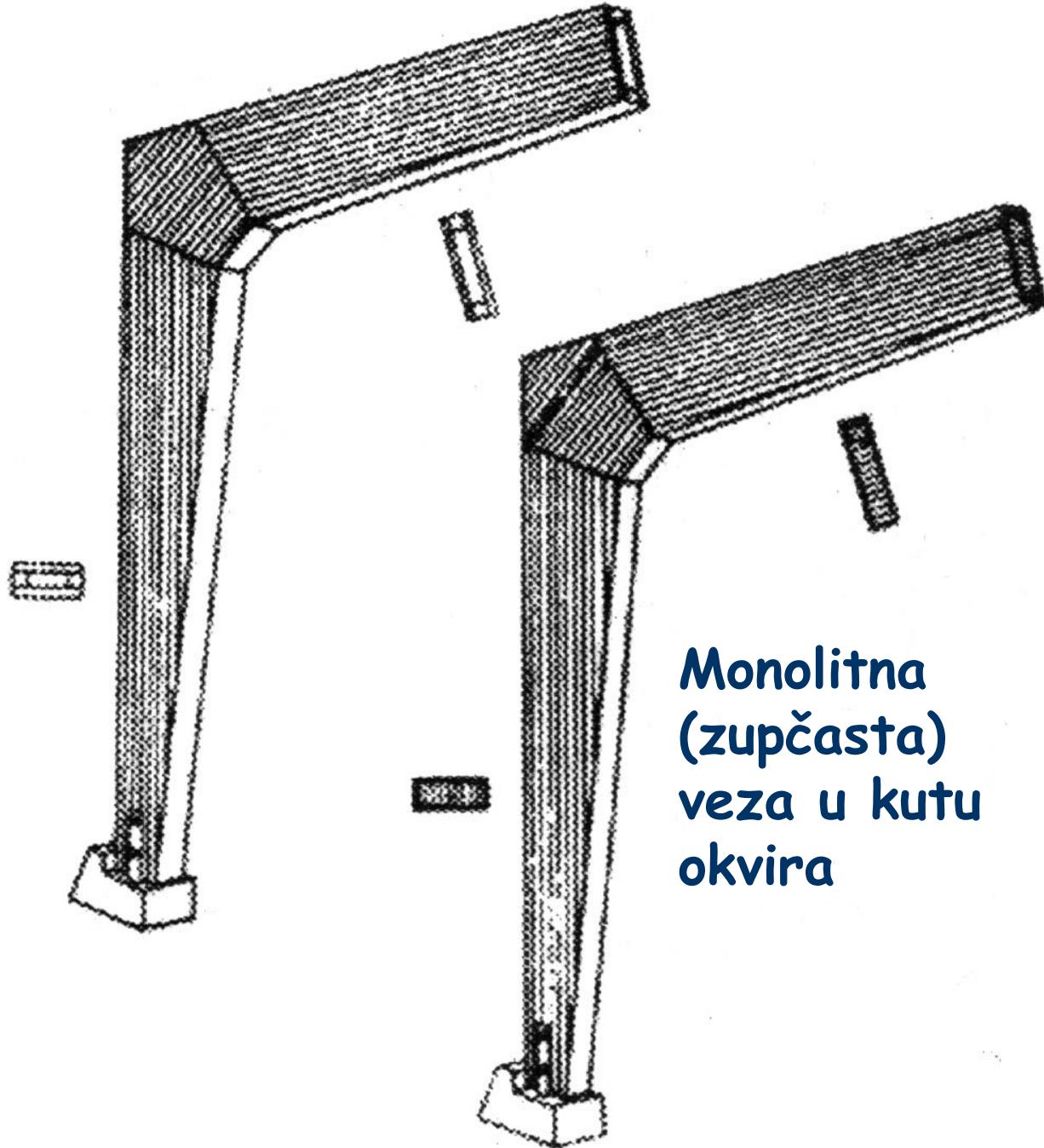




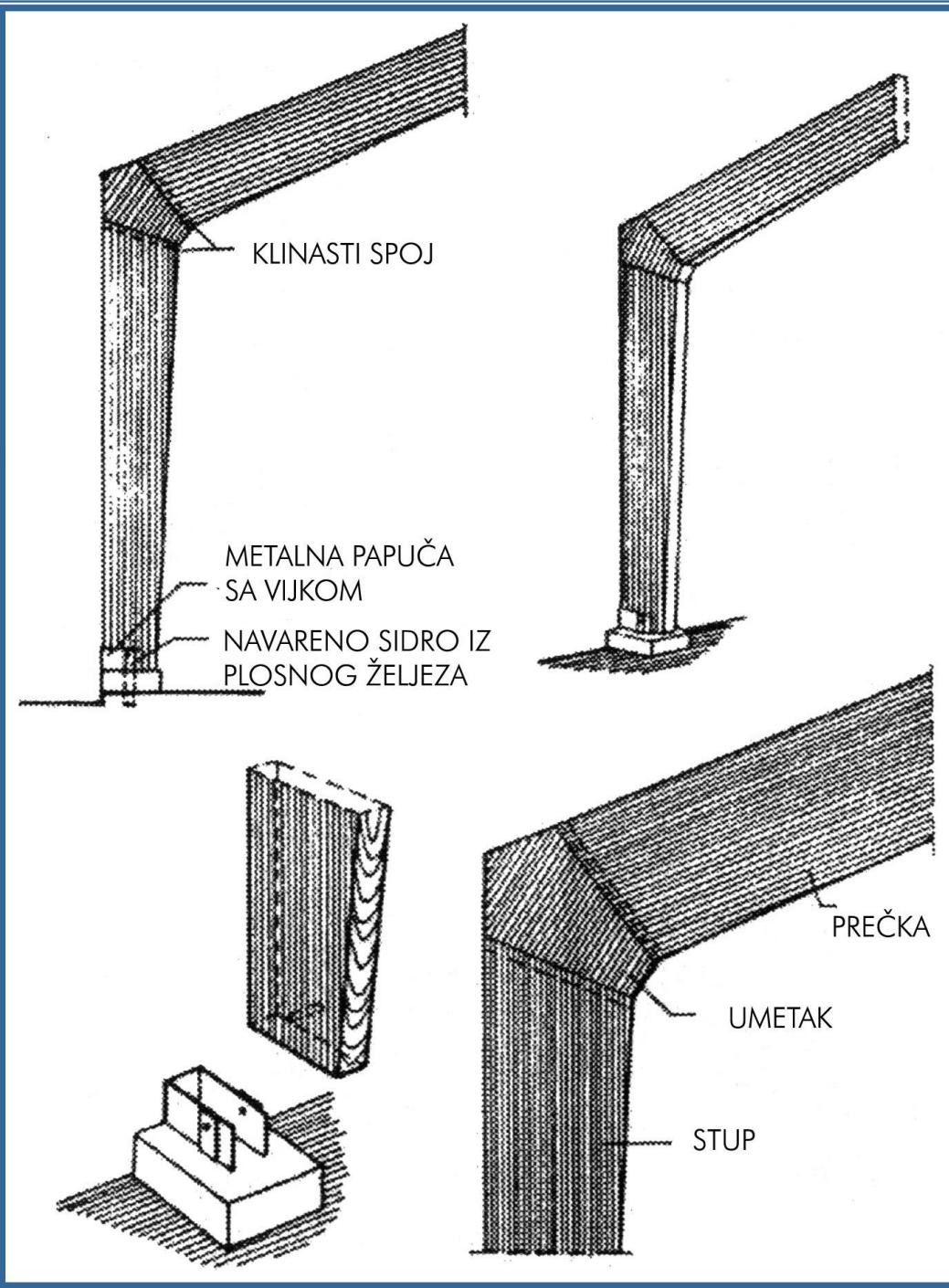


Montažna veza u kutu okvira

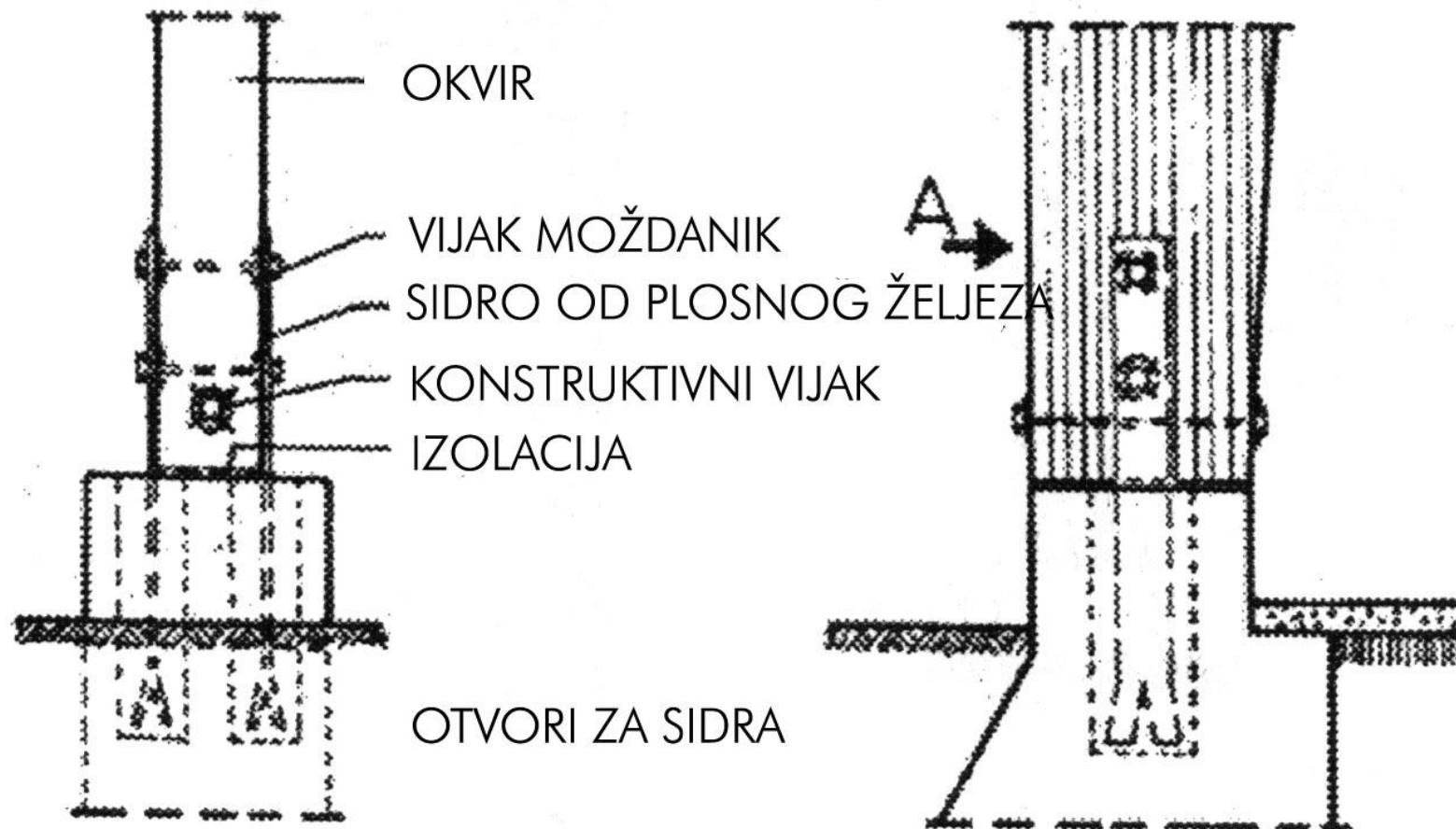
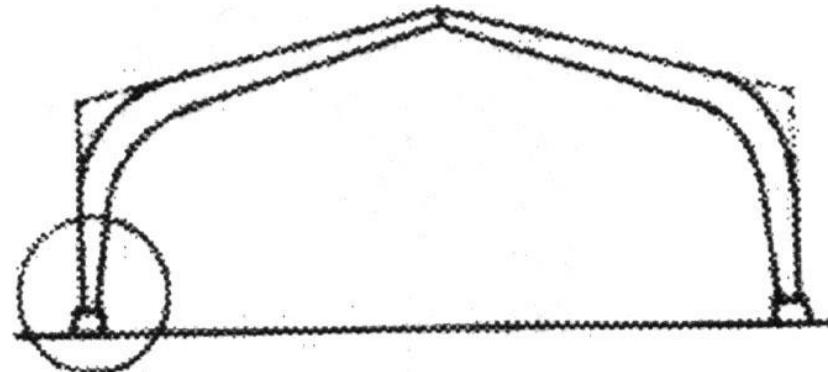




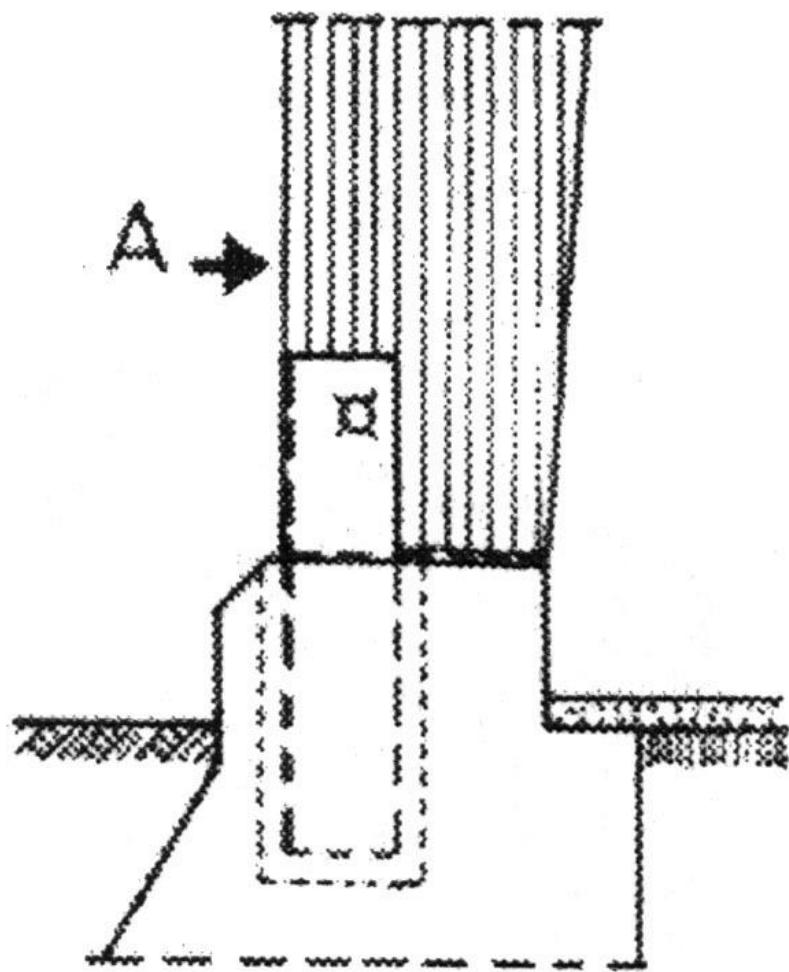
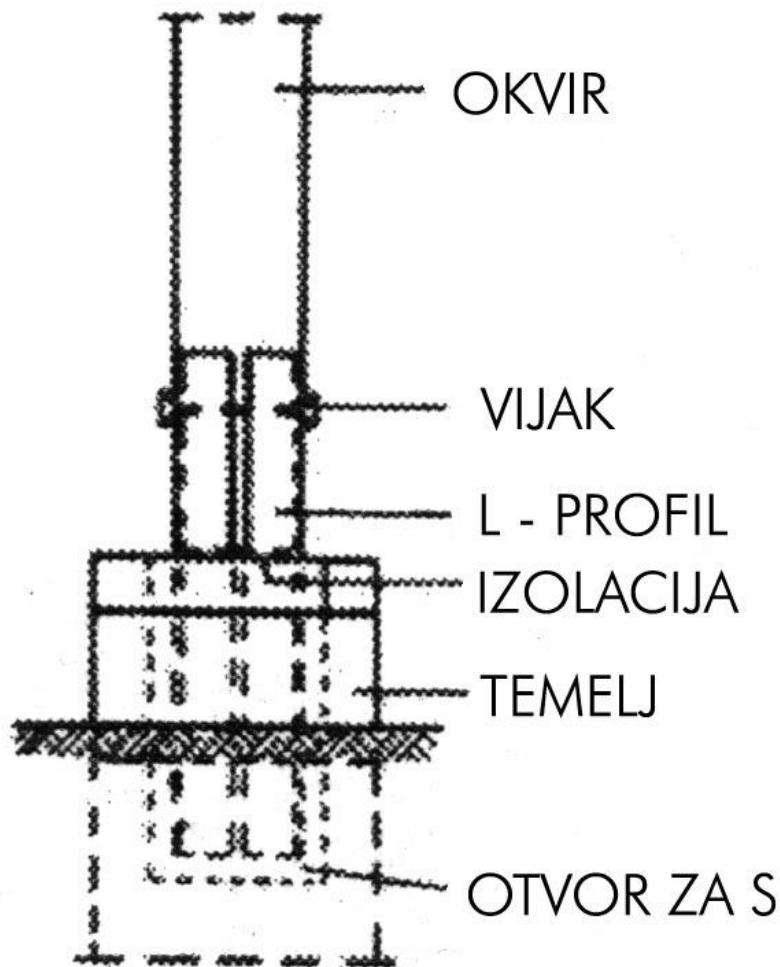
Monolitna
(zupčasta)
veza u kutu
okvira



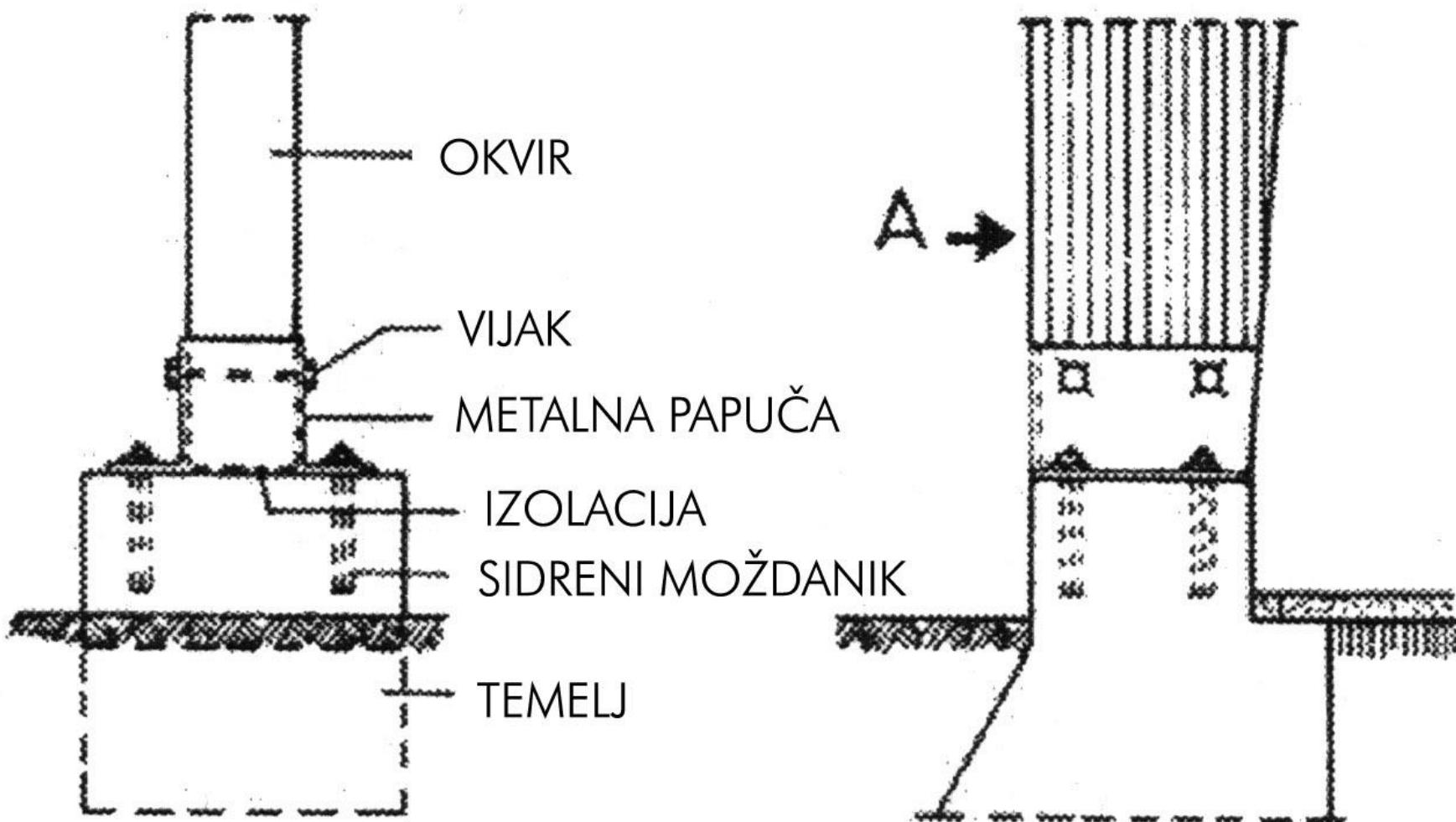
POGLED "A"



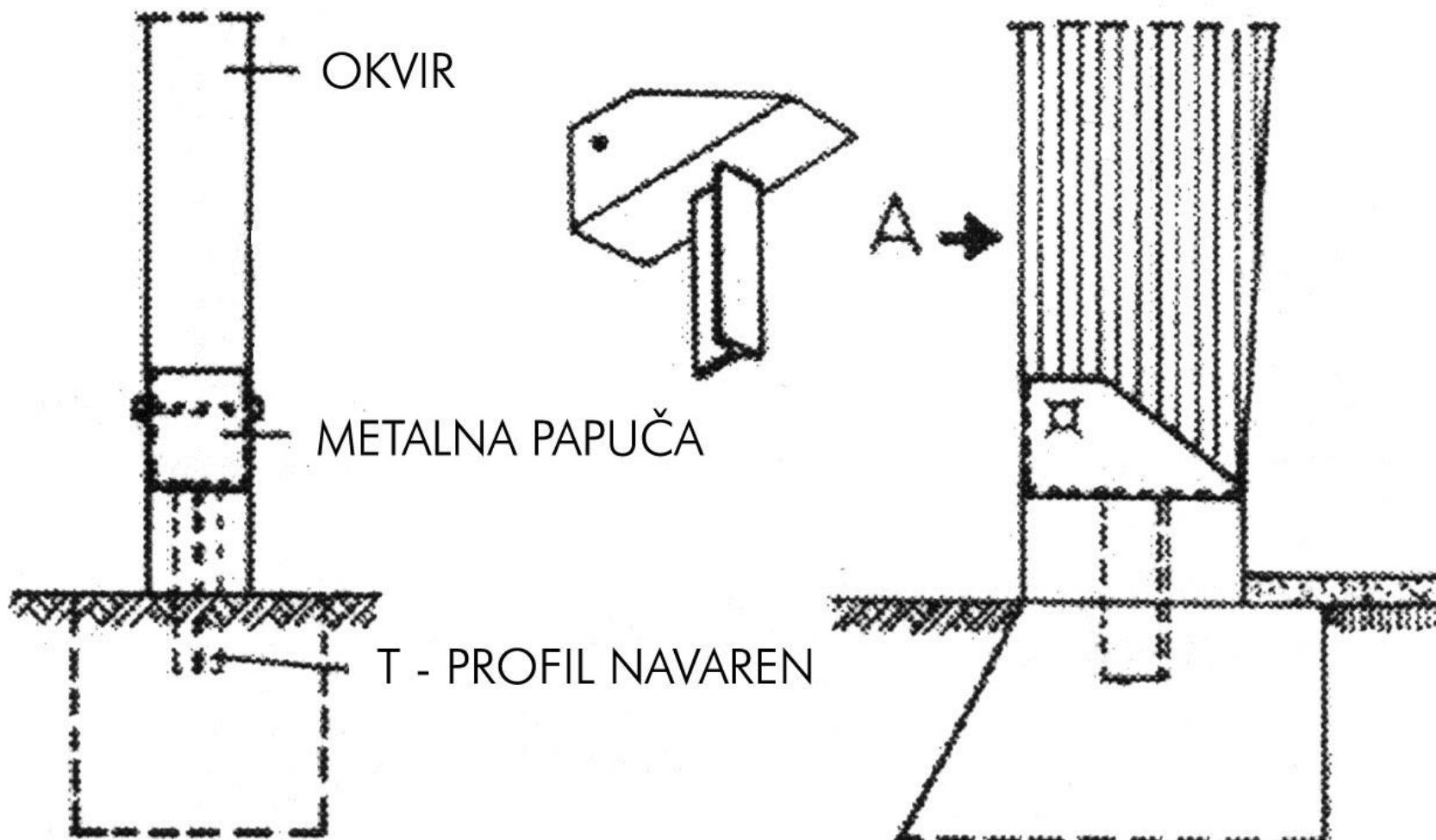
POGLED "A"



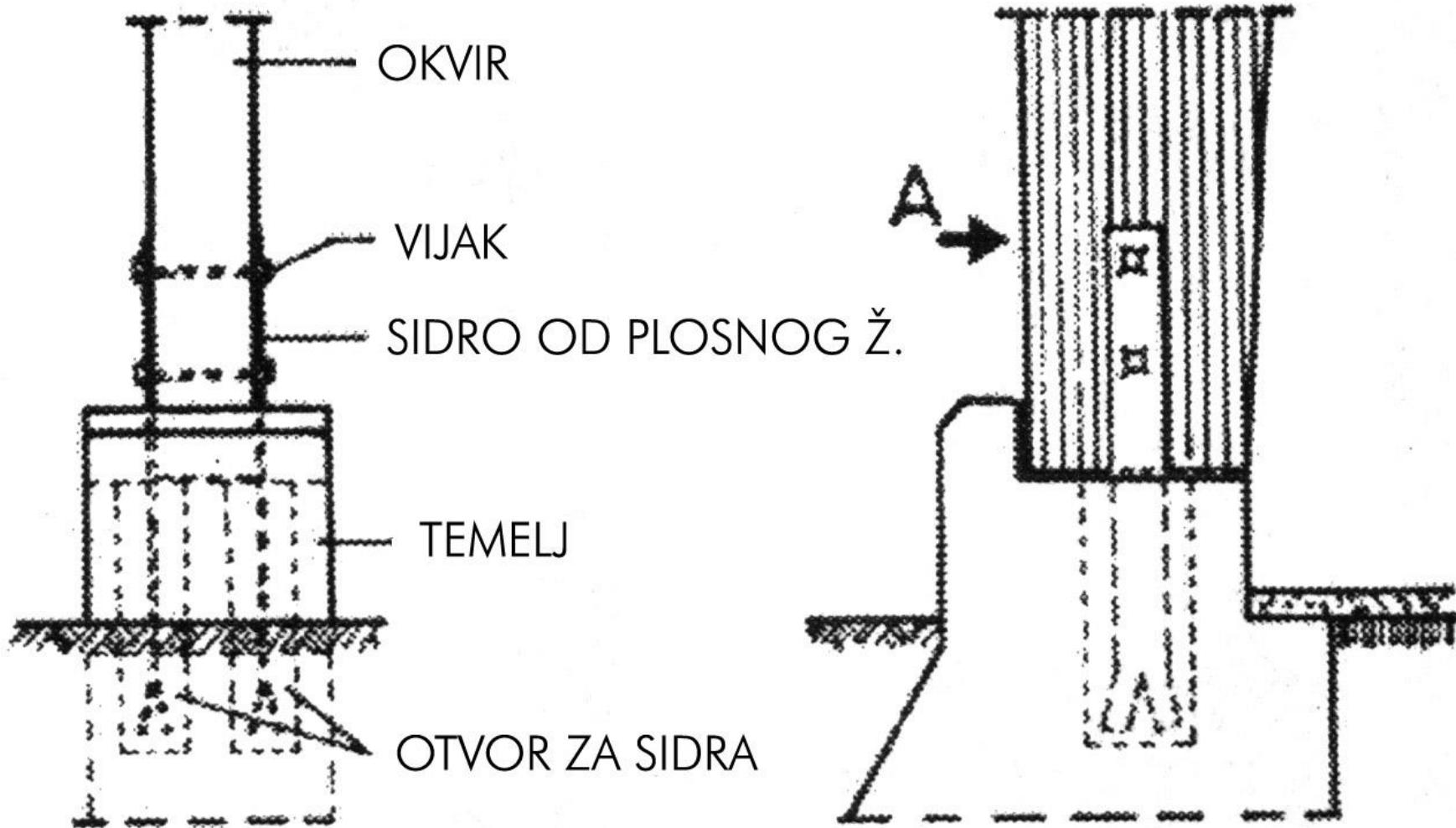
POGLED "A"



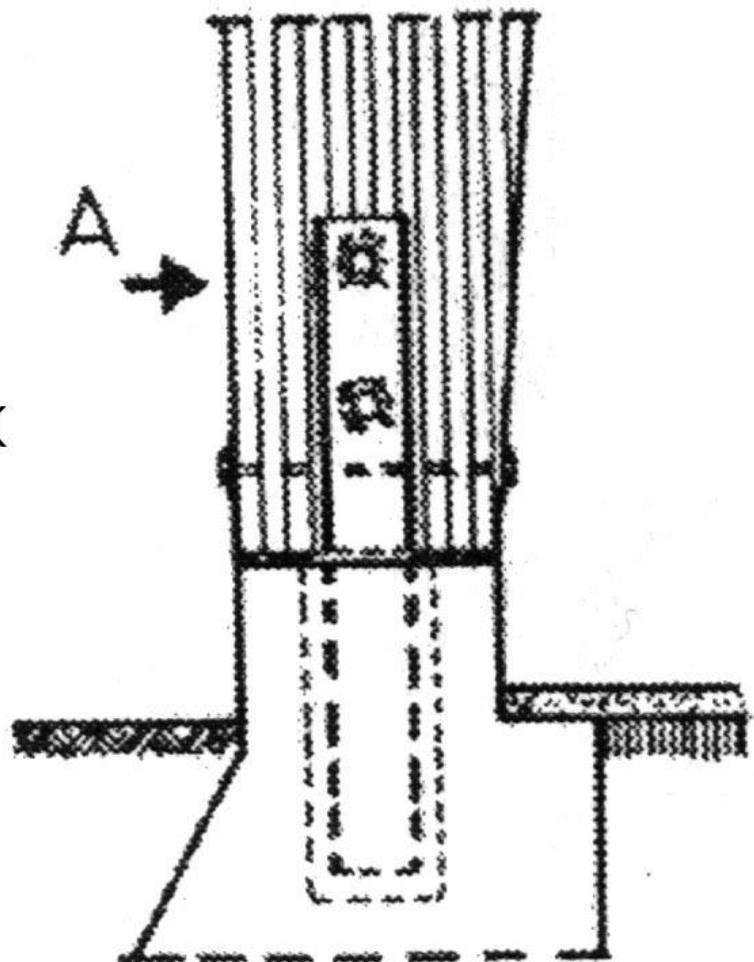
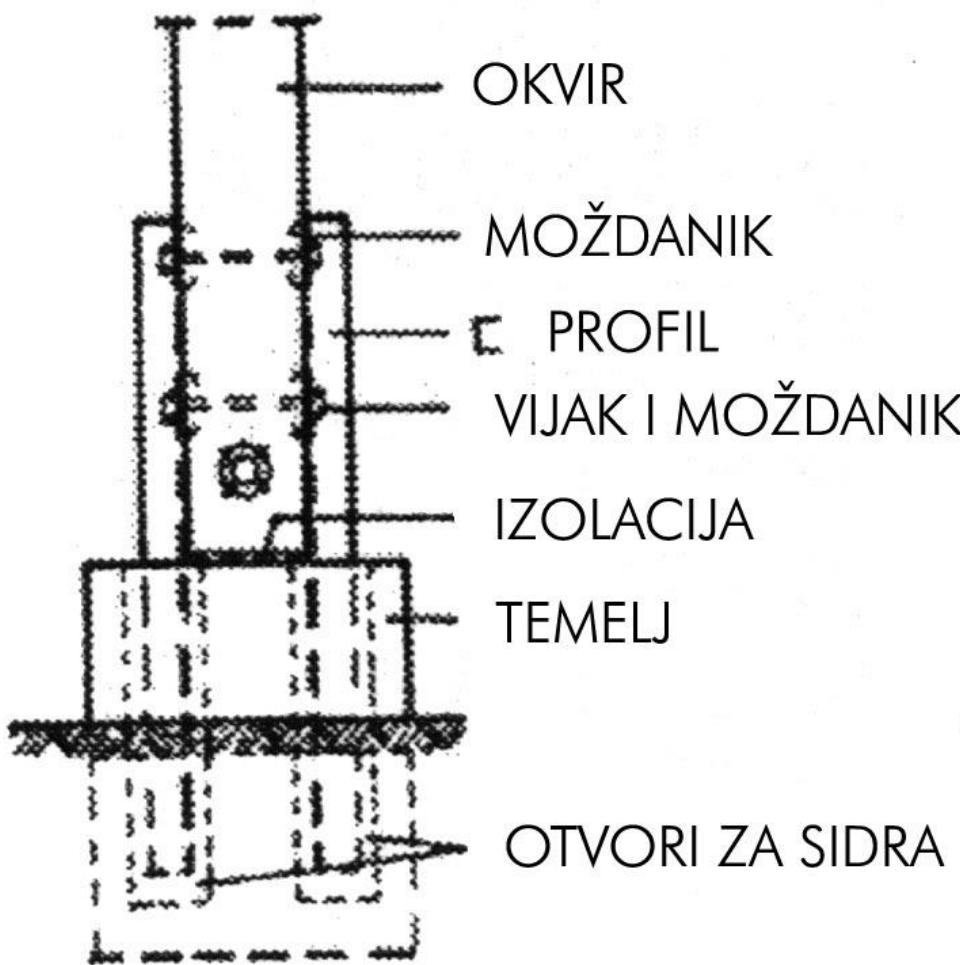
POGLED "A"



POGLED "A"



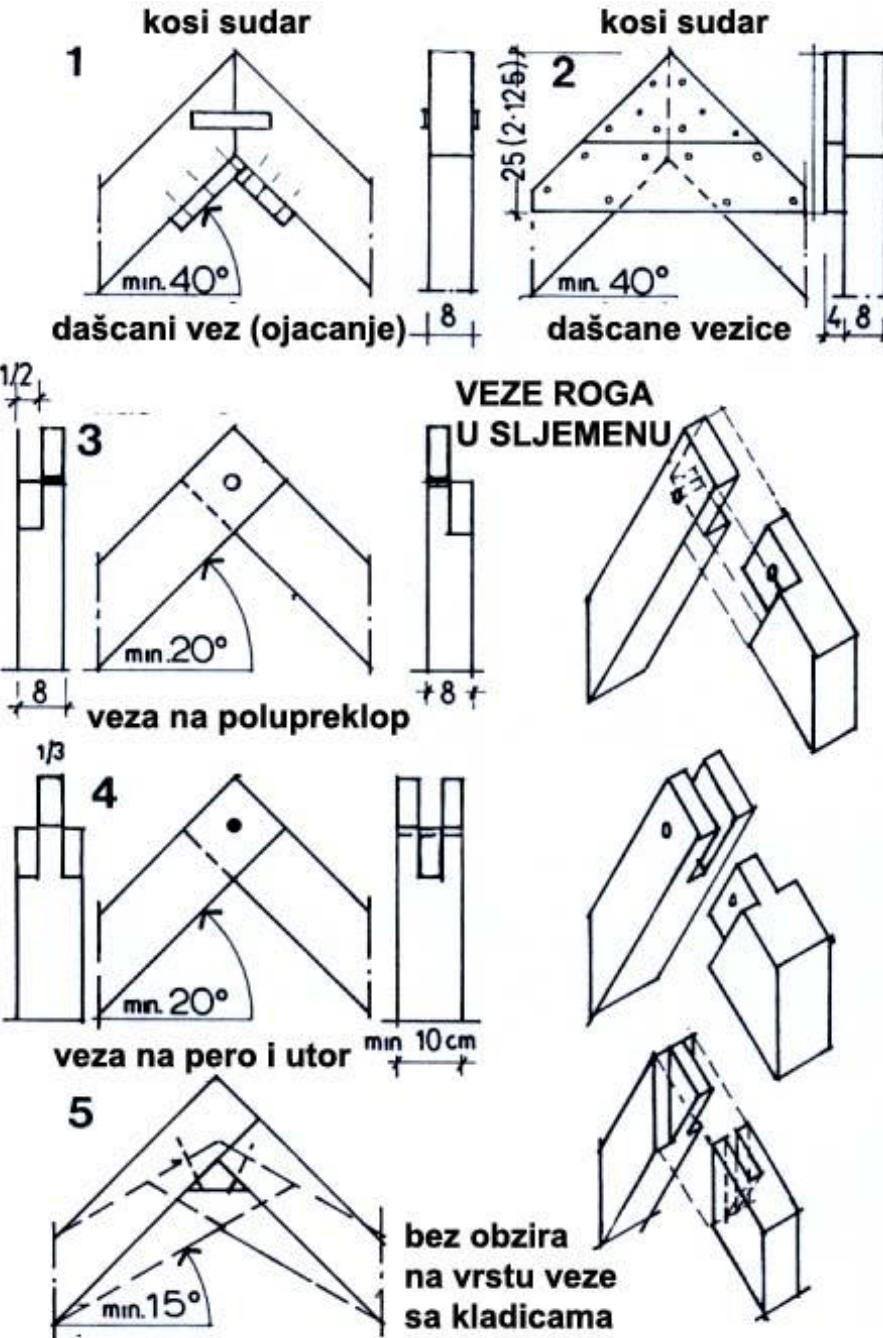
POGLED "A"



Osnove oblikovanja sljemena i ležaja u sustavima krovišta

DETALJI VEZA NOSIVIH ELEMENATA

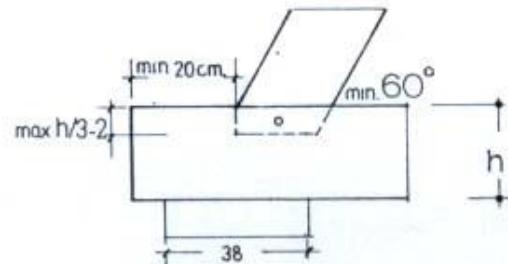
□ Detalj veze rogova u sljemenu



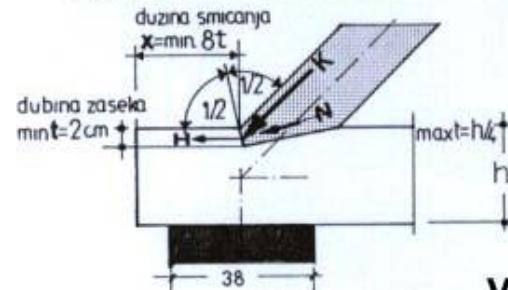
DETALJI VEZA NOSIVIH ELEMENATA

 Oslonac roga
na drvenu
veznu gredu

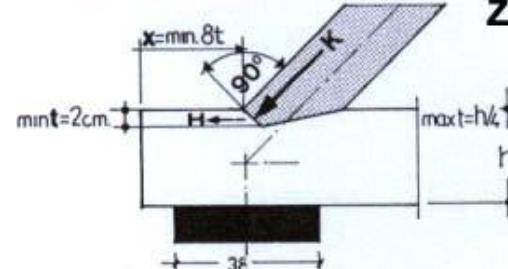
DETALJ OSLANJANJA ROGA - DRVENA STROPNA GREDA



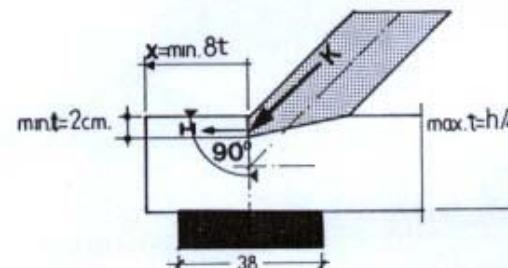
KOSI PREDNJI ČEONI



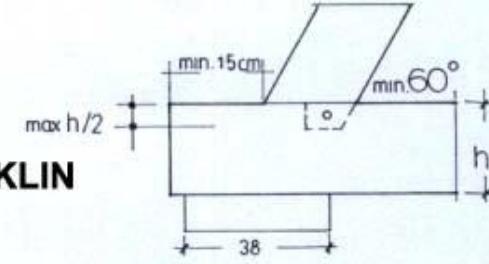
NORMALI



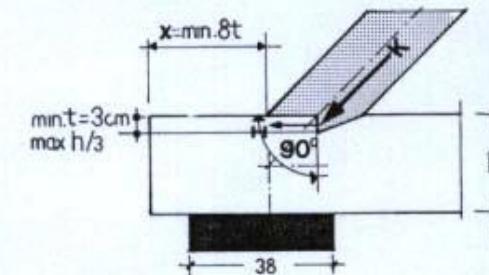
VERTIKALNI



NA KLIN

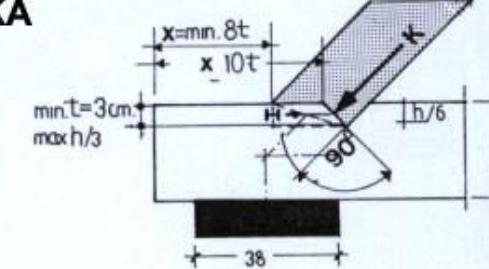


SREDNJI

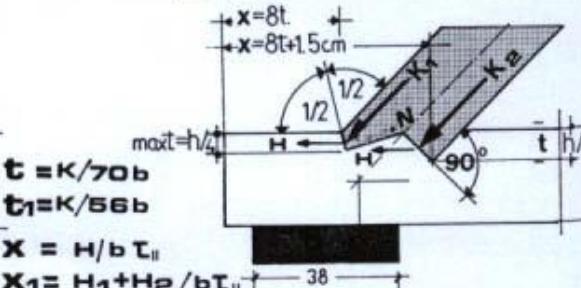


VRSTE I POLOŽAJ ZASJEKA

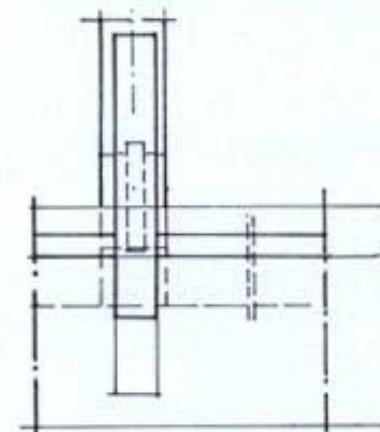
ZADNJI



DUPLI



DETALJ OSLANJANJA ROGOVA - AB STROPNA KONSTR.



Veza roga i praga - na klin

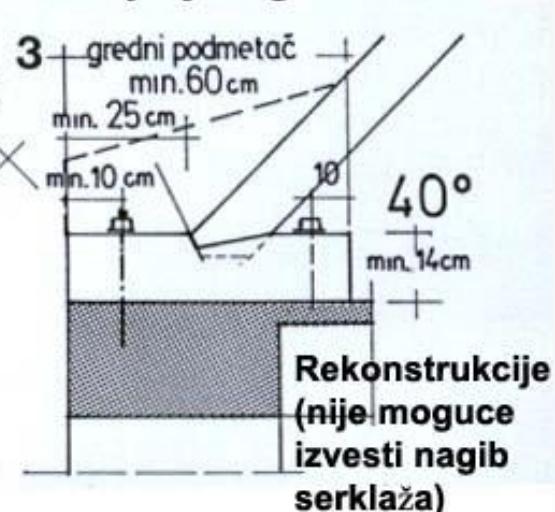
Osiguranje veze
skobicama, metalnim
vezicama ili
konektor-pločama

Prepušteni rog



kladica za vezu s pragom

Oslanjanje roga na kladice



**Rekonstrukcije
(nije moguce
izvesti nagib
serklaža)**

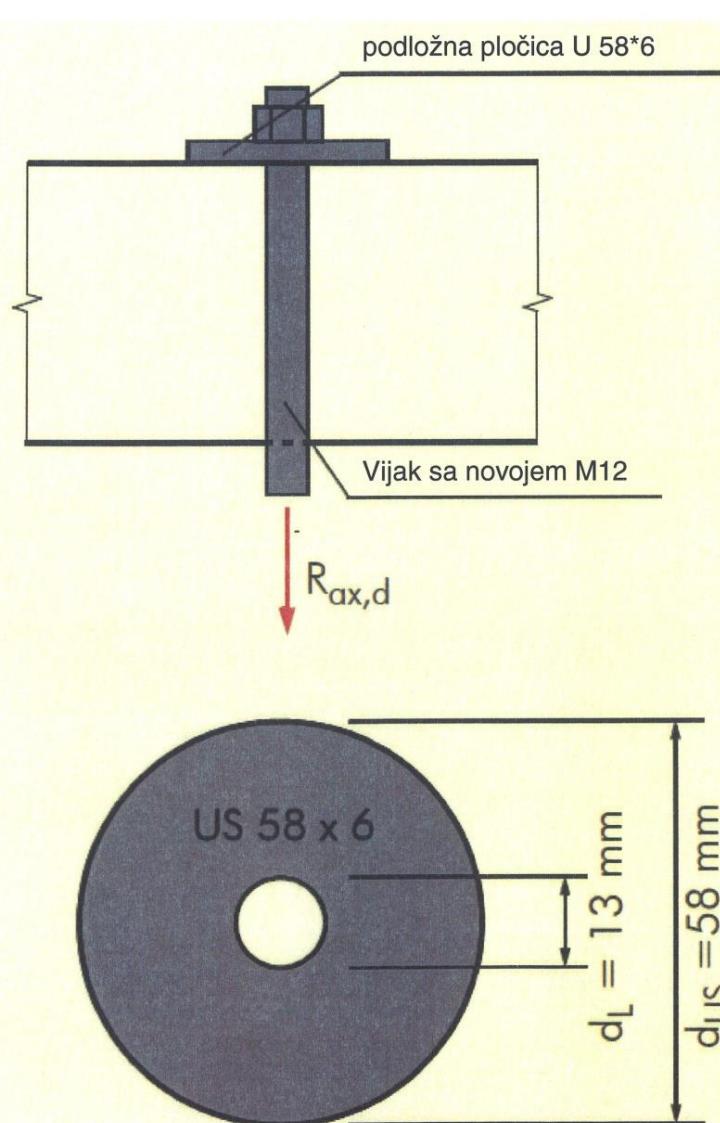
DETALJI VEZA NOSIVIH ELEMENTA

- Oslonac roga
na arm.-
betonsku
stropnu konstr.



Primjer 4.4 Objeseni teret pomoću navijene šipke i podložne pločice

Primjer 4.4 Objeseni teret pomoću navijene šipke i podložnih pločica



Materijal:

Puno drvo C 24

Klasa vlage 1, klasa opterećenja
(kratko), ($k_{mod} = 0,9$).

$$\gamma_M = 1,3$$

Navijena šipka M 12, čelik klase 4.6.

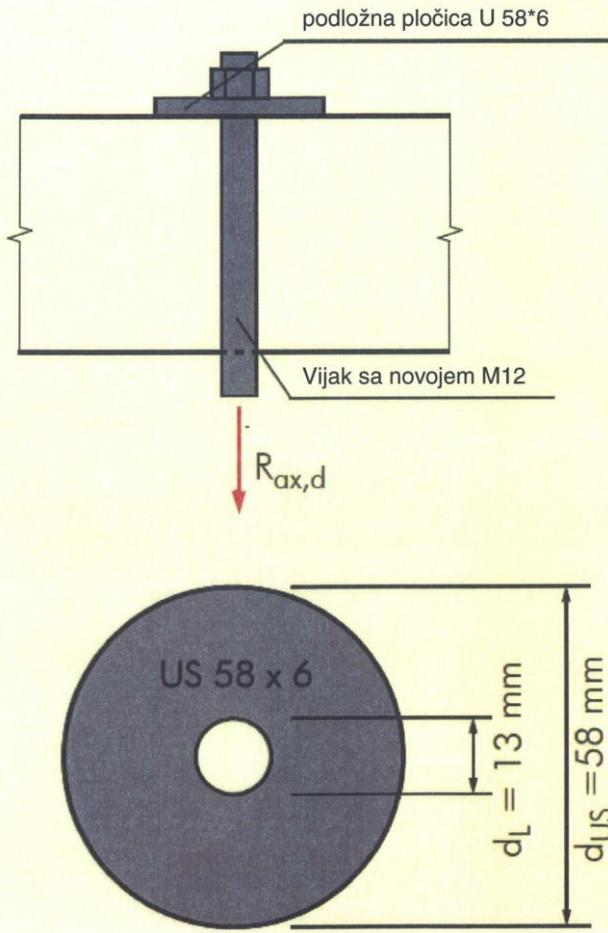
$$\gamma_M = 1,1$$

$$f_{y,k} = 240 \text{ N/mm}^2$$

Podložna pločica:
U 58 x 6 mm

i podložne pločice

Primjer 4.4 Objekten teret pomoću navijene šipke i podložnih pločica



Dokaz nosivosti:

Vlačna nosivost navijene šipke:

$$A_{ef} = 84,3 \text{ mm}^2$$

$$R_{ax,d} = \frac{A_{ef} \cdot f_{y,k}}{\gamma_{st}} = \frac{84,3 \cdot 240}{1,25} = 16186 N$$

Podložna pločica:

$$A_{us} = \pi \cdot (58-13)^2 / 4 = 2509 \text{ mm}^2$$

Ispod podložne pločice drveni elemenat je napregnut tlakom okomito na vlakna

$$f_{c,90,d} = \frac{f_{c,90,k} \cdot k_{mod}}{\gamma_M} = \frac{2,5 \cdot 0,90}{1,30} = 1,73 N / mm^2$$

$$k_{c,90,d} = k_{c,90} \cdot \left(\frac{150}{l} \right)^{0,25} = 1,80 \cdot \left(\frac{150}{58} \right)^{0,25} = 2,28$$

$$R_{US,d} = A_{US} \cdot f_{c,90,d} \cdot k_{c,90} = 2509 \cdot 1,73 \cdot 2,28 = 9897 \text{ N} - \text{mjerodavna sila}$$